



university of
 groningen

kvi - center for advanced
 radiation technology

Optimization of low-energy beam transport

Kernfysisch Versneller Instituut –
Center for advanced radiation technology (KVI-CART)

H.R. Kremers, J.P.M. Beijers, S. Brandenburg
Zernikelaan 25, 9747 AA, Groningen.
The Netherlands

- Introduction
- KVI- situation (brief)
 - Magnet aberrations and 4rms-emittance growth
- Optimization low energy beam line
 - Quick compensation by an additional sextupole effect?
 - General method to calculate the 4rms-emittance growth
 - Sextupoles
 - Solenoid lens
 - Einzel
 - Conclusions.

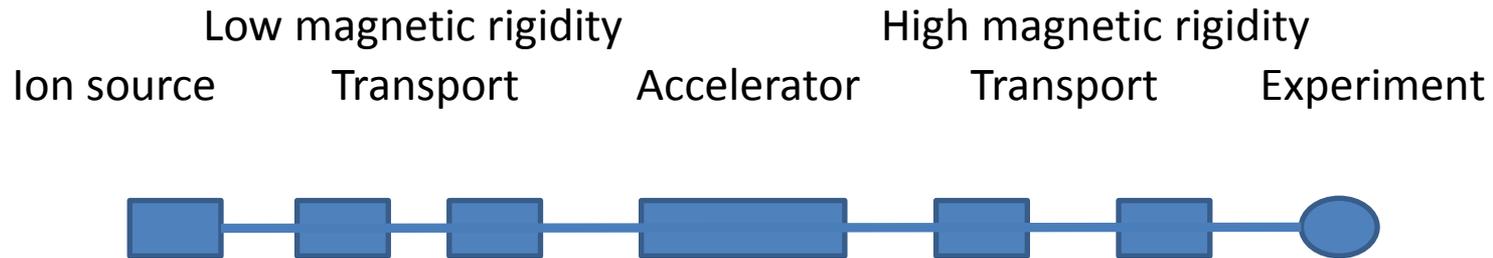
Introduction



university of
 groningen

kvi - center for advanced
 radiation technology

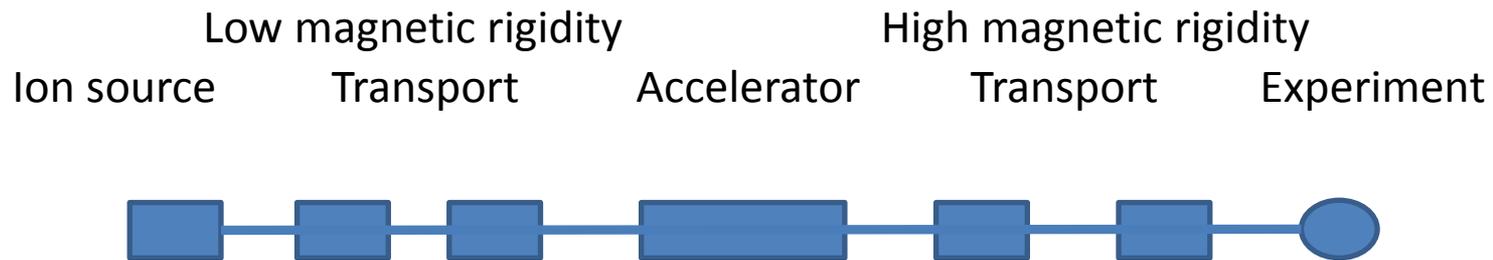
Accelerator Laboratories:



Introduction



Accelerator Laboratories:

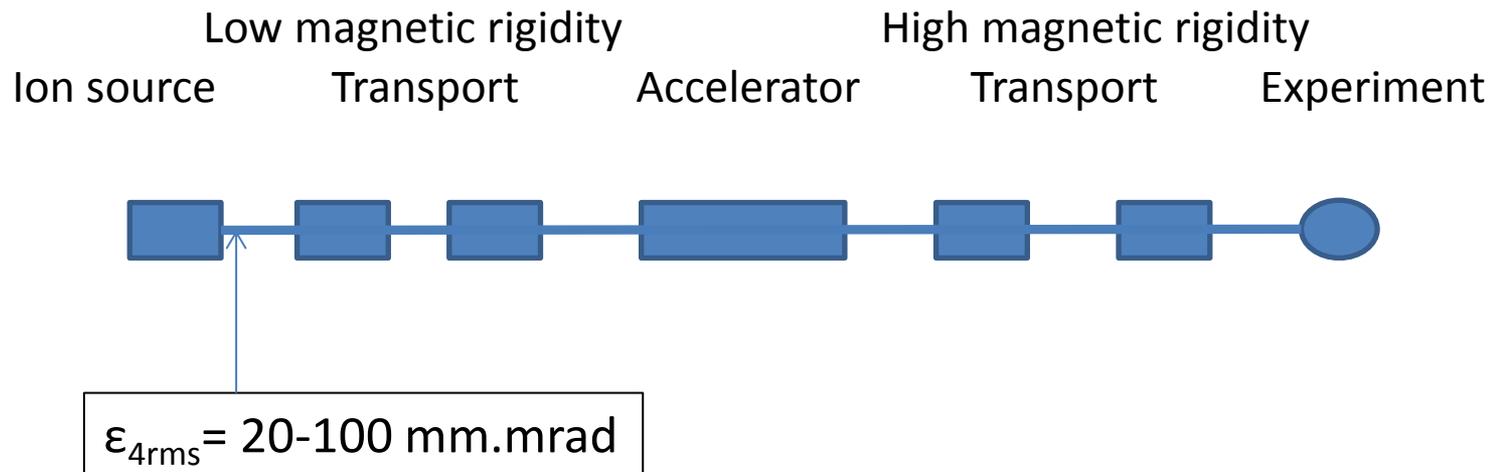


$$\epsilon_{4rms} = 20-100 \text{ mm.mrad}$$

Introduction



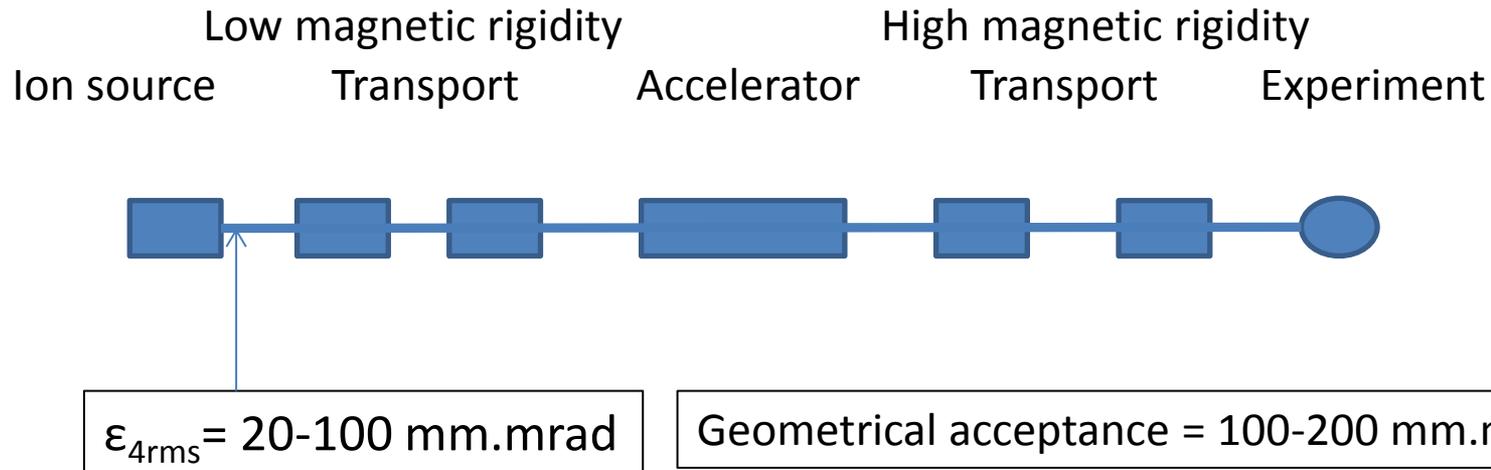
Accelerator Laboratories:



Introduction



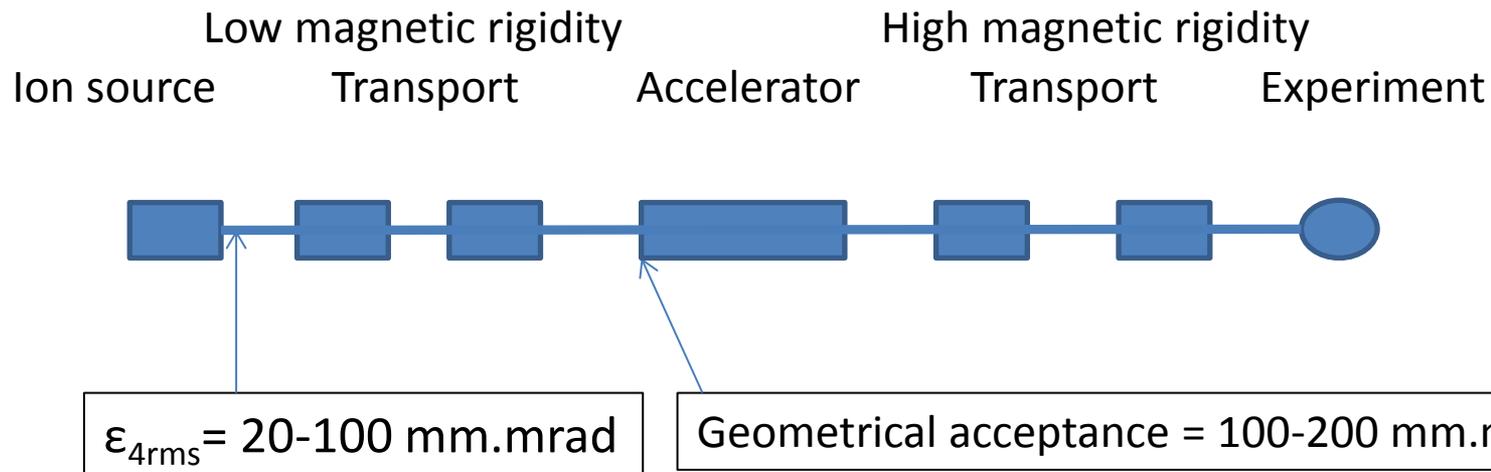
Accelerator Laboratories:



Introduction



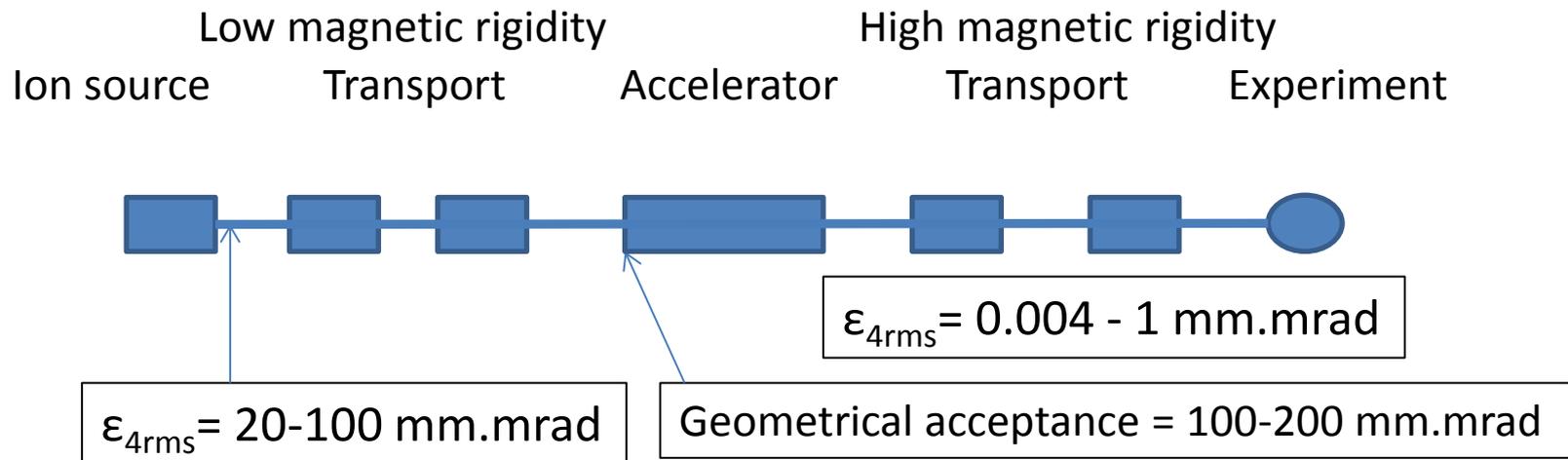
Accelerator Laboratories:



Introduction



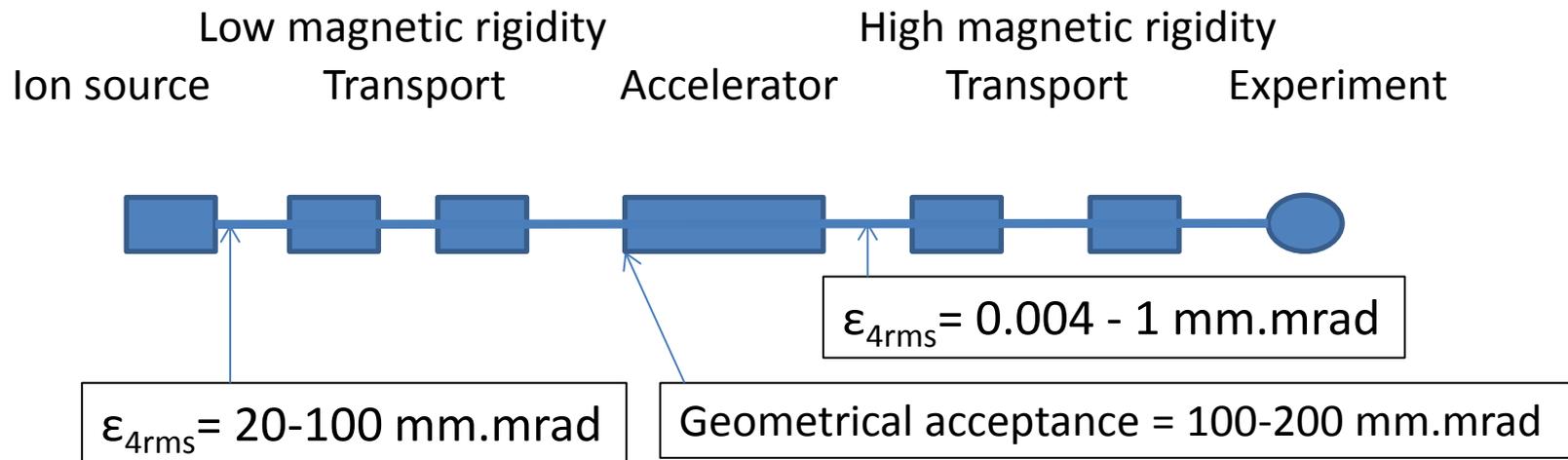
Accelerator Laboratories:



Introduction



Accelerator Laboratories:



Introduction



Accelerator Laboratories:

$$\epsilon_{4rms} = 300-600 \text{ mm.mrad}$$

Low magnetic rigidity High magnetic rigidity
Ion source Transport Accelerator Transport Experiment



$$\epsilon_{4rms} = 0.004 - 1 \text{ mm.mrad}$$

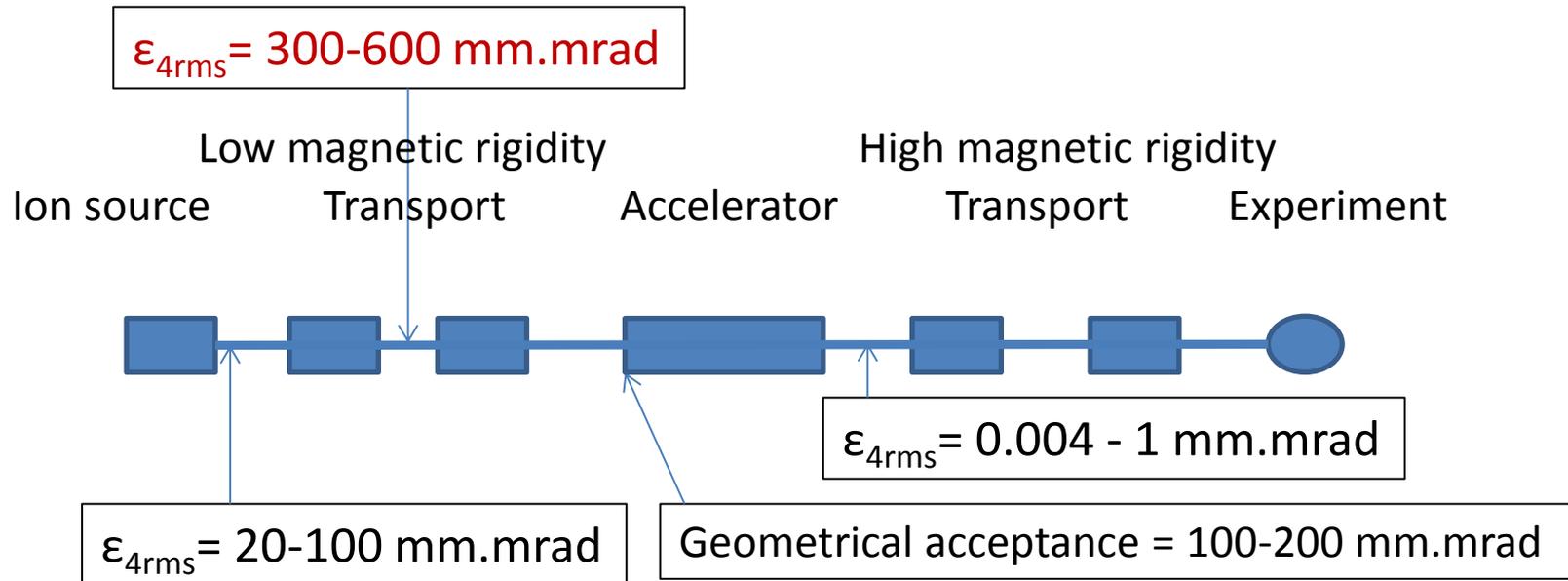
$$\epsilon_{4rms} = 20-100 \text{ mm.mrad}$$

Geometrical acceptance = 100-200 mm.mrad

Introduction



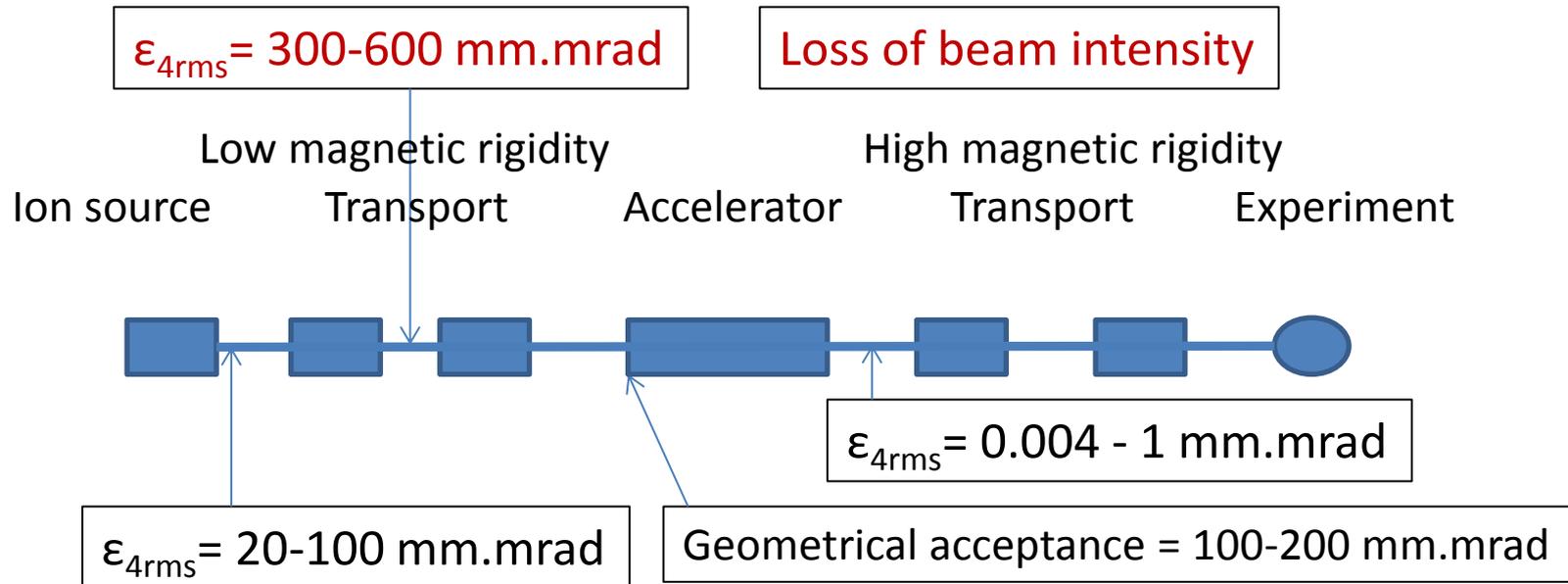
Accelerator Laboratories:



Introduction



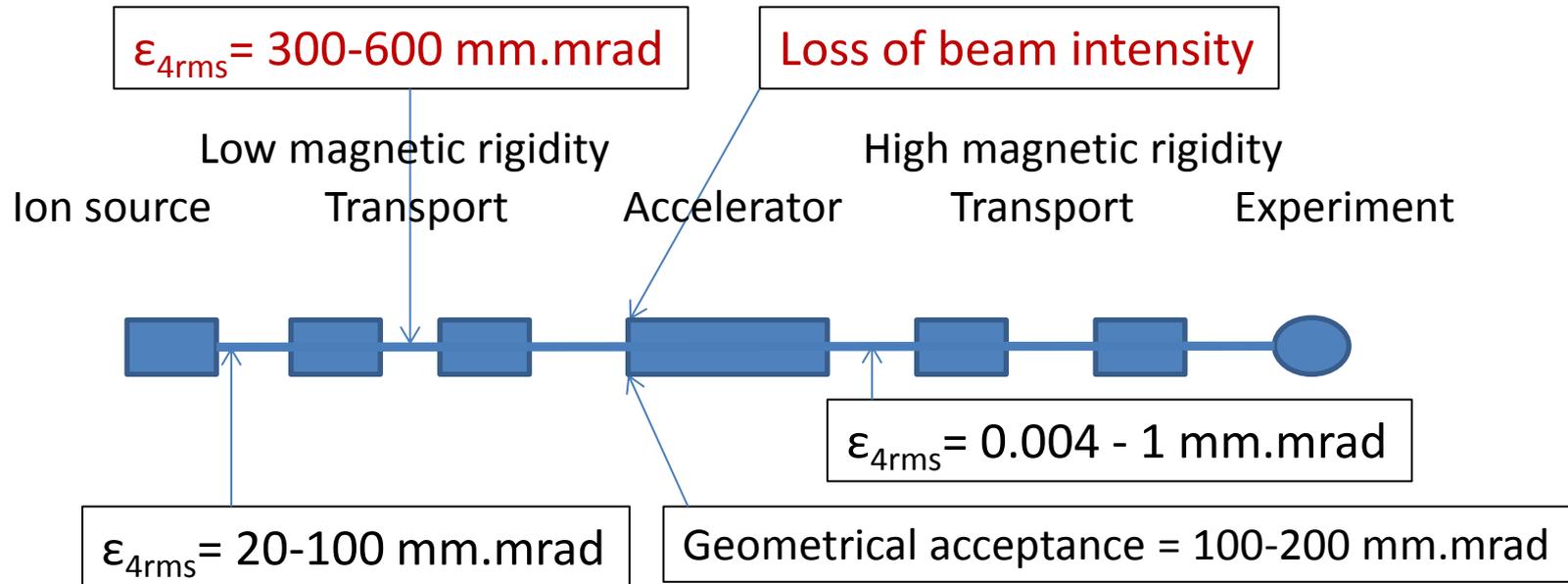
Accelerator Laboratories:



Introduction



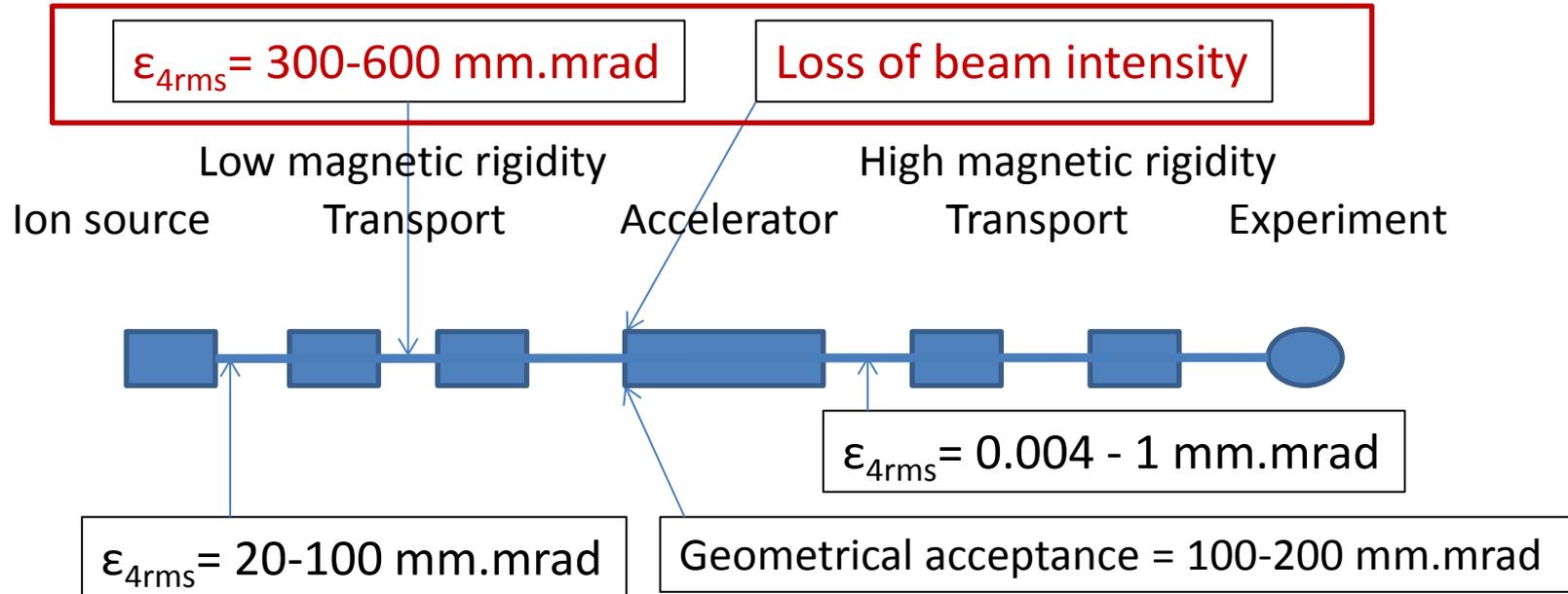
Accelerator Laboratories:



Introduction



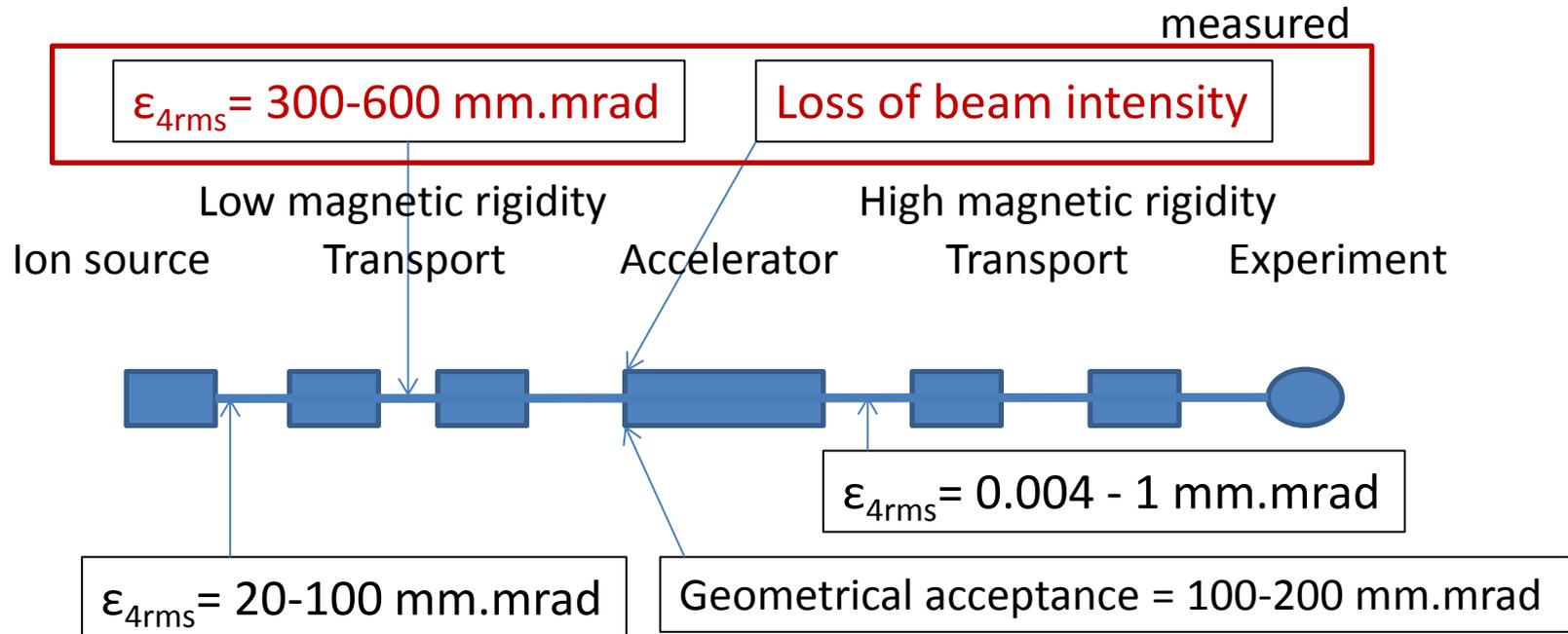
Accelerator Laboratories:



Introduction



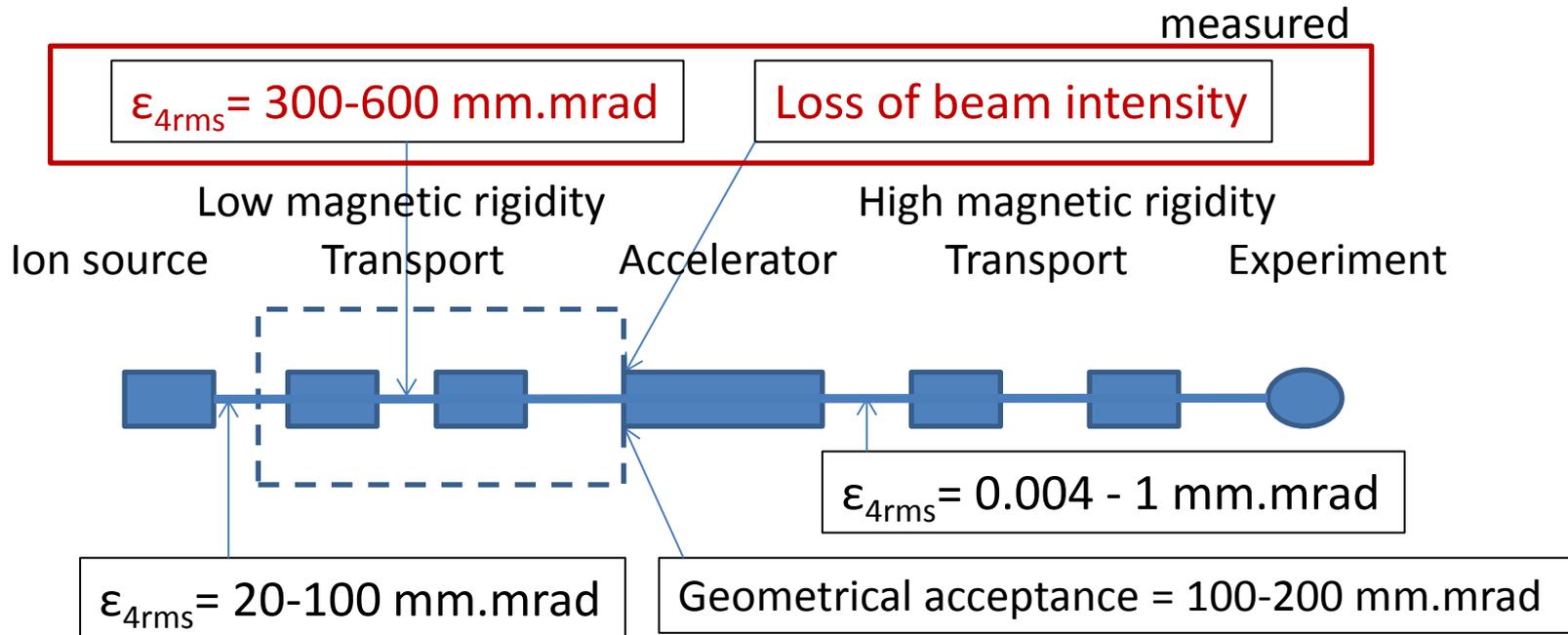
Accelerator Laboratories:



Introduction



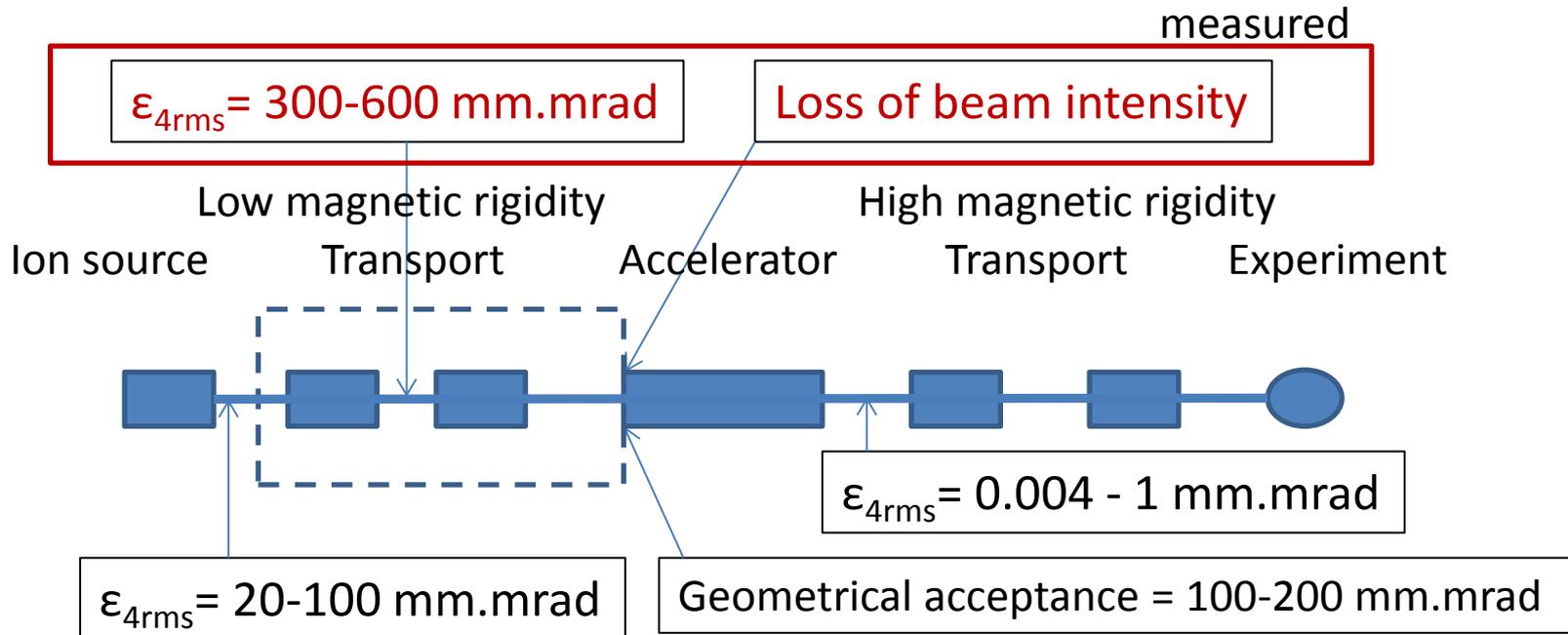
Accelerator Laboratories:



Introduction



Accelerator Laboratories:



Challenge: avoid emittance blowup due to:

1. lens aberrations
2. absence of space charge compensation

Research emittance growth

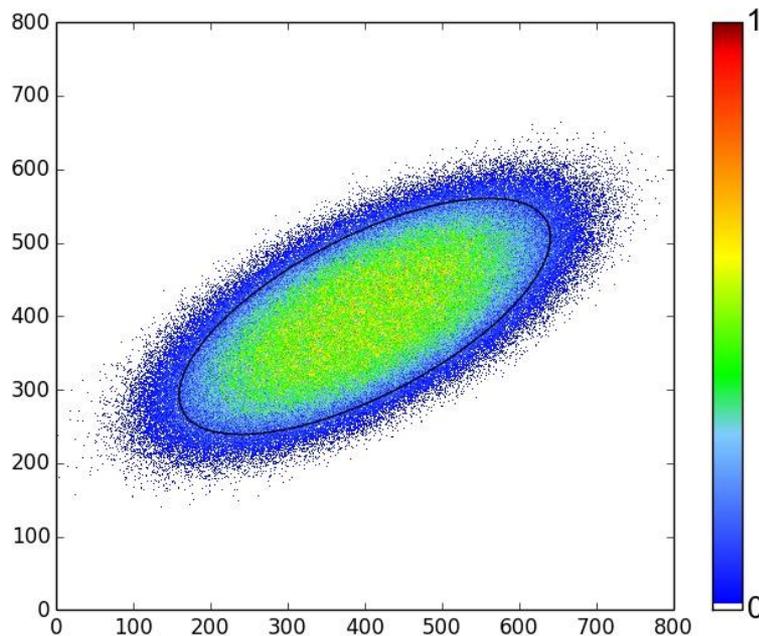
– Simulations

- Particle tracking codes, Raytrace, Track, GPT,
+ : any field configuration. Lorentz3D
- : slow (equation of motion is calculated for every track)
- Mapping codes: Transport, GIOS, COSY Infinity 9.1
+ : fast (equation of motion is already in the matrix)
- : fixed elements.

– Measurements

- Measurement of emittance
 - Slit grid, Allison scanner:
 - measurement in one plane, integrates over other planes
 - + proven technology
 - pepper pot emittance meter:
 - + measurement in two planes, cross correlations, slices emittances
 - Fixed grid

Gaussian distribution



$$\sigma_{11} = \iint (x_i - \langle x \rangle)^2 \rho(x, x') dx dx'$$

$$\sigma_{22} = \iint (x'_i - \langle x' \rangle)^2 \rho(x, x') dx dx'$$

$$\sigma_{12} = \iint (x_i - \langle x \rangle) (x'_i - \langle x' \rangle) \rho(x, x') dx dx'$$

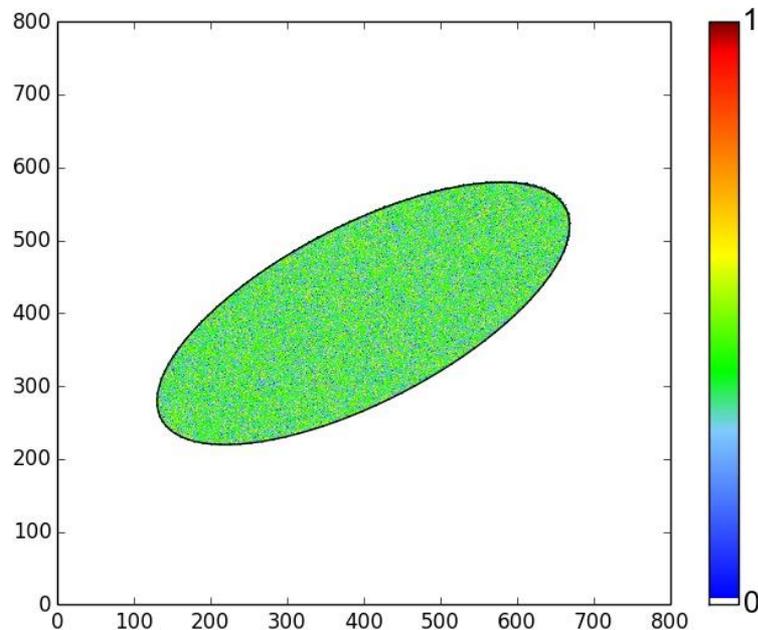
$$\varepsilon_{xx'-4rms} = 4 \cdot \sqrt{\sigma_{11}\sigma_{22} - \sigma_{12}^2} = \frac{A_{86\%}}{\pi}$$

$$\varepsilon_{xx'-4rms,n} = \varepsilon_{xx'-4rms} \cdot \beta \cdot \gamma$$

Emittance



Gaussian distribution



$$\sigma_{11} = \iint (x_i - \langle x \rangle)^2 \rho(x, x') dx dx'$$

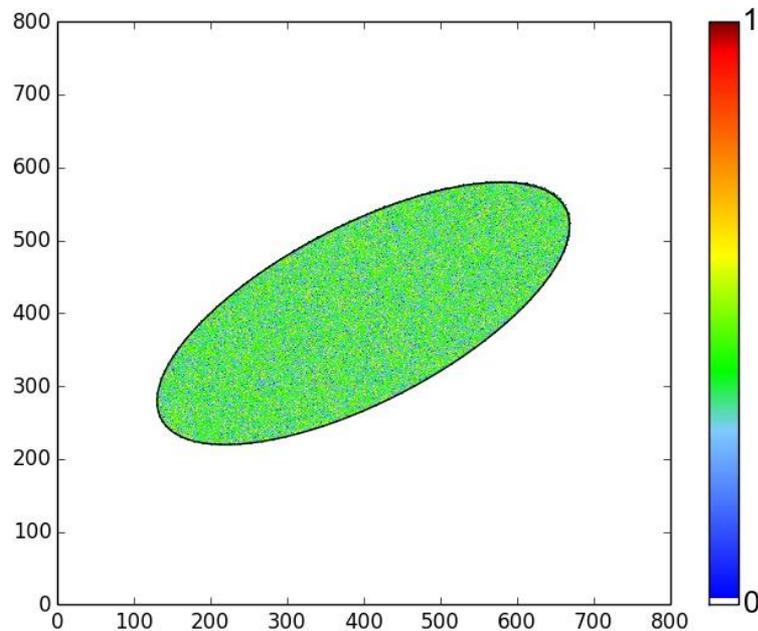
$$\sigma_{22} = \iint (x'_i - \langle x' \rangle)^2 \rho(x, x') dx dx'$$

$$\sigma_{12} = \iint (x_i - \langle x \rangle) (x'_i - \langle x' \rangle) \rho(x, x') dx dx'$$

$$\varepsilon_{xx'-4rms} = 4 \cdot \sqrt{\sigma_{11}\sigma_{22} - \sigma_{12}^2} = \frac{A_{86\%}}{\pi}$$

$$\varepsilon_{xx'-4rms,n} = \varepsilon_{xx'-4rms} \cdot \beta \cdot \gamma$$

Gaussian distribution



$$\sigma_{11} = \iint (x_i - \langle x \rangle)^2 \rho(x, x') dx dx'$$

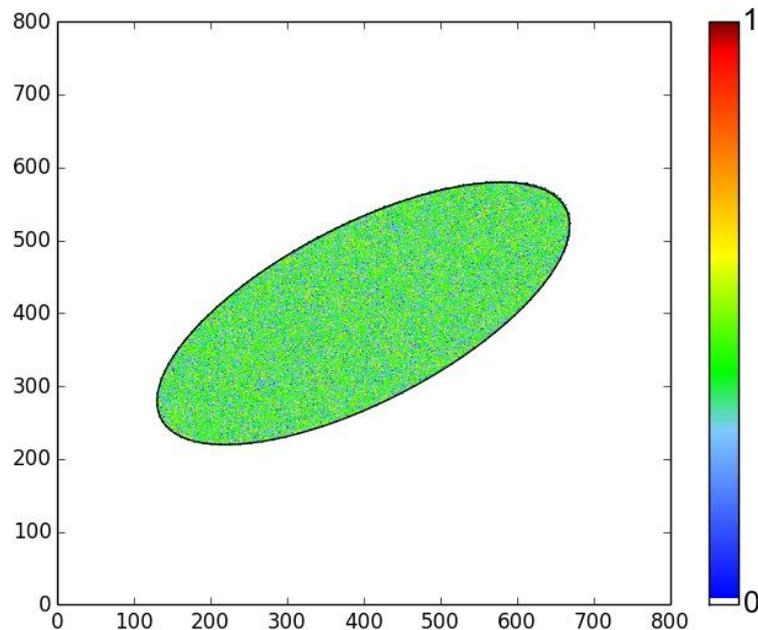
$$\sigma_{22} = \iint (x'_i - \langle x' \rangle)^2 \rho(x, x') dx dx'$$

$$\sigma_{12} = \iint (x_i - \langle x \rangle) (x'_i - \langle x' \rangle) \rho(x, x') dx dx'$$

$$\varepsilon_{xx'-4rms} = 4 \cdot \sqrt{\sigma_{11}\sigma_{22} - \sigma_{12}^2} = \frac{A_{86\%}}{\pi}$$

$$\varepsilon_{xx'-4rms,n} = \varepsilon_{xx'-4rms} \cdot \beta \cdot \gamma$$

Gaussian distribution



$$\sigma_{11} = \iint (x_i - \langle x \rangle)^2 \rho(x, x') dx dx'$$

$$\sigma_{22} = \iint (x'_i - \langle x' \rangle)^2 \rho(x, x') dx dx'$$

$$\sigma_{12} = \iint (x_i - \langle x \rangle) (x'_i - \langle x' \rangle) \rho(x, x') dx dx'$$

$$\varepsilon_{xx'-4rms} = 4 \cdot \sqrt{\sigma_{11}\sigma_{22} - \sigma_{12}^2} = \frac{A_{86\%}}{\pi}$$

$$\varepsilon_{xx'-4rms,n} = \varepsilon_{xx'-4rms} \cdot \beta \cdot \gamma$$

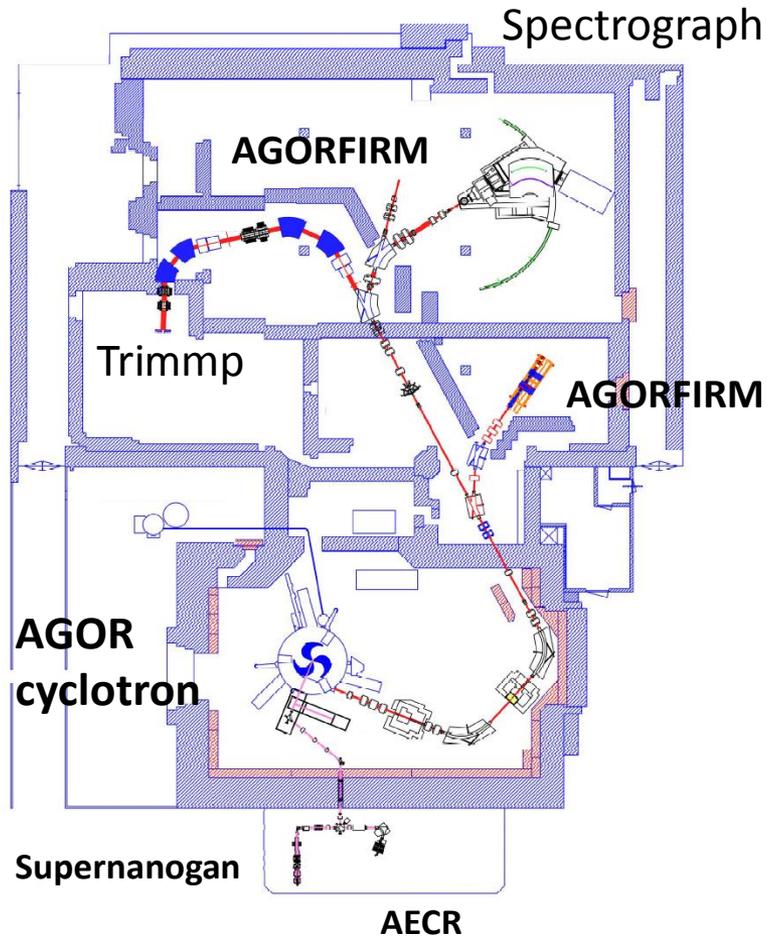
KVI-CART facility layout



university of
groningen

kvi - center for advanced
radiation technology

- Top view experimental hall



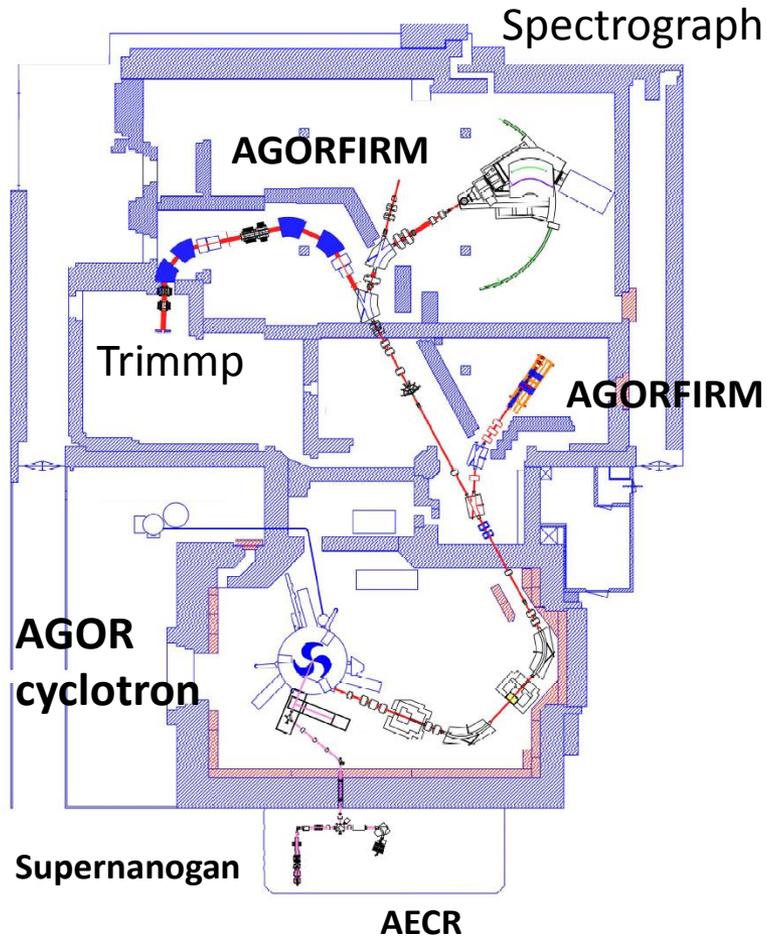
KVI-CART facility layout



university of
groningen

kvi - center for advanced
radiation technology

- Top view experimental hall



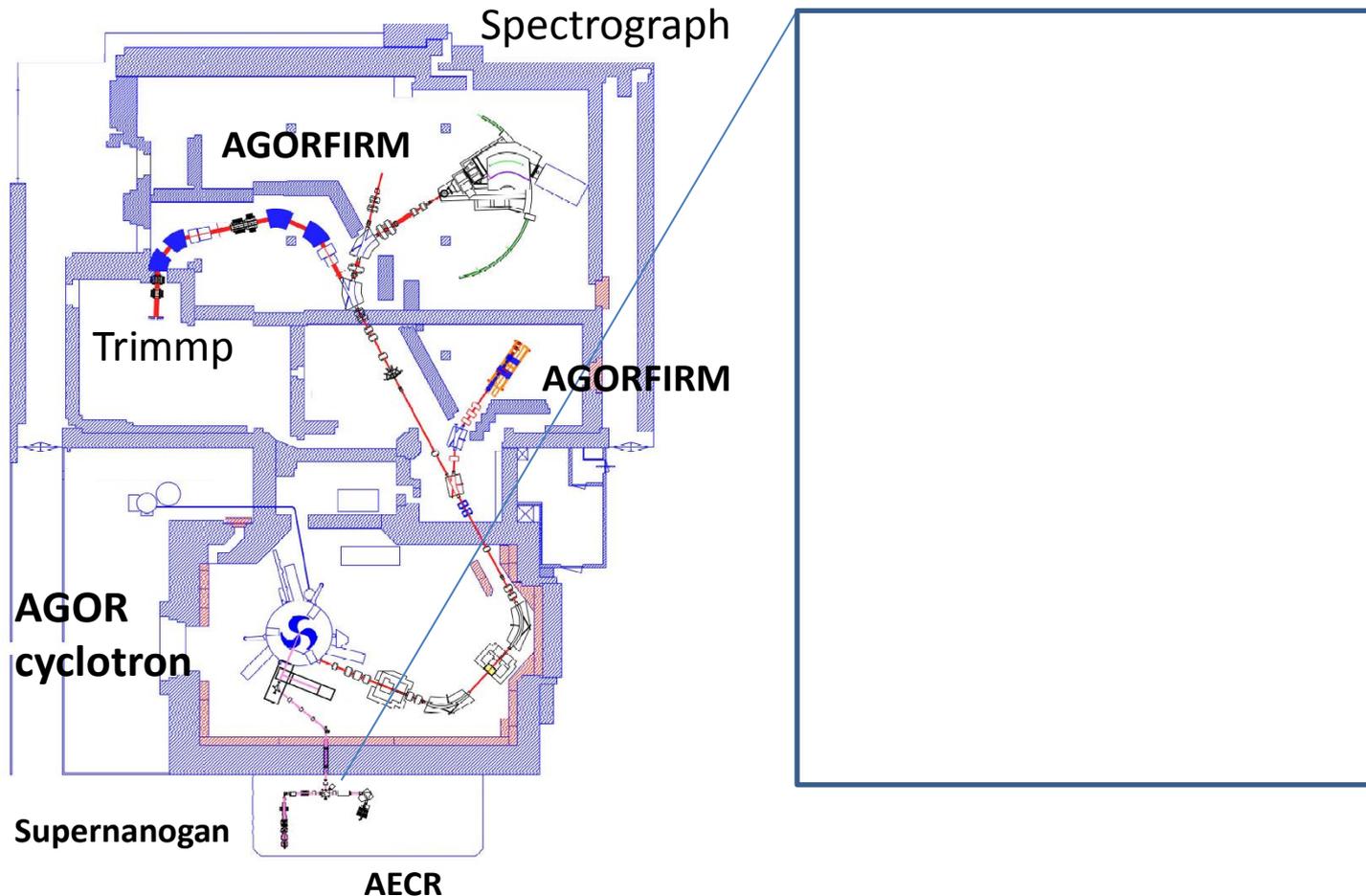
KVI-CART facility layout



university of
groningen

kvi - center for advanced
radiation technology

- Top view experimental hall



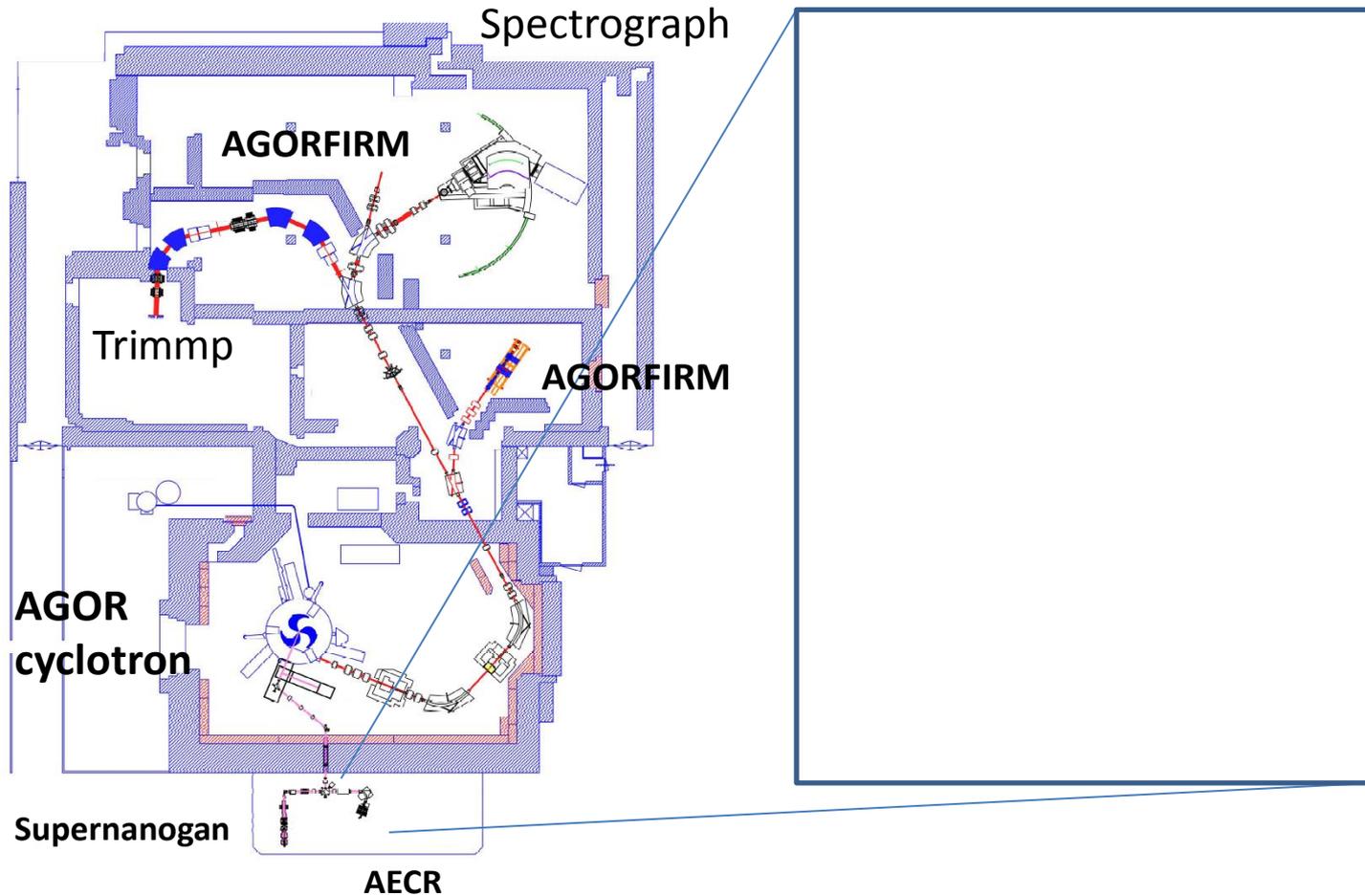
KVI-CART facility layout



university of
groningen

kvi - center for advanced
radiation technology

- Top view experimental hall



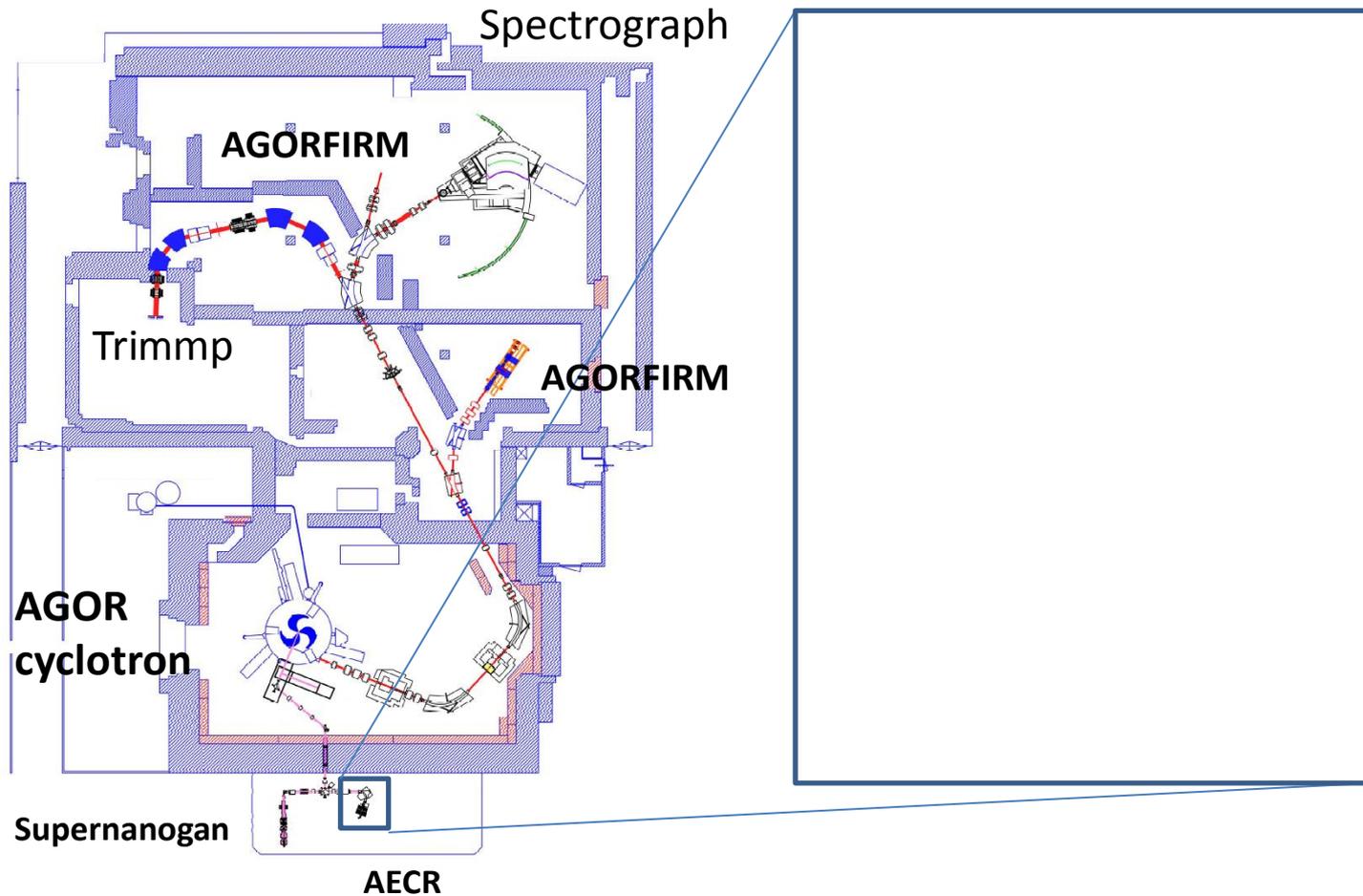
KVI-CART facility layout



university of
 groningen

kvi - center for advanced
 radiation technology

- Top view experimental hall



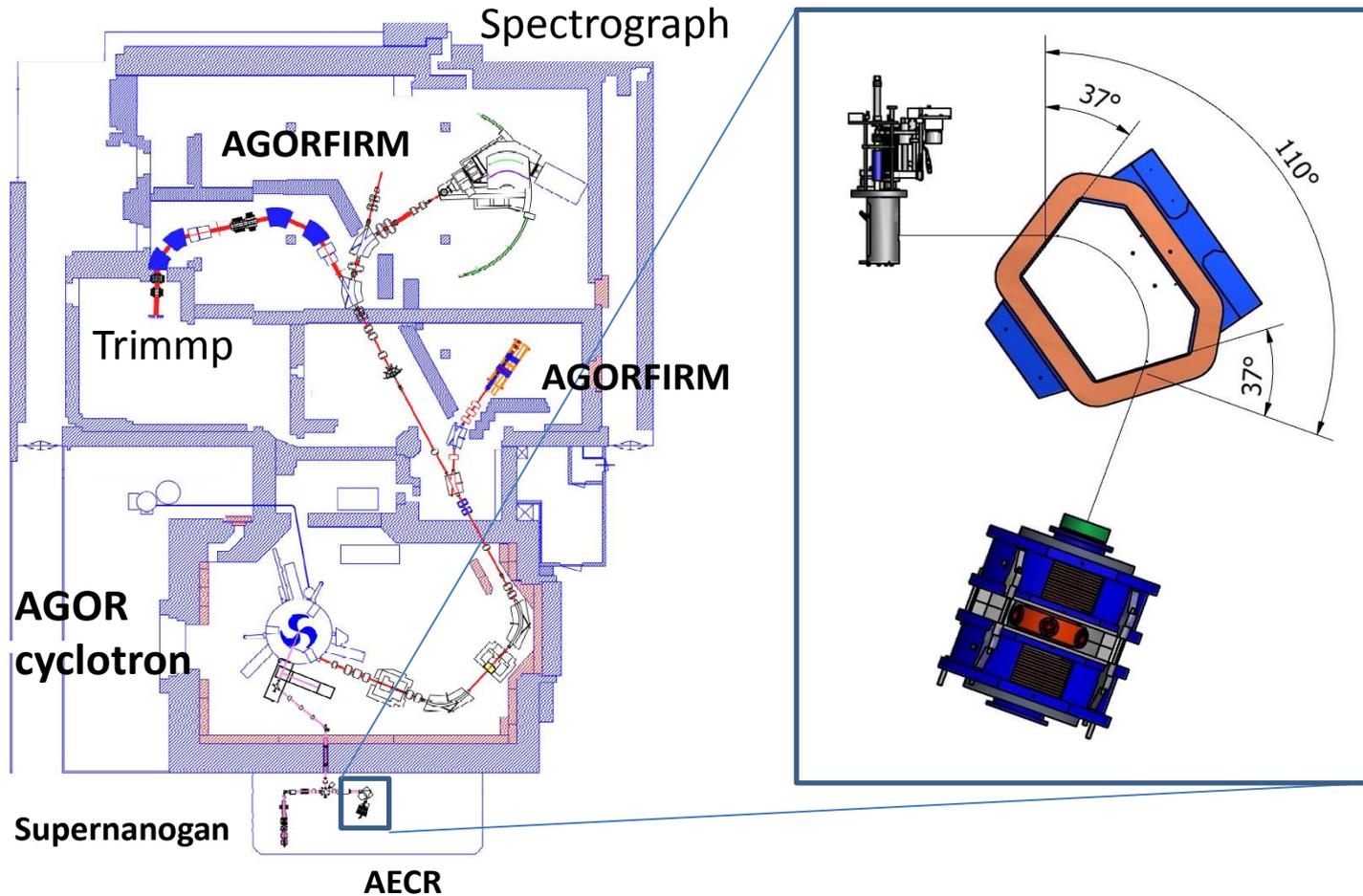
KVI-CART facility layout



university of
 groningen

kvi - center for advanced
 radiation technology

- Top view experimental hall



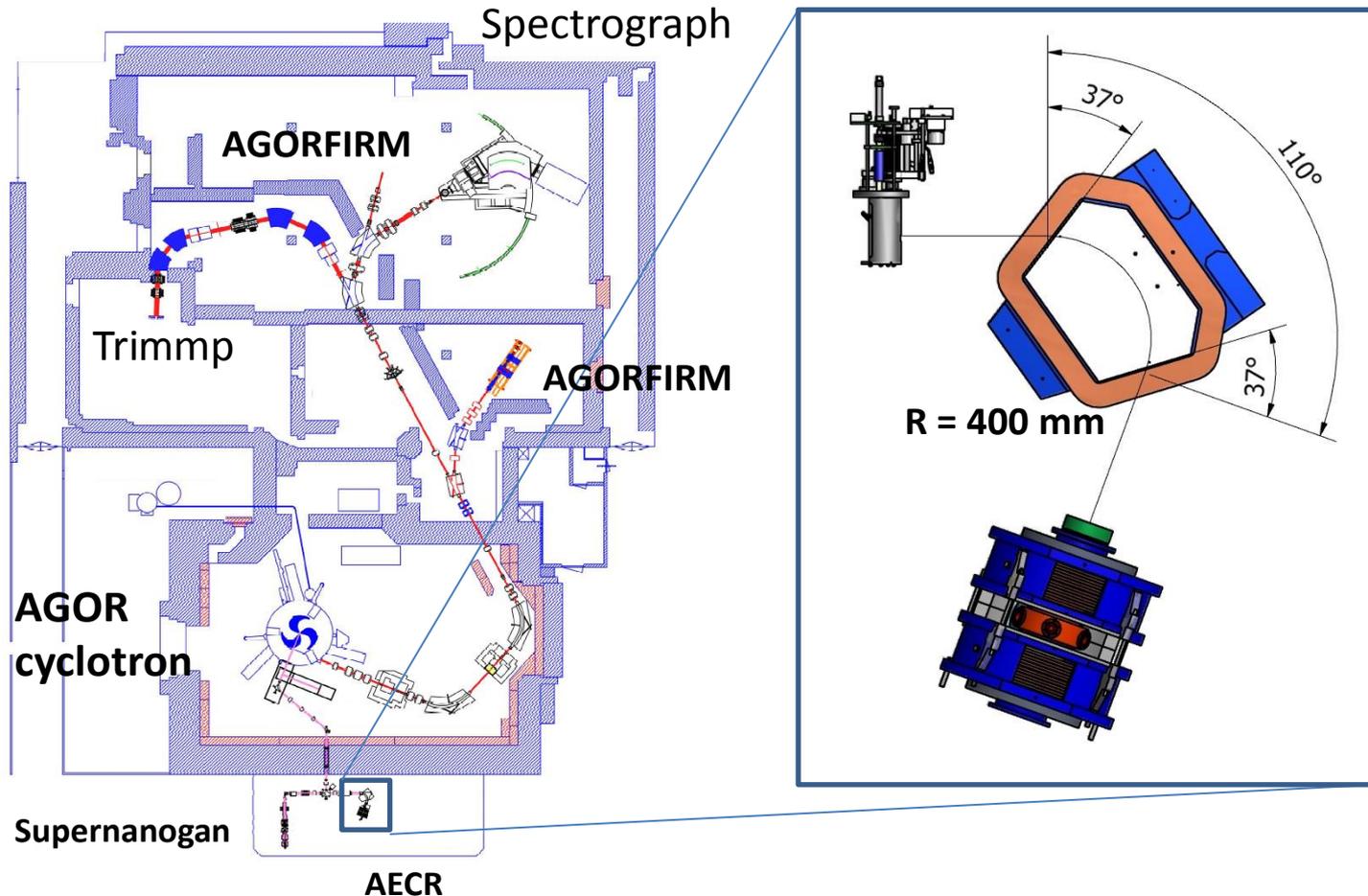
KVI-CART facility layout



university of
 groningen

kvi - center for advanced
 radiation technology

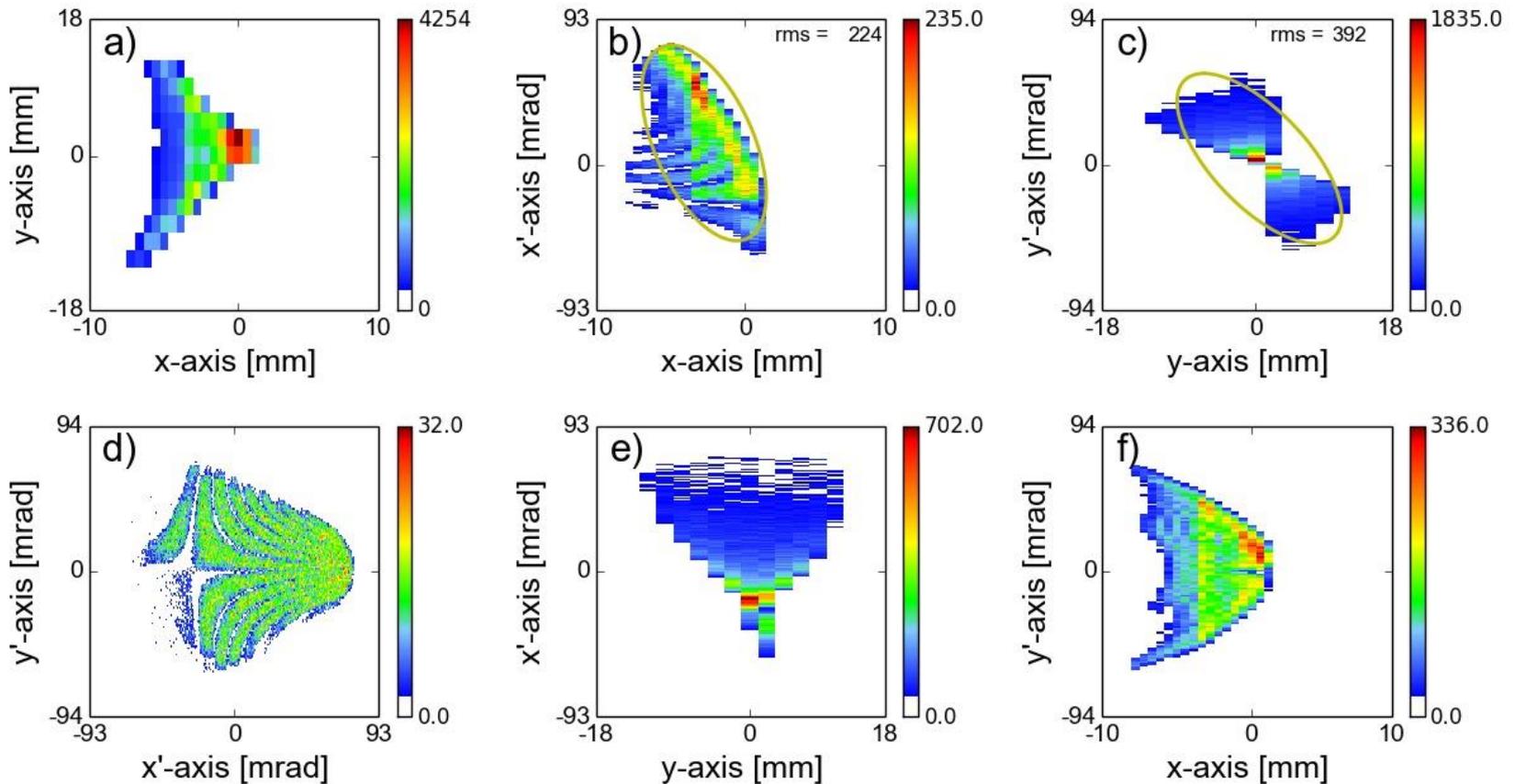
- Top view experimental hall



Measured and simulated



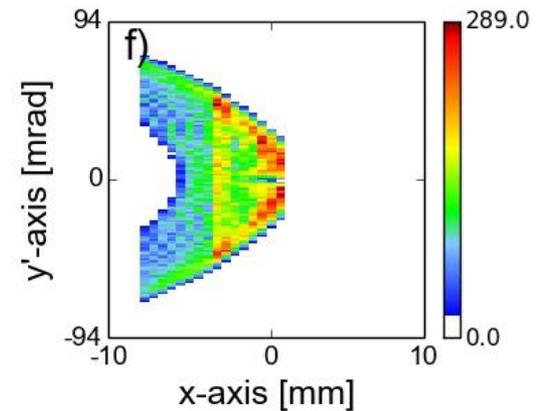
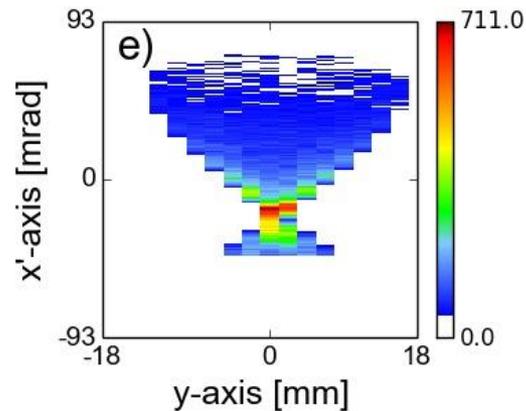
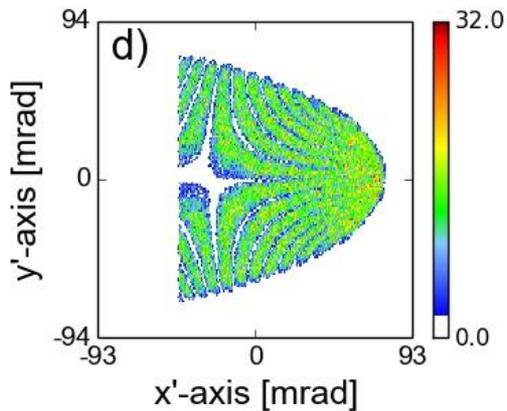
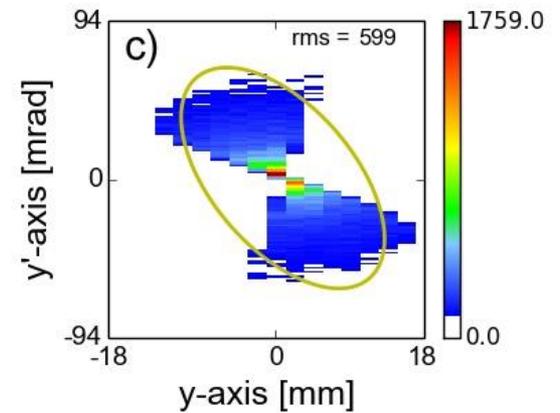
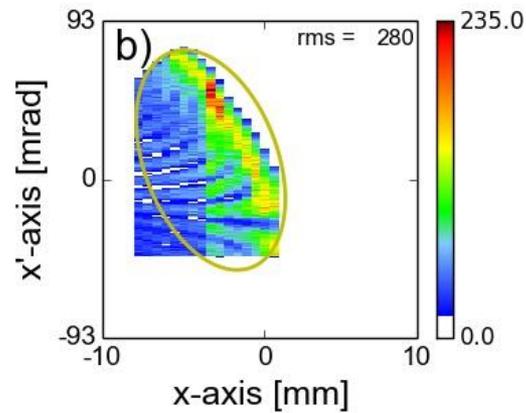
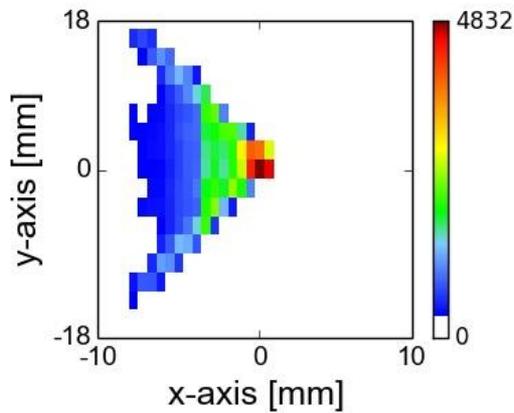
- Simulated phase-space projections of a 25 kV He¹⁺ validated by measurements



Measured and simulated



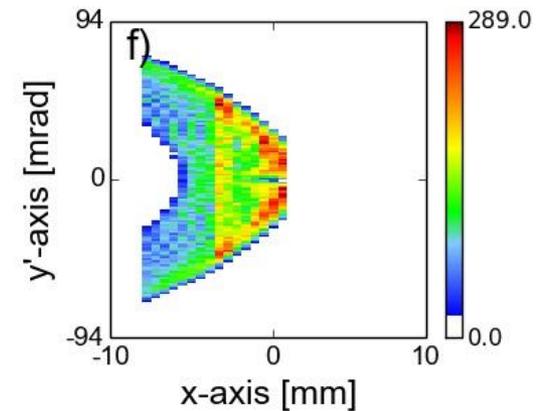
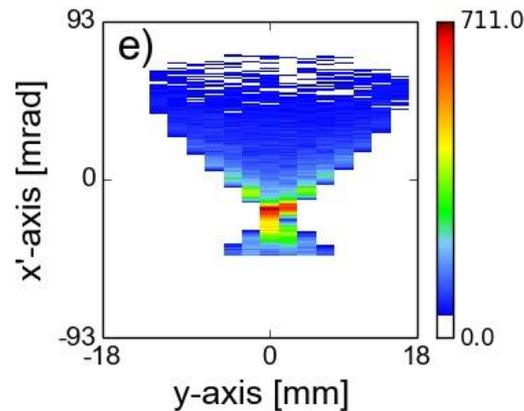
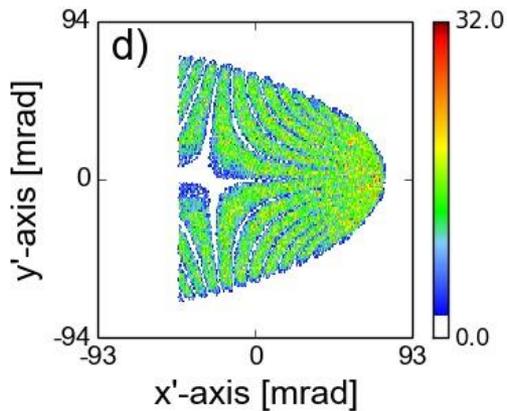
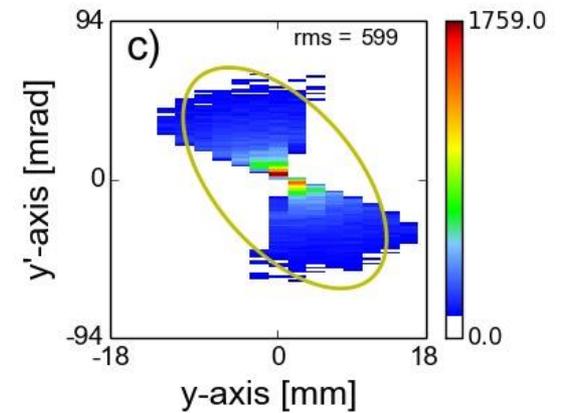
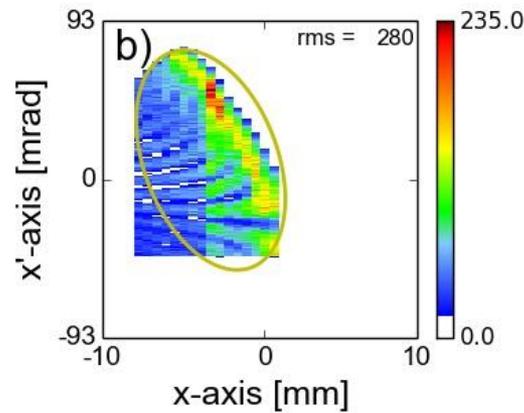
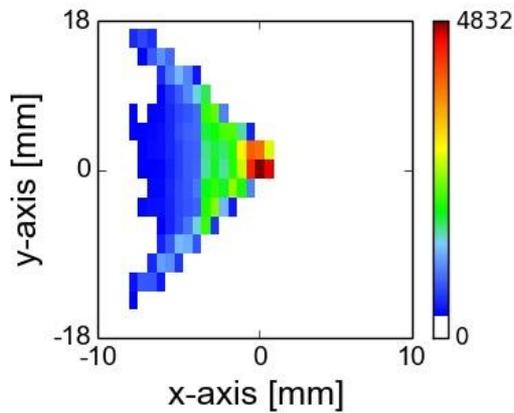
- Simulated phase-space projections of a 25 kV He¹⁺ validated by measurements



Measured and simulated



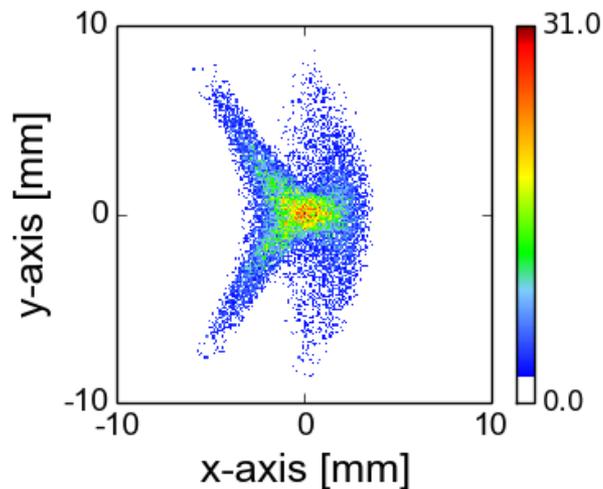
- Simulated phase-space projections of a 25 kV He¹⁺ valid at the electron source



- Conclusion:

- Higher order components ($y|x'y'$), ($x|y'y'$) and ($x|x'x'$) identified
- Strengths : 5.3, - 2.4 and -0.9 respectively.

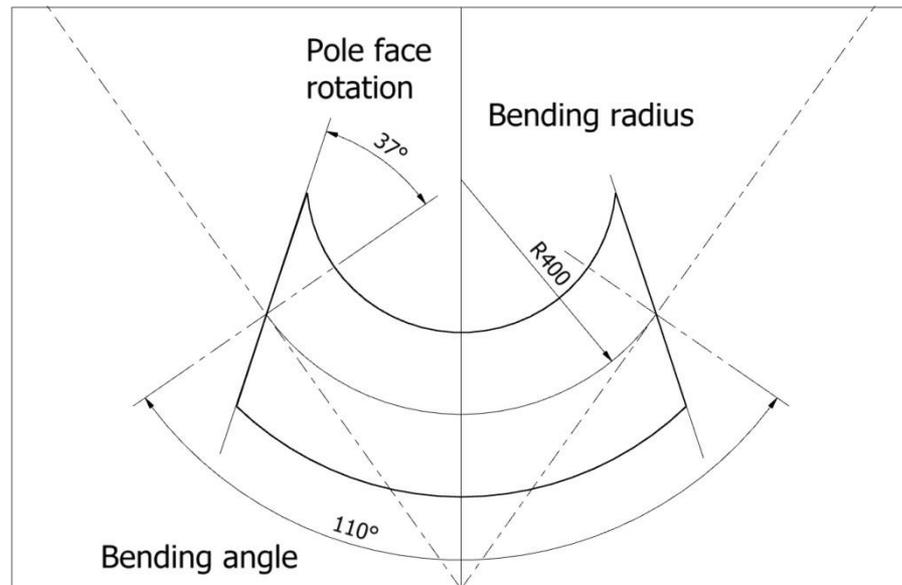
- Ion displacement in image plane due to aberrations are 26, 12 and 5 times larger than first order imaging. Image = aberration



25 kV He¹⁺ with phase-space cutoffs

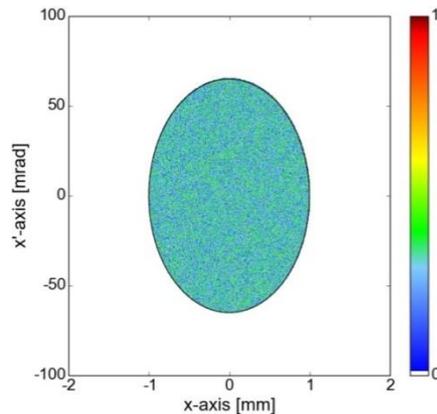


- How to fix the aberrations
- Method to calculate the emittance growth
- Apply this method to:
 - Add sextupoles
 - sextupoles
 - Add field lenses
 - Solenoid
 - Einzel lens

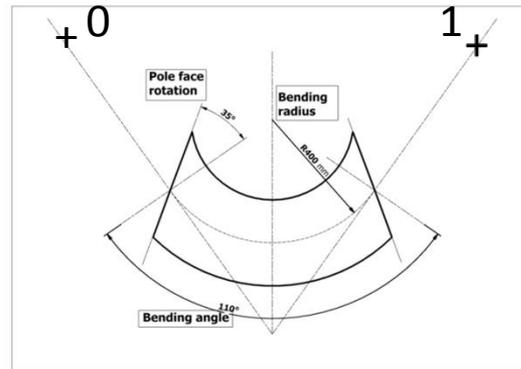


Method to calculate the 4-rms emittance growth

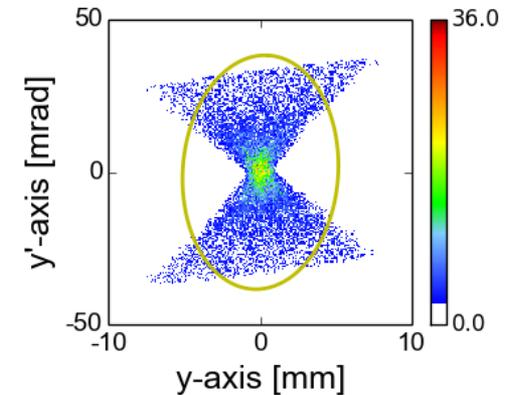
X_0



$X_1 = M^{(k)} \cdot X_0$



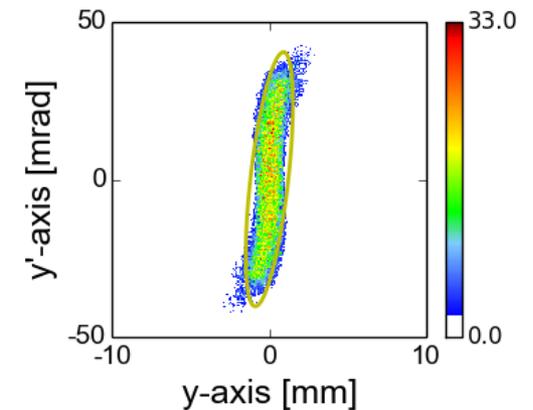
X_1



4rms = 65 mm.mrad

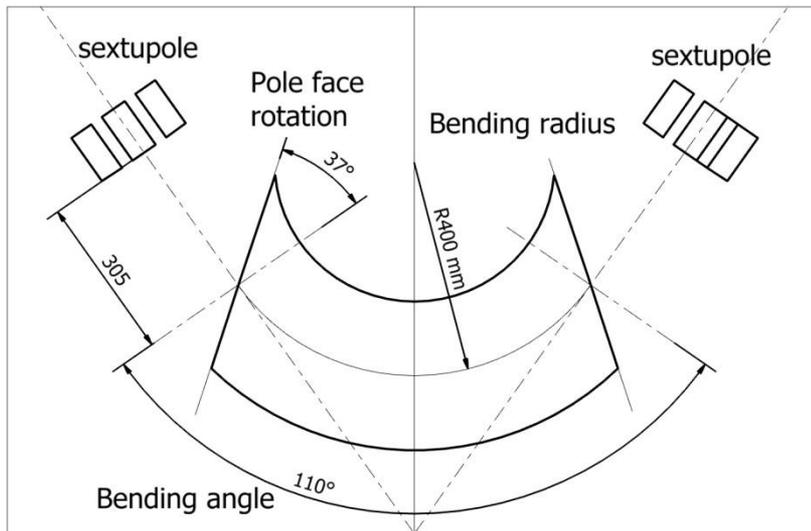
Area = 65.p mm.mrad

No difference with or without ion
 distribution in extraction aperture



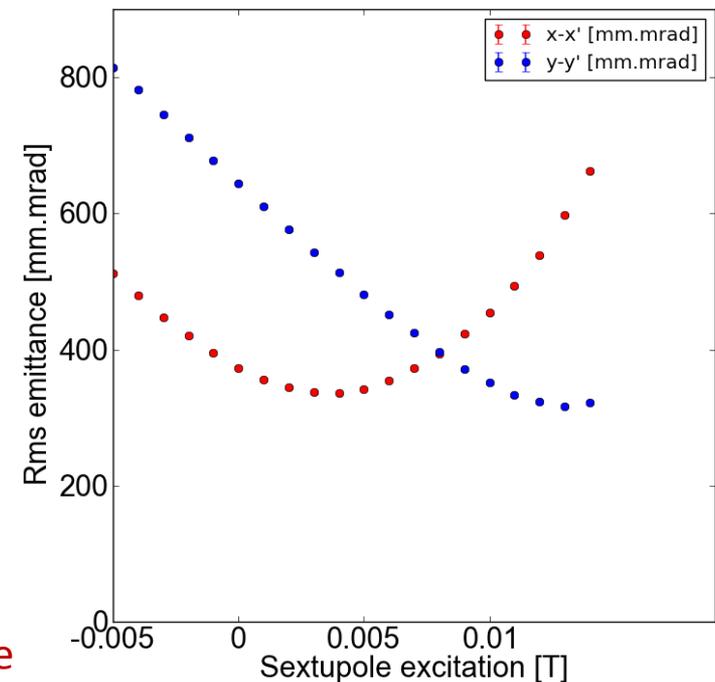
Dipole with an additional two Sextupoles

- Top view analyzing magnet



4RMS emittance 21 H¹⁺

as function sextupole excitation



$(y|x'y')$ $(x|y'y')$ $(x|x'x')$

5.3 -2.4 -0.9

-5.3 +2.7 -2.7

0 +0.3 -3.6

aberrations dipole

compensation sextupoles 0.013T

dipole corrected with sextupoles

- Compensation by sextupoles and small pole face adjustment

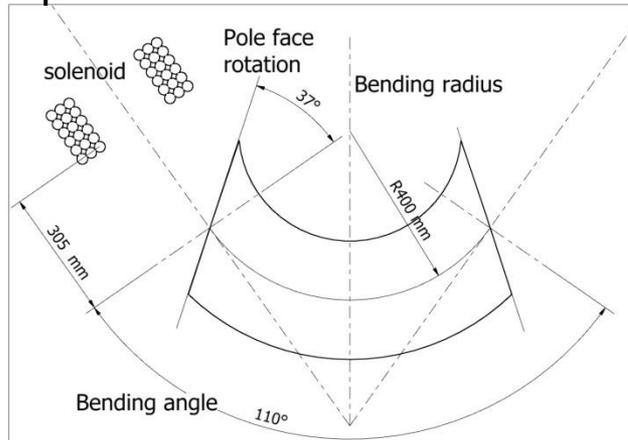
$\Theta_1 = x_1$	%	$\Theta_1 = x'_1$	%	$\Theta_1 = y_1$	%	$\Theta_1 = y'_1$	%	ID coeff
1.01E+00	100	2.19E+00	3					(θx)
-3.74E-08	0	9.94E-01	100					$(\theta x')$
				-1.01	100	-1.26	2	(θy)
				-3.36E-10	0	-0.99	100	$(\theta y')$
-3.011	1226							$(\theta x'^2)$
-15.615	407							$(\theta x'^3)$
36.2	944							$(\theta x'y'^2)$
				-36.3	943			$(\theta x'^2y')$
				-34.4	893			$(\theta y'^3)$
-173	289							$(\theta x'^2y'^2)$
-155	260							$(\theta y'^4)$
				119	197			$(\theta x'^3y')$
				629	1044			$(\theta x'y'^3)$
1857	198							$(\theta x'y'^4)$
				-3191	339			$(\theta x'^2y'^3)$
				-1669	177			$(\theta y'^5)$

Conclusion:

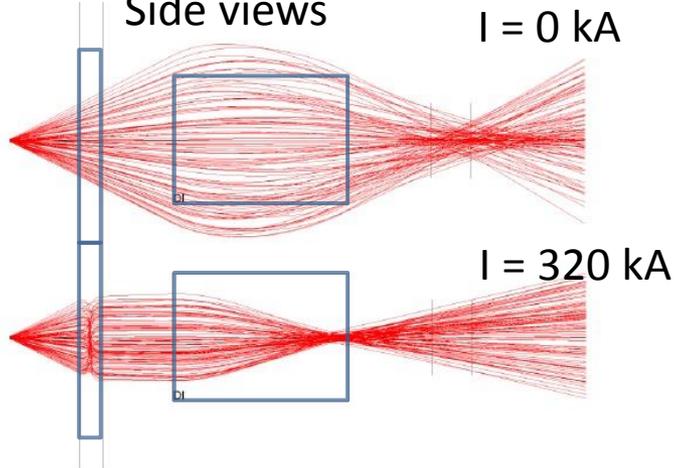
1. Yes, second order is partially compensated. However large higher order terms.

Dipole with an additional solenoid

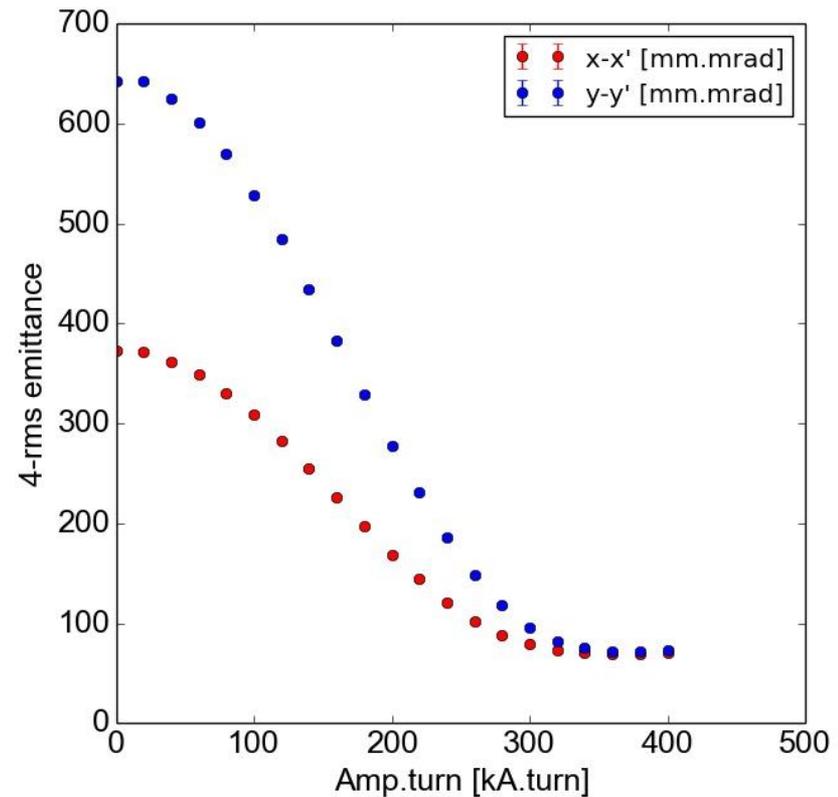
- Top view



Side views

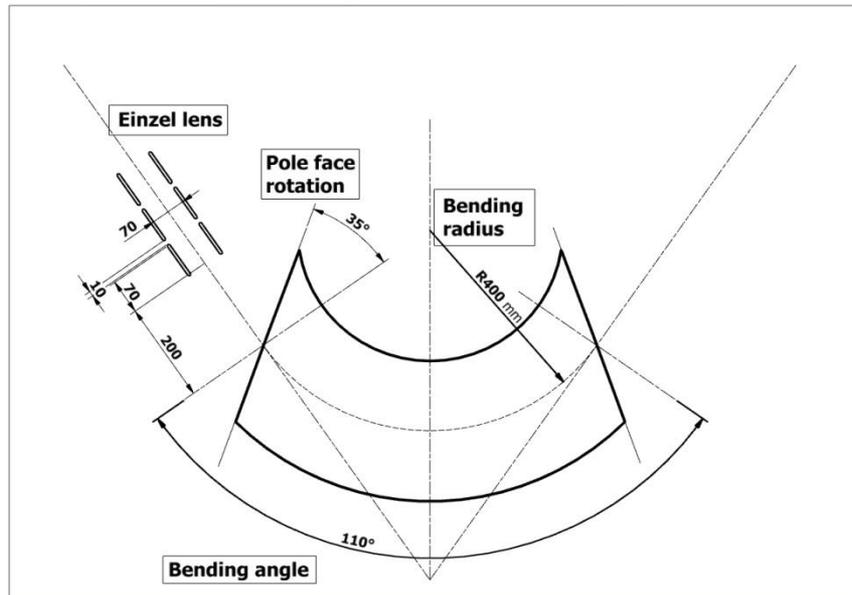


21 kV H¹⁺



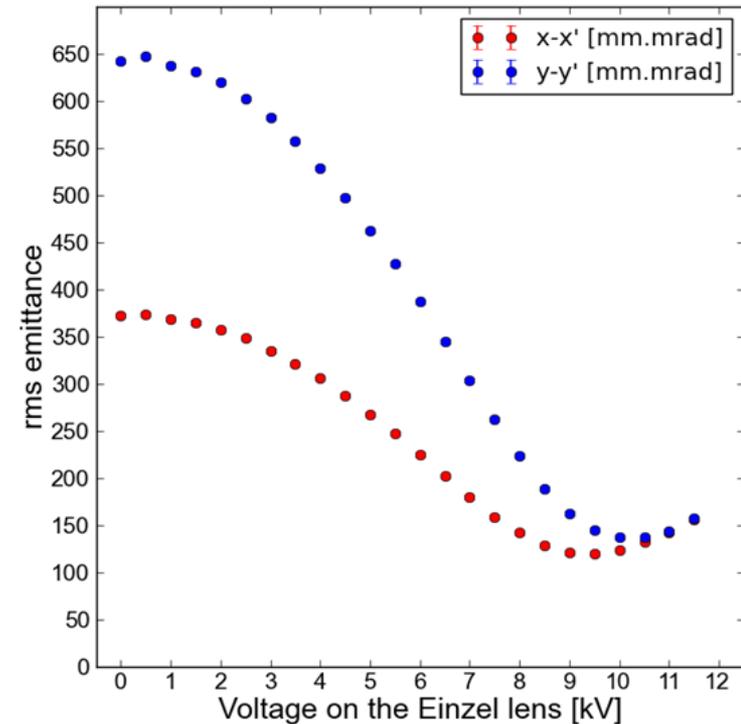
Dipole with additional einzel-lens

- Top view analyzing magnet



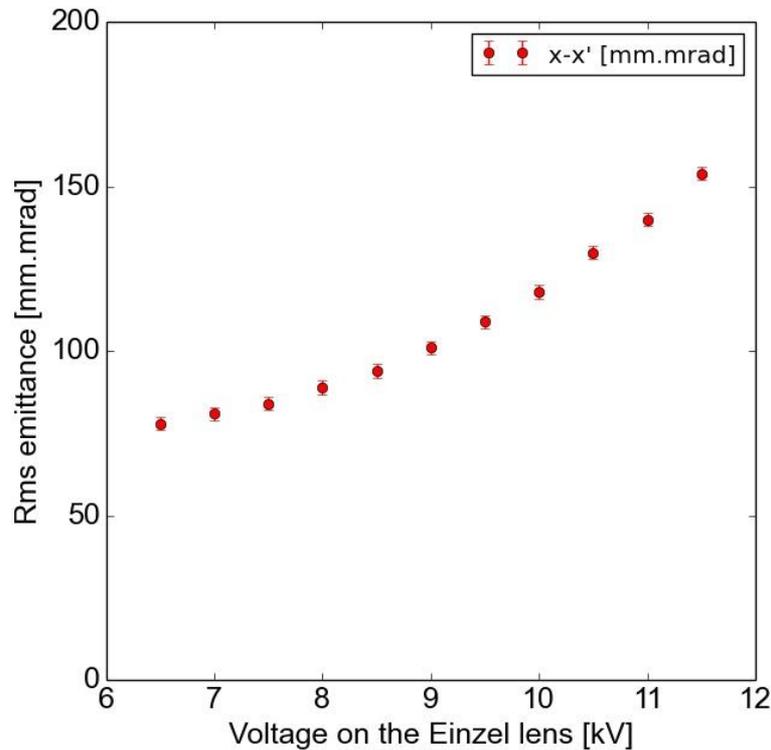
4RMS emittance 21 kV H^{1+}

as a function of the Einzel lens potential

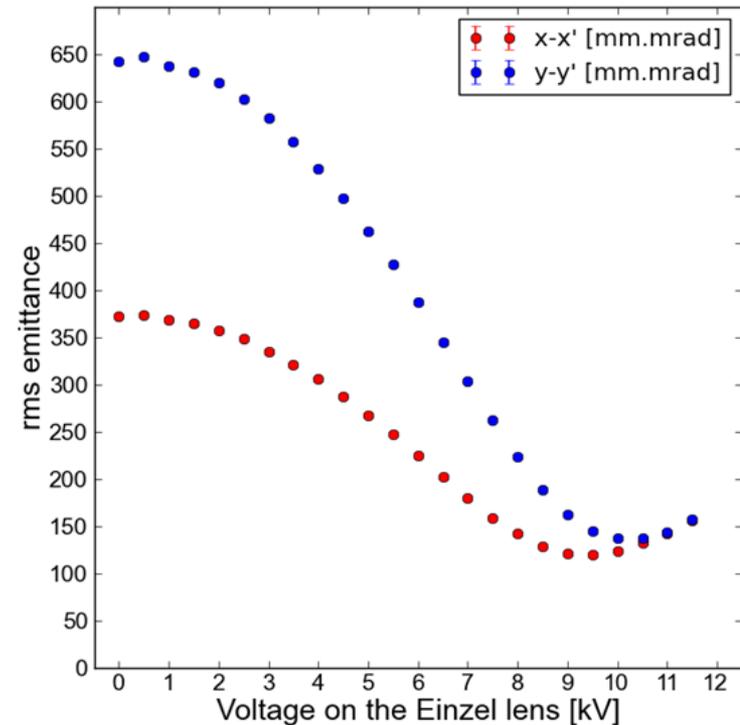


Detail : In the image plane of the dipole remnant 4-rms emittance generated by the einzel lens.

4-rms emittance growth due to einzel lens , 21 kV H¹⁺



4-rms emittance in image plane dipole of a 21 kV H¹⁺ beam



Conclusions:

- 1) Solenoid option is the best option. However 500 kA.Turn is difficult to integrate in existing setup.
- 2) Einzel lens reduces the emittance growth roughly with factor of 3 in both planes.
- 3) Diameter of the Einzel lens should be larger than 70 mm diameter.
- 4) Design strategy for a low energy beam-lines to accept beams with large divergence:
 - 1) First, reduce the fringe fields as much as possible and included additional correction.
 - 2) Secondly, calculate which coefficients causes the aberrations and change the phase-space upstream such that the effect of fringe fields on the beam phase-space is minimized.

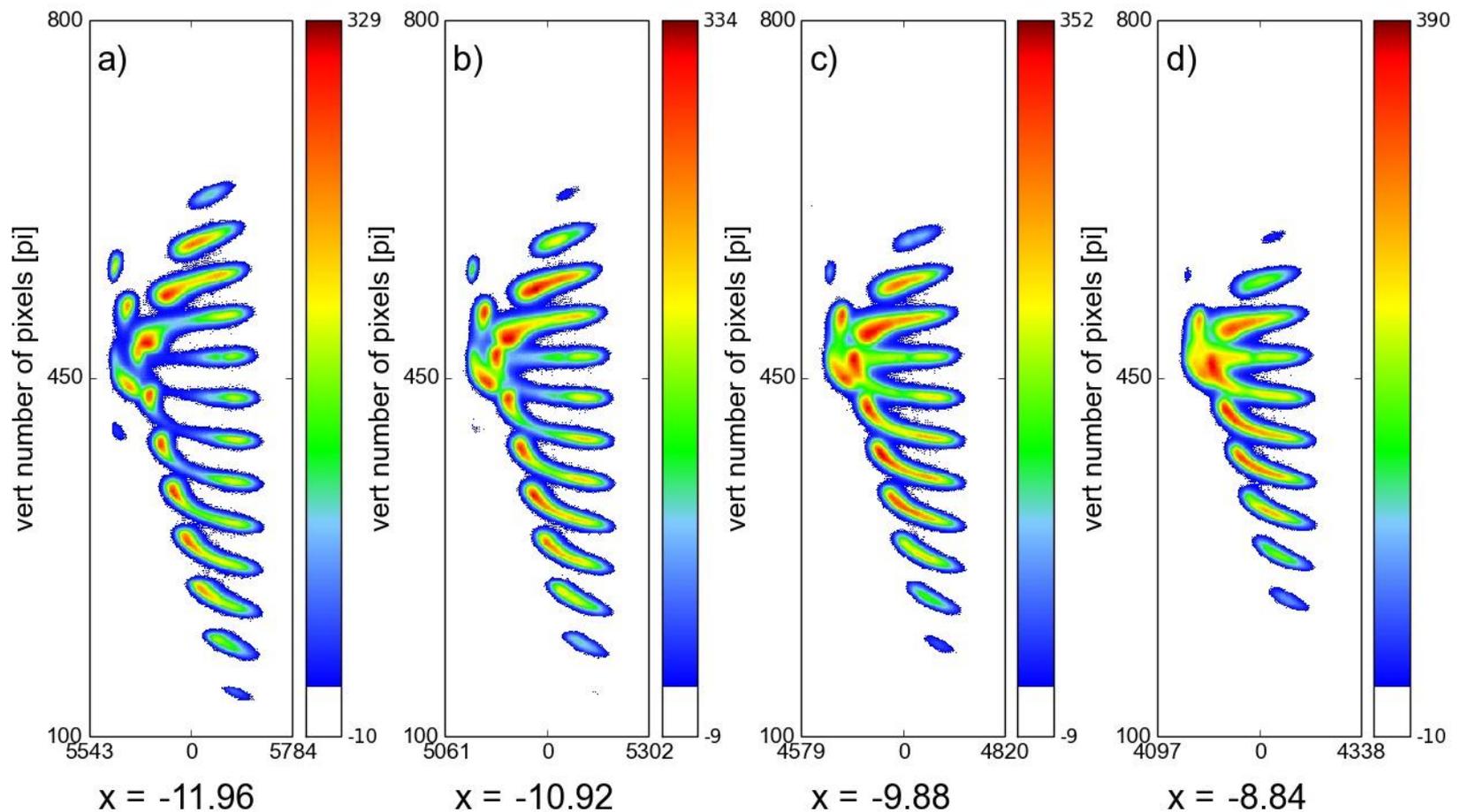


university of
 groningen

kvi - center for advanced
 radiation technology

- Thank you for your attention

- Measurements 25 kV He¹⁺ beam

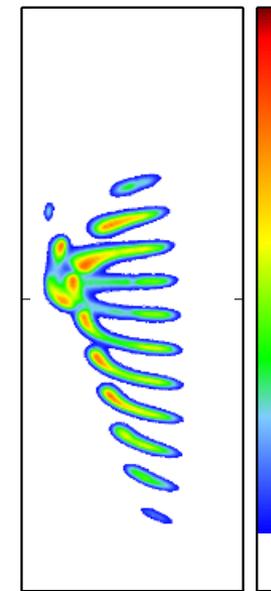
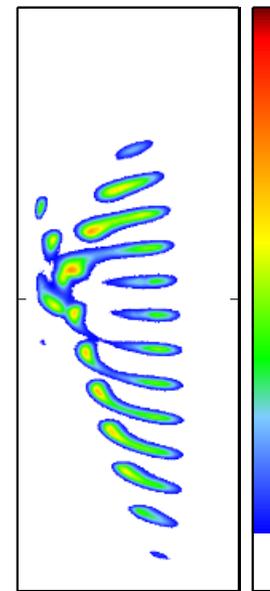
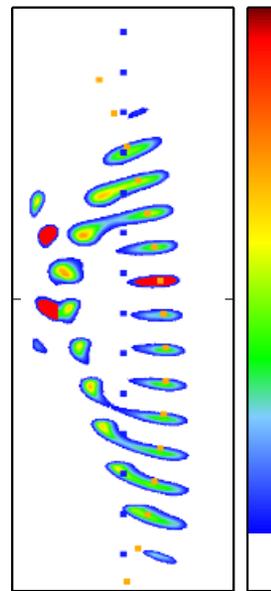
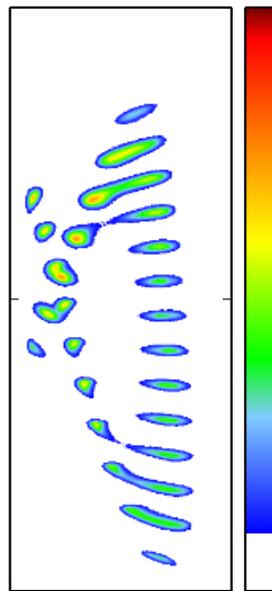


Measured



- Measurements 25 kV He¹⁺ beam

800 329 800 334 800 352 800 390



100 5543 0 5784 -10

x = -11.96

100 5061 0 5302 -9

x = -10.92

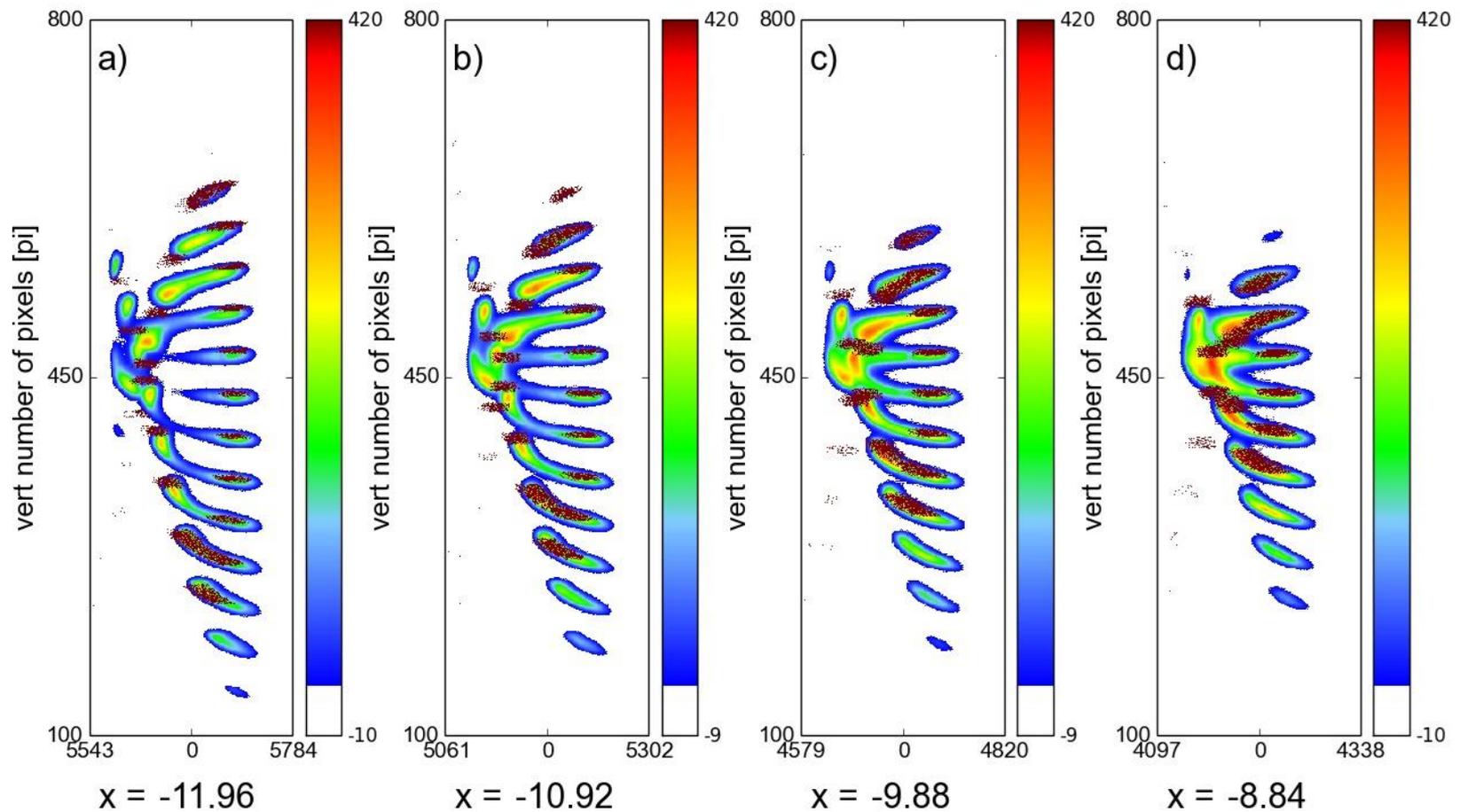
100 4579 0 4820 -9

x = -9.88

100 4097 0 4338 -10

x = -8.84

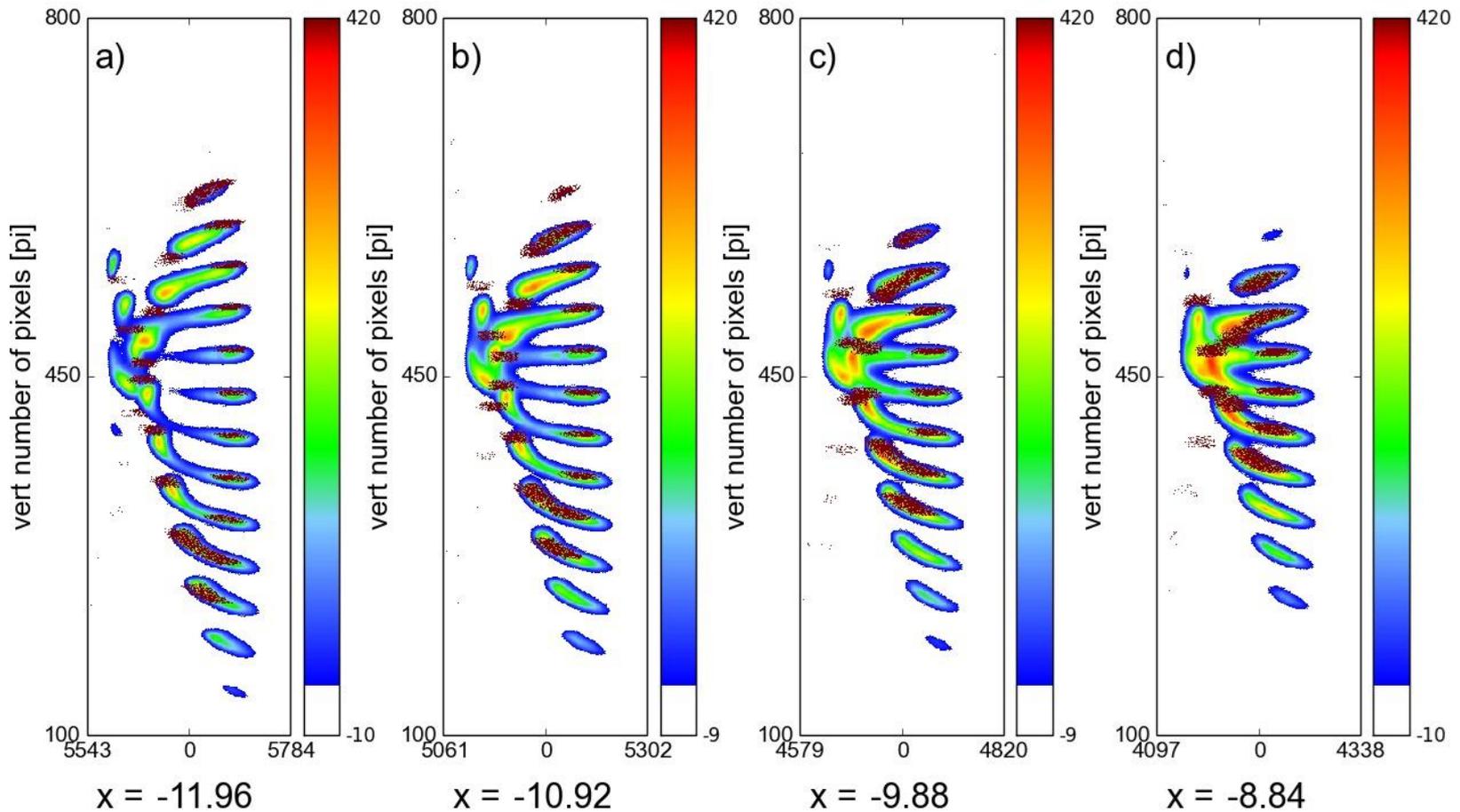
- Measurements 25 kV He¹⁺ beam



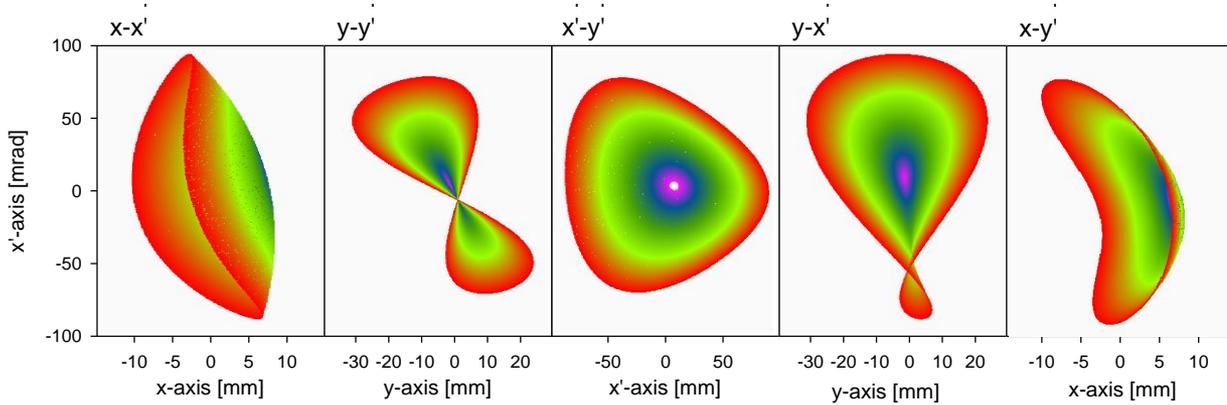
Measured



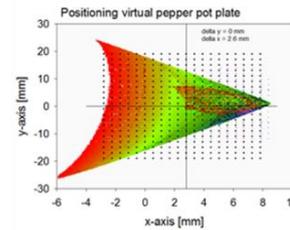
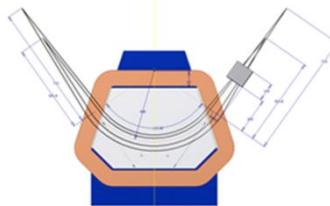
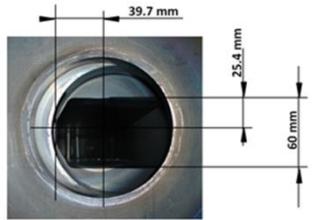
- Measurements compared with simulations of a 25 kV He¹⁺ beam



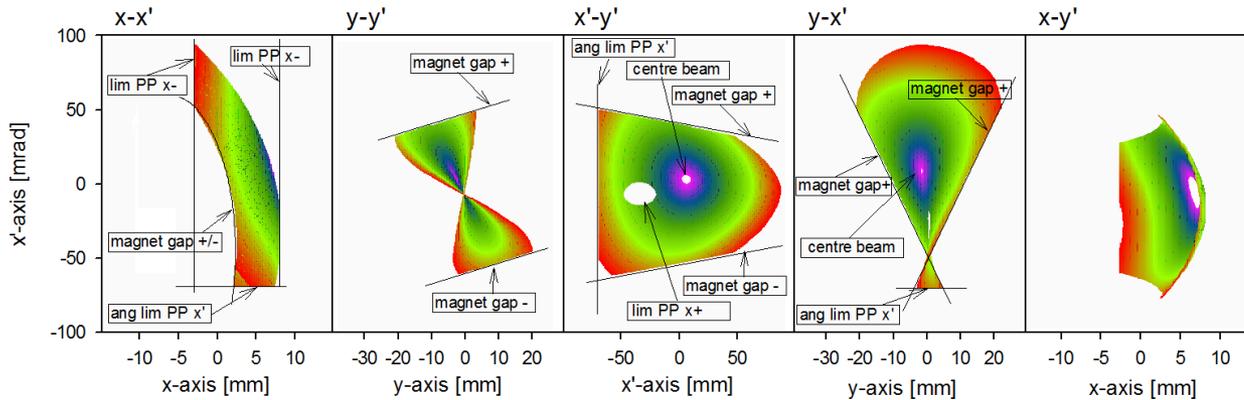
Simulated influence of limiters on projections



Complete beam



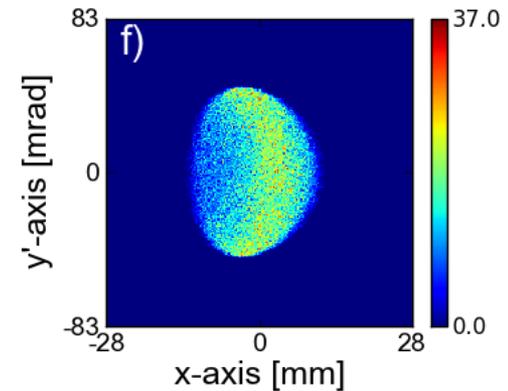
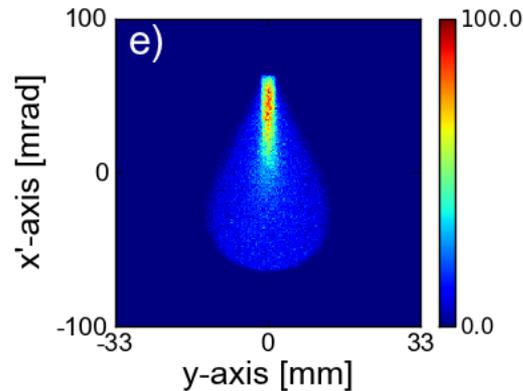
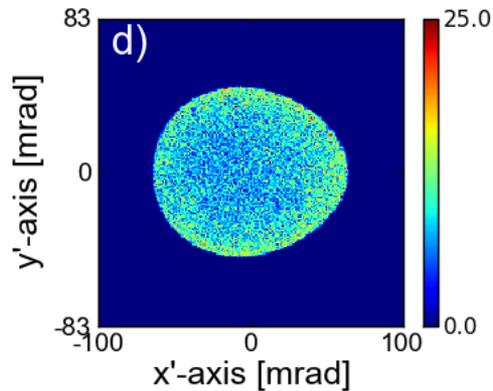
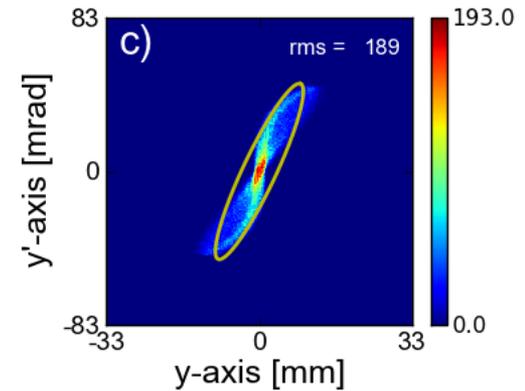
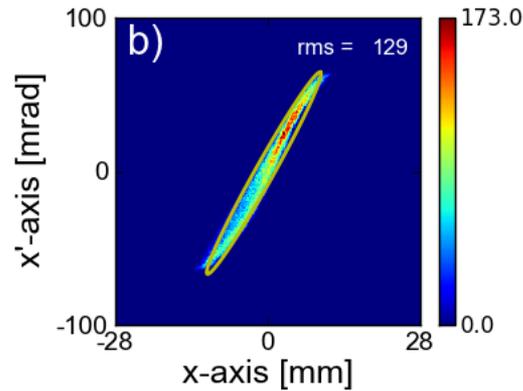
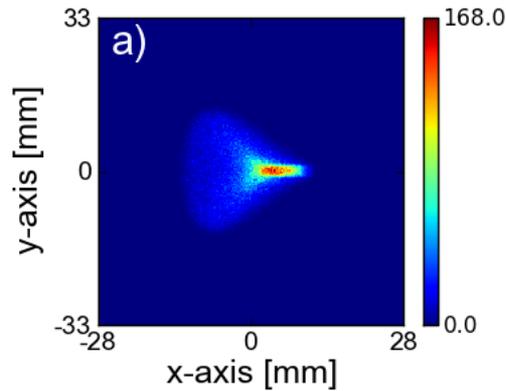
The limitations



Effects on
 projections

Result in phase-space of the Einzel lens

('Fifth order calculation: Drift (0.3175) - Einzel (0.075) - Drift (0.3175) - Dipole - Drift (0.534) - Image plane', '8.5')

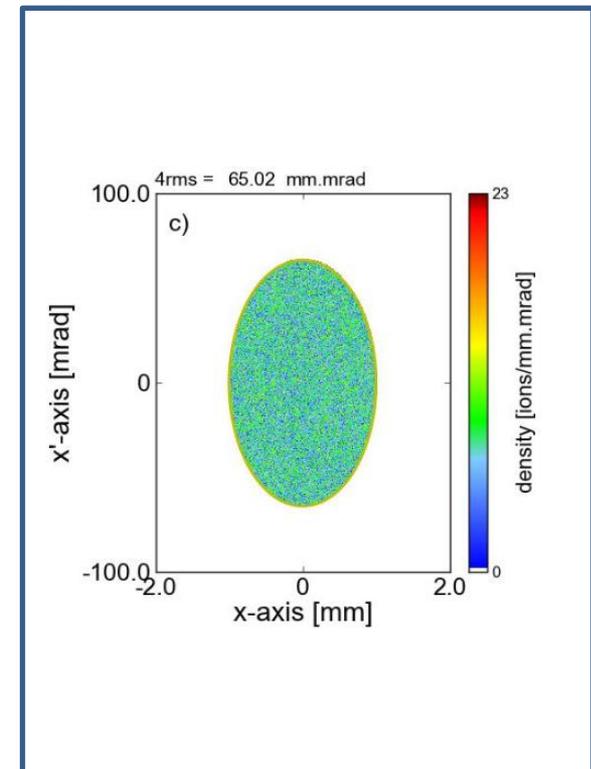


- Theoretical model of the setup $X_1 = M_T \cdot X_0$

Transfer matrix: M_t

x_1	%	x'_1	%	y_1	%	y'_1	%	$(x, x', y, y', \delta, l)_0$
0.82648	24	2.26816	5.8	0	0	0	0	100000
1.668E-06	0	1.20995	108	0	0	0	0	010000
0	0	0	0	-0.85078	9.2	-1.258137	3.8	001000
0	0	0	0	9.100E-02	35	-1.040819	110	000100
-1.3220	0	-0.84624	0	0	0	0	0	200000
-2.0211	-2	-1.6758	0.1	0	0	0	0	110000
-0.94047	33	-1.1015	3.4	0	0	0	0	020000
0	0	0	0	1.96766	0	-3.98394	0	101000
0	0	0	0	3.85987	1.5	-3.84397	0.4	011000
0	0	0	0	5.16242	2	5.65309	0.6	100100
0	0	0	0	5.34891	71	3.59906	13	010100
-3.35827	0	-5.66803	0	0	0	0	0	002000
-3.03125	3	-6.27946	0.6	0	0	0	0	001100
-2.43596	86	-3.12330	9.8	0	0	0	0	000200

X_0 : KV distribution



- Theoretical model of the setup

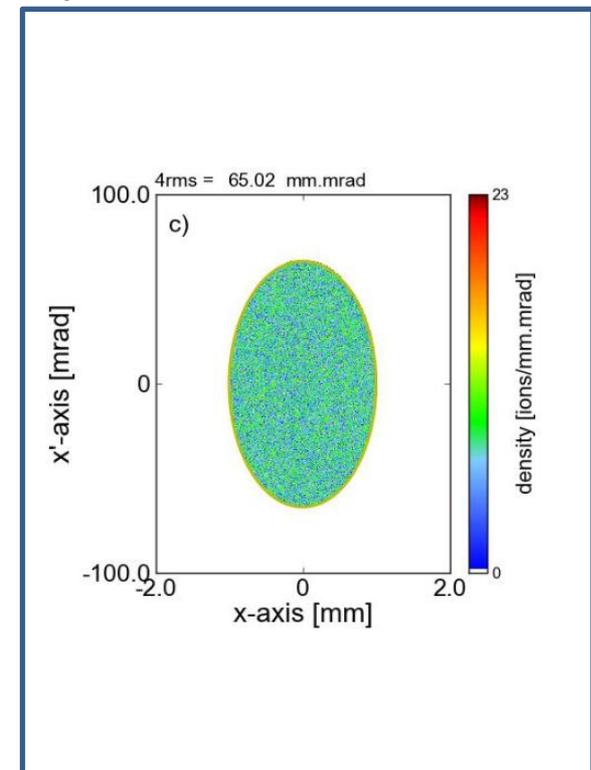
$$X_1 = M_T \cdot X_0$$

Transfer matrix: M_t

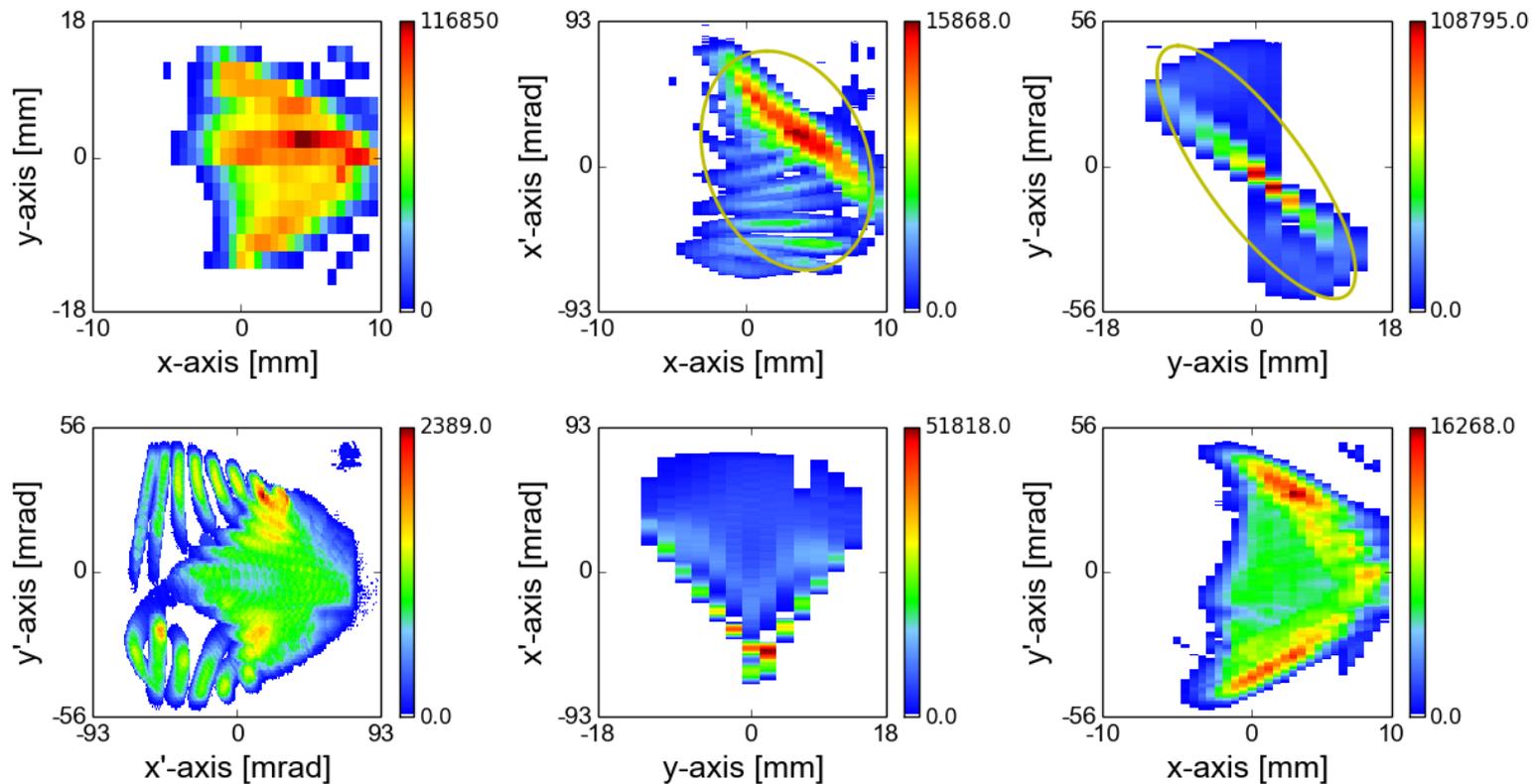
$$\begin{aligned} \theta_1 = & (\theta/x)x_0 + (\theta/x')x'_0 + (\theta/y)y_0 + (\theta/y')y'_0 + (\theta/xx)x_0^2 \\ & + (\theta/xx')x_0x'_0 + (\theta/x'x')x'^2_0 + (\theta/xy)x_0y_0 + (\theta/x'y)x'_0y_0 \\ & + (\theta/xy')x_0y'_0 + (\theta/x'y')x'_0y'_0 + (\theta/yy)y_0^2 + (\theta/yy')y_0y'_0 + (\theta/y'y')y'^2_0 \end{aligned}$$

x_1	%	x'_1	%	y_1	%	y'_1	%	$(x,x',y,y',\delta,l)_0$
0.82648	24	2.26816	5.8	0	0	0	0	100000
1.668E-06	0	1.20995	108	0	0	0	0	010000
0	0	0	0	-0.85078	9.2	-1.258137	3.8	001000
0	0	0	0	9.100E-02	35	-1.040819	110	000100
-1.3220	0	-0.84624	0	0	0	0	0	200000
-2.0211	-2	-1.6758	0.1	0	0	0	0	110000
-0.94047	33	-1.1015	3.4	0	0	0	0	020000
0	0	0	0	1.96766	0	-3.98394	0	101000
0	0	0	0	3.85987	1.5	-3.84397	0.4	011000
0	0	0	0	5.16242	2	5.65309	0.6	100100
0	0	0	0	5.34891	71	3.59906	13	010100
-3.35827	0	-5.66803	0	0	0	0	0	002000
-3.03125	3	-6.27946	0.6	0	0	0	0	001100
-2.43596	86	-3.12330	9.8	0	0	0	0	000200

X_0 : KV distribution



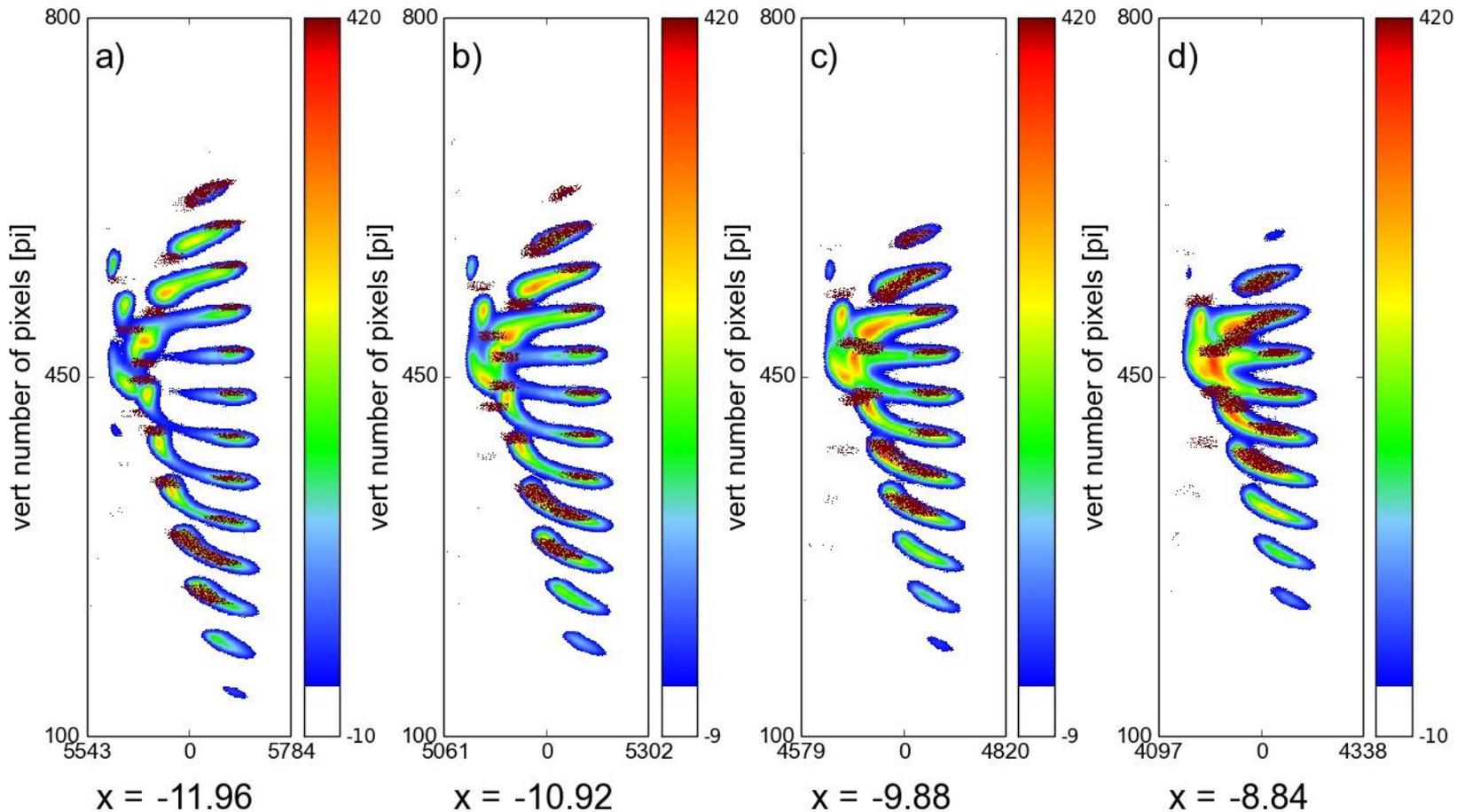
- Measured phase-space projections He^{2+} beam



$$\varepsilon_{xx'} - 4rms = 387 \text{ mm.mrad}$$

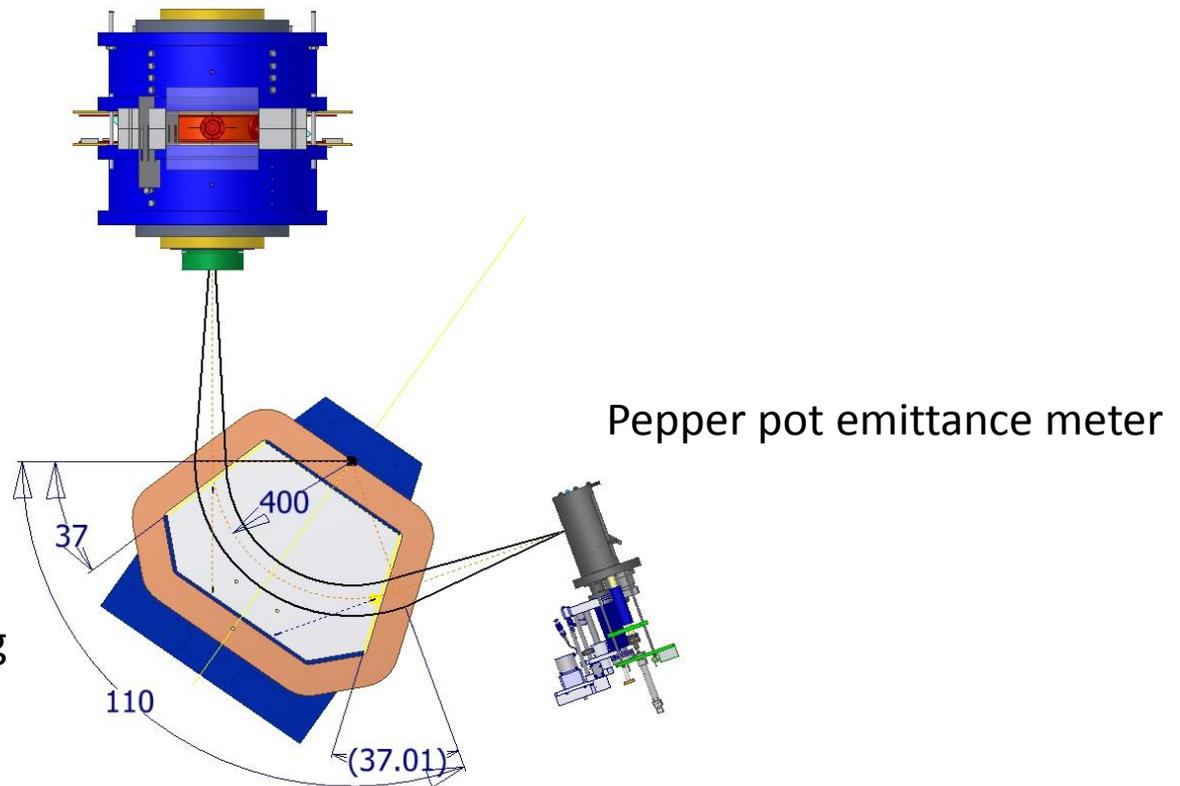
$$\varepsilon_{yy'} - 4rms = 359 \text{ mm.mrad}$$

- Measurements combined with simulations of a 25 kV He¹⁺ beam



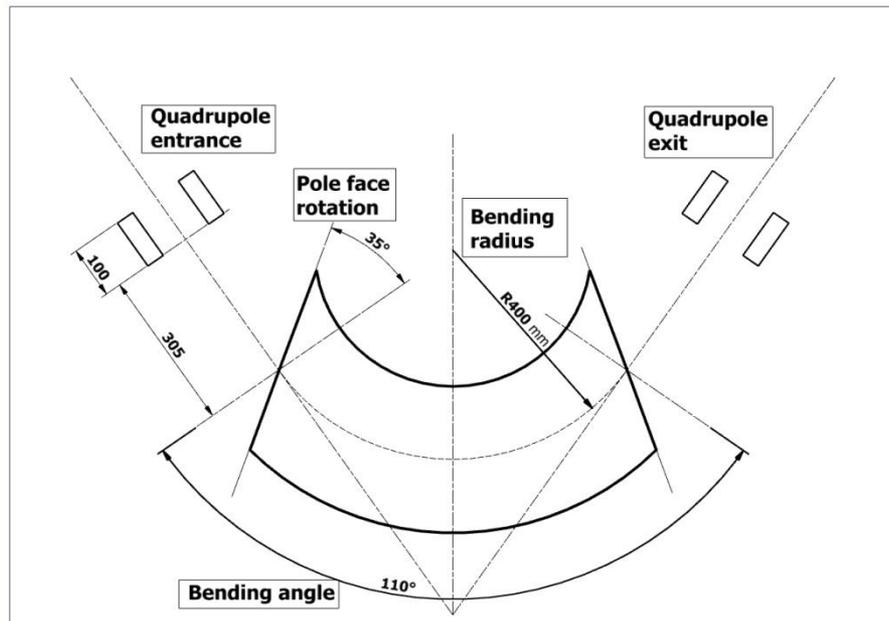
AECR (LBNL type)

34 kV Extraction Voltage



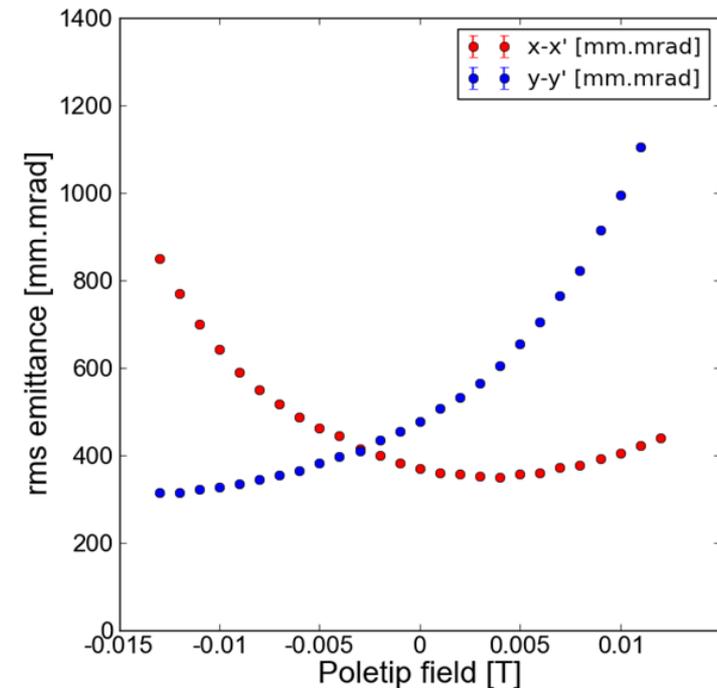
Dipole with an additional two quadrupoles

- Top view analyzing magnet



4RMS emittance 24.5 He^{1+}

as function of the quadrupole excitation





- Possible options to fix.
- Minimize the aberration
 - Add sextupoles
 - Pole curvature
 - Add sextupoles

