



# Superconducting RF Development for FRIB at MSU

Kenji Saito on behalf MSU

MSU NSCL Professor  
Superconducting RF Development Manager

MICHIGAN STATE  
UNIVERSITY



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# Acknowledgment

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Dalesio Bob (BNL),

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Helen Edward(FNAL)

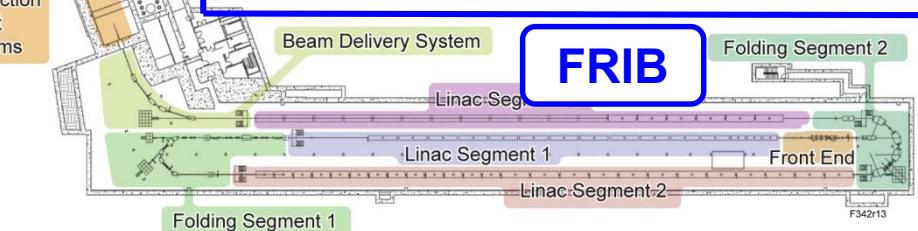
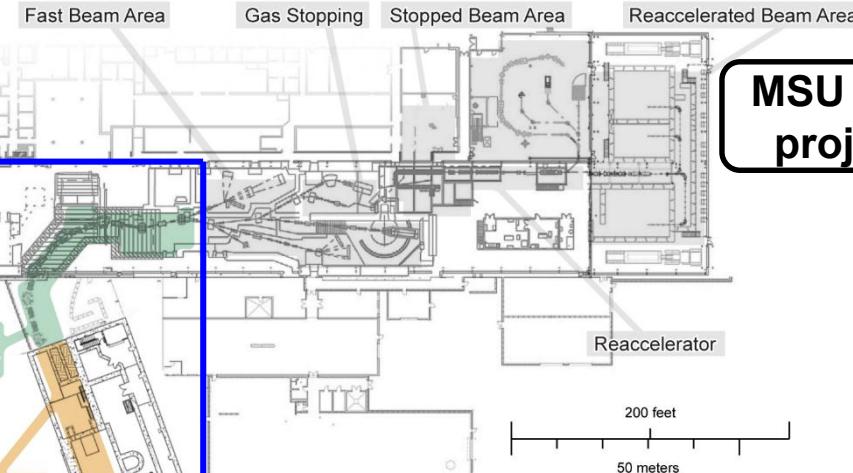


# Outline

- **FRIB Project**
- **FRIB Cryomodule Prototyping**
- **FRIB SRF Development around Cavity**
  - Niobium materials
  - Processing
  - Cavities
  - Coupler and Tuner
- **Cavity/Fringe Field Interaction**
  - 8T solenoid prototyping
  - Magnetic shield behavior exposed high magnetic field
  - Cavity/fringe field interaction
  - 3D full modeling
- **Summary**

# FRIB Scope & Machine Requirements

FRIB is a DOE project for nuclear science, total fund \$730M



- Delivers FRIB accelerator as part of a DOE-SC national user facility with high reliability & availability
- Accelerate ion species up to  $^{238}\text{U}$  with energies  $> 200 \text{ MeV/u}$
- Provide beam power up to 400 kW Satisfy beam-on-target requirements
- Future energy upgradability  $> 400 \text{ MeV/u}$  by filling vacant slots with 12 cryomodules

- Features:
  - Heavy iron beam intensity frontier machine, e.g.  $5 \times 10^{13} \text{ }^{238}\text{U}/\text{s}$ , 250 times higher than ATLAS
  - All SRF from low beta to middle beta section and 2K operation
  - Large nuclear physics user (~1300 users) facility

# FRIB CF Constriction and SRF Highbay

## Project Stage

CD0: Planning

CD1: Proposal, Sept. 2010

CD2: Baseline design, Aug. 2012

CD3-a: Conventional facility, June 2013

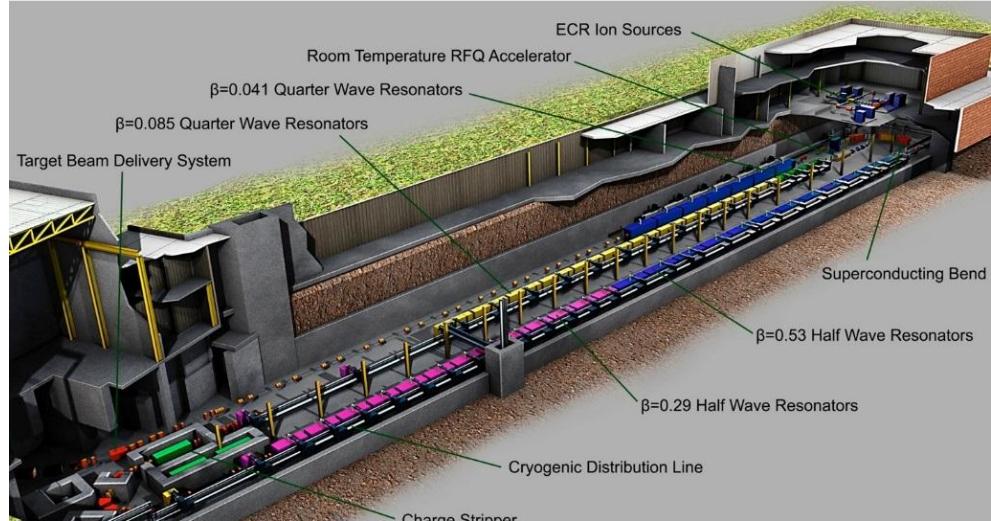
CD3-b: Accelerator system, August 2014

**Acc. System construction starts Oct. 2014**

Early completion 2020

CD4: Completion, to be 2022

**Completed SRF Highbay, under installing infrastructure**



THPP046 L. Popielarski



Tunnel construction started in May 2014



Infrastructure installation in SRF highbay

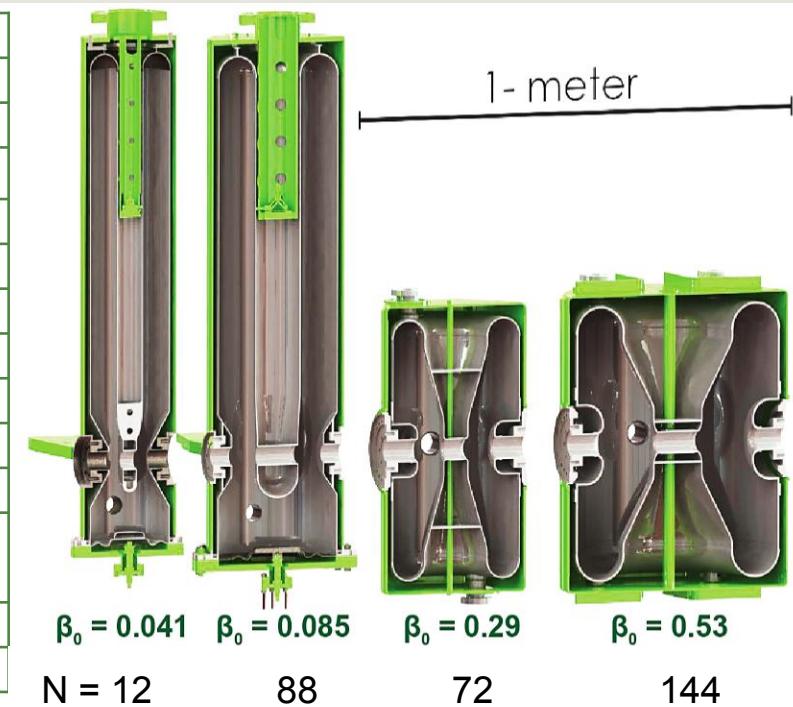


Facility for Rare Isotope Beams  
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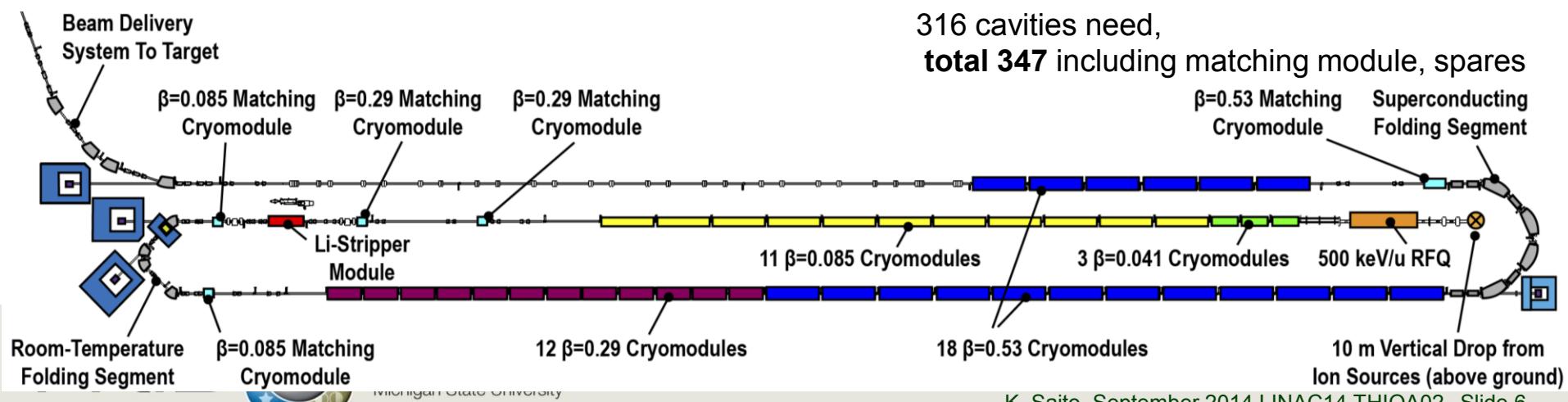
# FRIB SRF Scope

**Challenge: All SRF from low  $\beta(0.041)$  to middle  $\beta(0.53)$**

Cavity Type	QWR	QWR	HWR	HWR
$\beta_0$	0.041	0.085	0.285	0.53
f [MHz]	80.5	80.5	322	322
V <sub>a</sub> [MV]	0.810	1.80	2.09	3.70
E <sub>acc</sub> [MV/m]	5.29	5.68	7.89	7.51
E <sub>p</sub> /E <sub>acc</sub>	5.82	5.89	4.22	3.53
B <sub>p</sub> /E <sub>acc</sub> [mT/(MV/m)]	10.3	12.1	7.55	8.41
R/Q [ $\Omega$ ]	402	455	224	230
G [ $\Omega$ ]	15.3	22.3	77.9	107
Aperture [m]	0.036	0.036	0.040	0.040
L <sub>eff</sub> $\equiv \beta\lambda$ [m]	0.153	0.317	0.265	0.493
Lorenz detuning [Hz/(MV/m) <sup>2</sup> ]	< 4	< 4	< 4	< 4
Specific Q <sub>0</sub> @VT	1.4E+9	2.0E+9	5.5e+9	9.2E+9
Q <sub>L</sub>	6.3E+6	1.9E+6	5.6E+6	9.7E+6

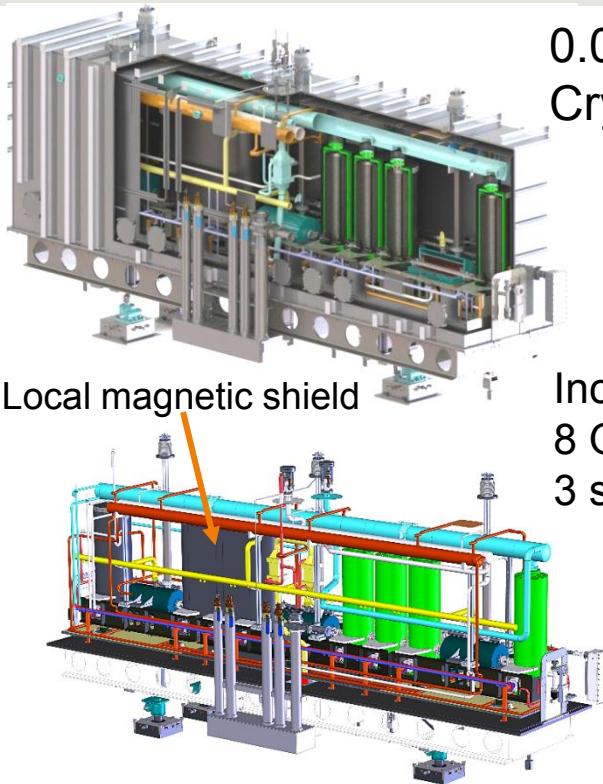


N = 12      88      72      144  
316 cavities need,  
**total 347** including matching module, spares



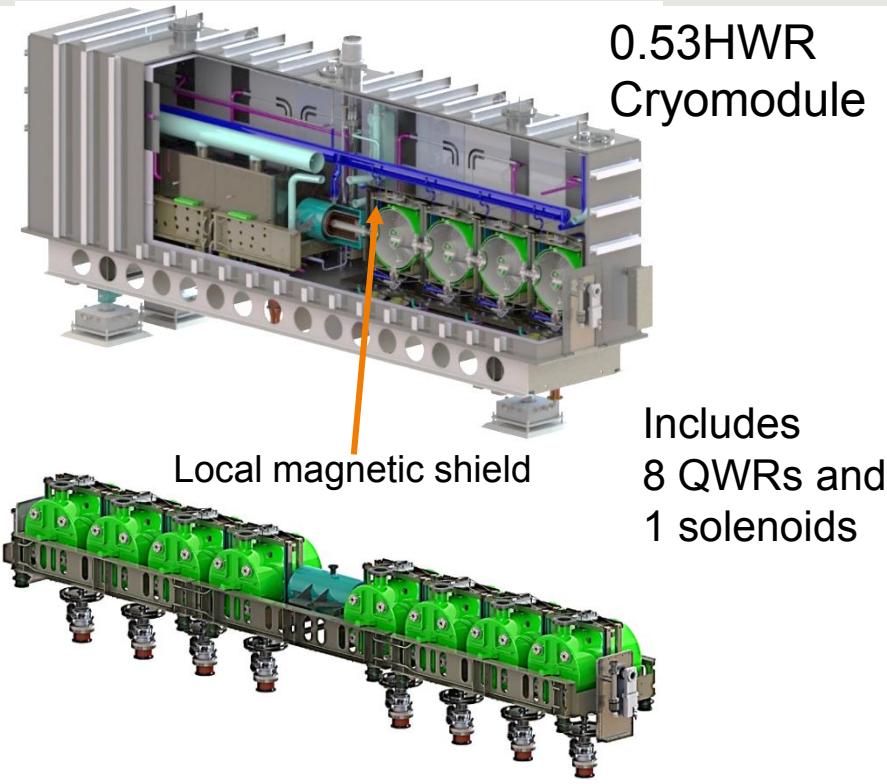
# FRIB Cryomodules, Examples

Need totally 49 CMs: 3(0.041), 11(0.085), 12(0.29), 18(0.53), and 5 matching CMs



0.085QWR  
Cryomodule

Local magnetic shield  
Includes  
8 QWRs and  
3 solenoids



0.53HWR  
Cryomodule

Includes  
8 QWRs and  
1 solenoid

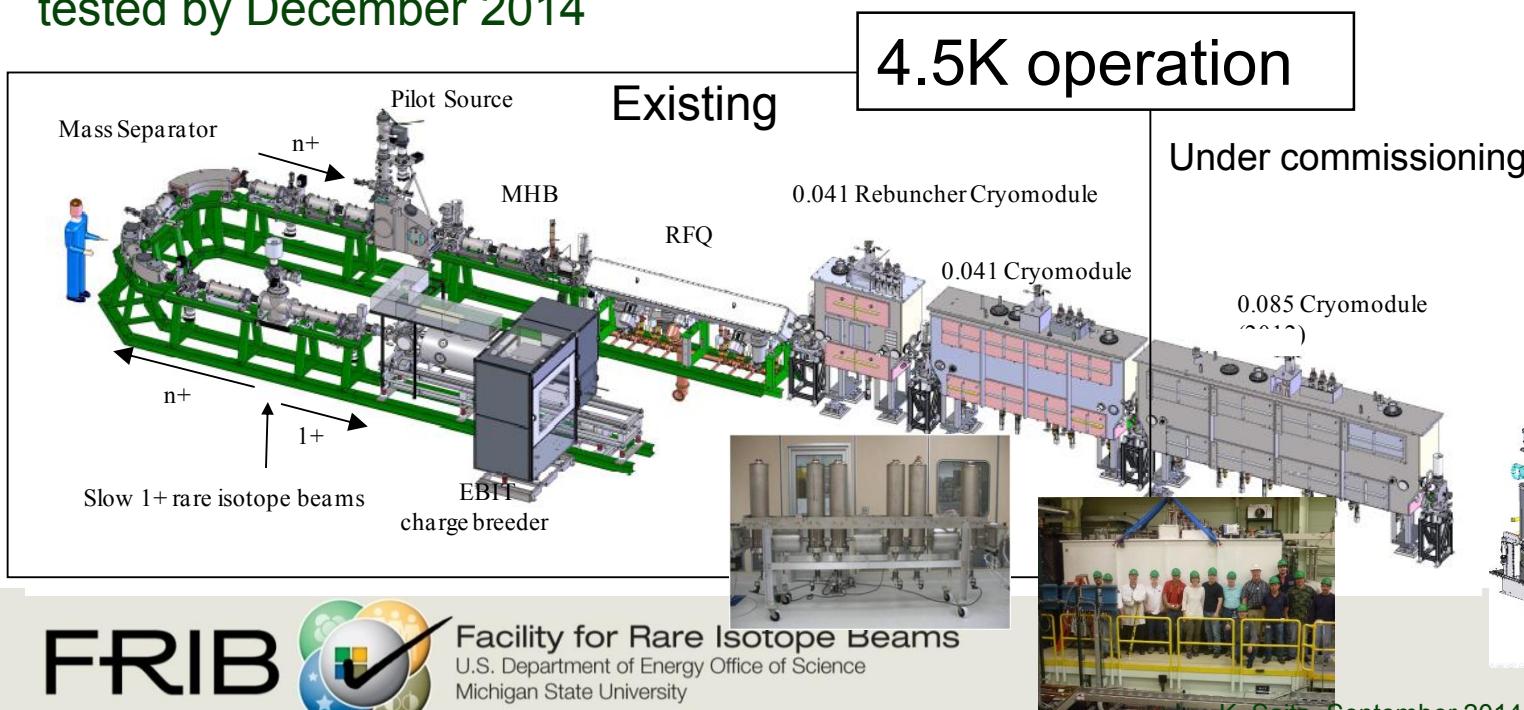
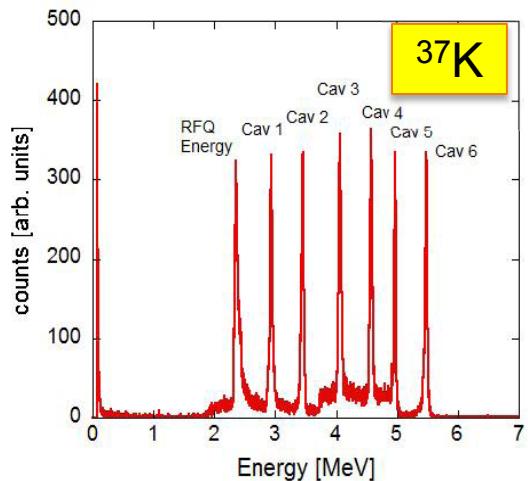
## ▪ FRIB Cryomodule Features

- **Local shield**: cost reduction for magnetic shielding and reliable shielding
- **Bottom-up assembly**: easy assembly and better alignment
- **2K operation**: better cavity performance and less micro-phonics by stable pressure control

# Cryomodule Developments at MSU

## ReA is a benchmark for FRIB

- MSU is constructing ReA project by own fund
- ReA SRF system as a benchmark for FRIB CM system
- A buncher (CM#1, 0.041) and an accelerator module (CM#2, 0.041) are successfully operated with beam since 2012
- Additional 0.085 CM (CM#3) has been installed and is under commissioning August-September 2014 **MOPP044, T. Xu**
- Additional FRIB type CM (ReA6, 0.085) will be installed and tested by December 2014



Facility for Rare Isotope Beams  
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# Lessons Learned from ReA3 Construction

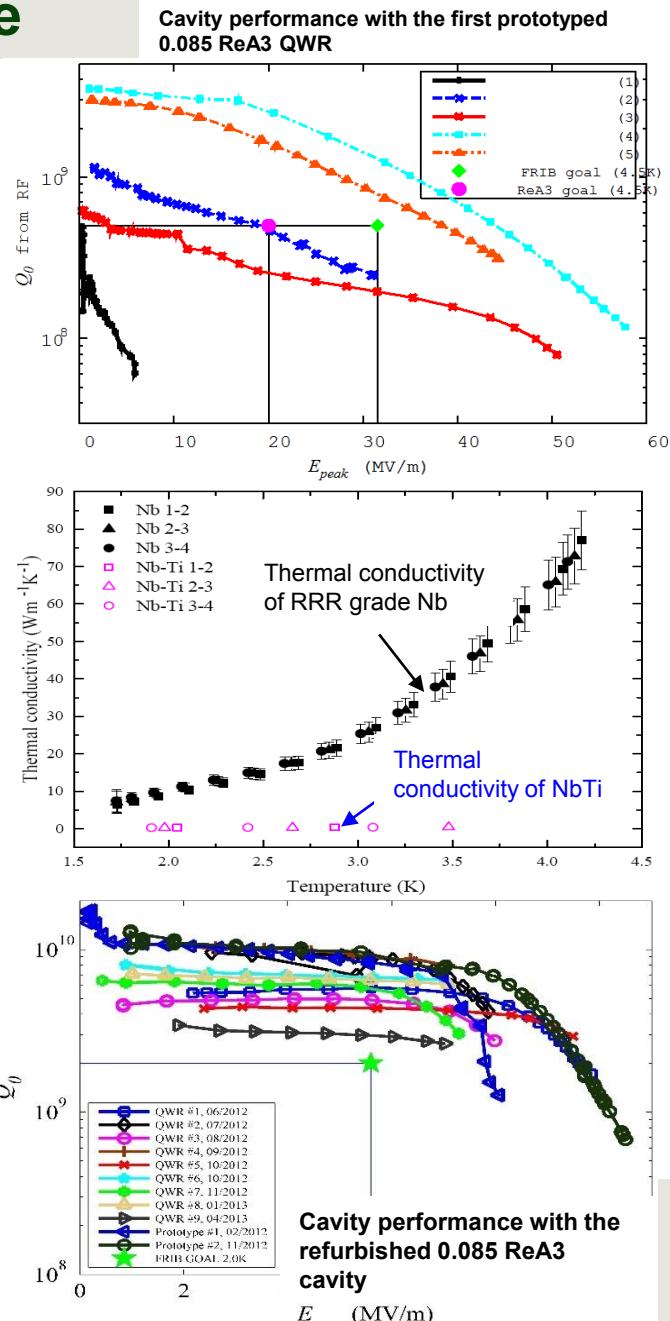
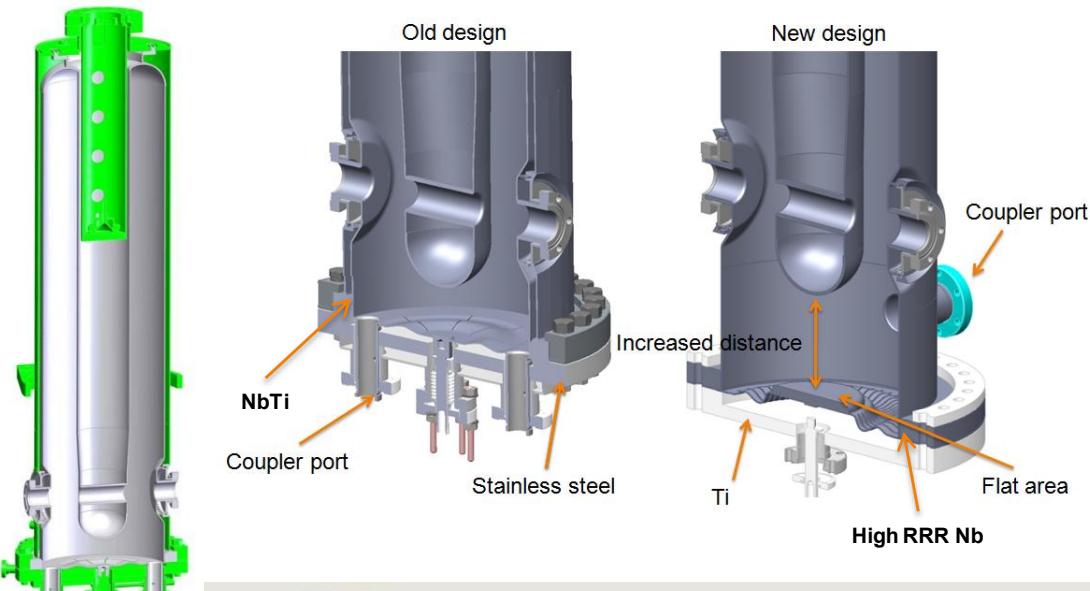
## Bottom flange issue

### ▪ ReA3, 1<sup>st</sup> prototyped $\beta=0.085$ cavities

- Insufficient cooling the tuning plate due to NbTi bottom flange with poor thermal conductivity
- Modified design
  - Elongated the bottom outer tube to reduce magnetic field and made a distance tuning plate-inner conductor
  - RF coupler moved from the tuning plate to the side

### ▪ Refurbished all 11 ReA3 QWRs

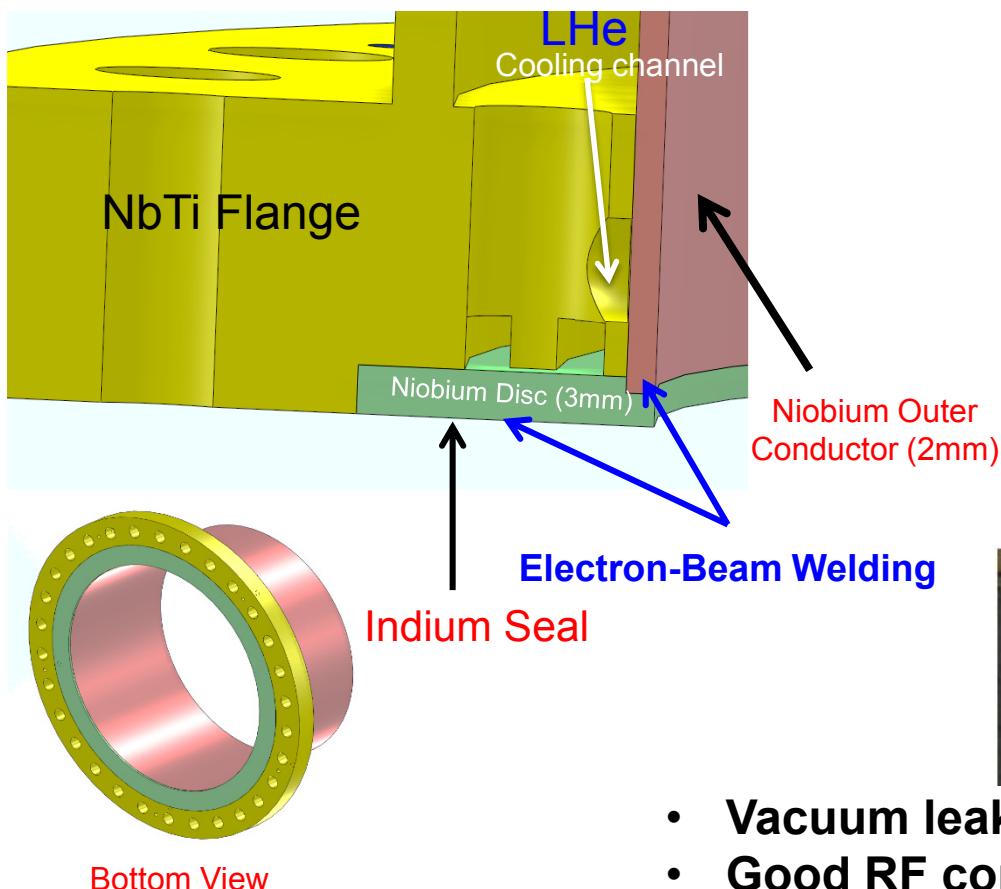
### ▪ Successfully validated the reliable performance with all refurbished cavities



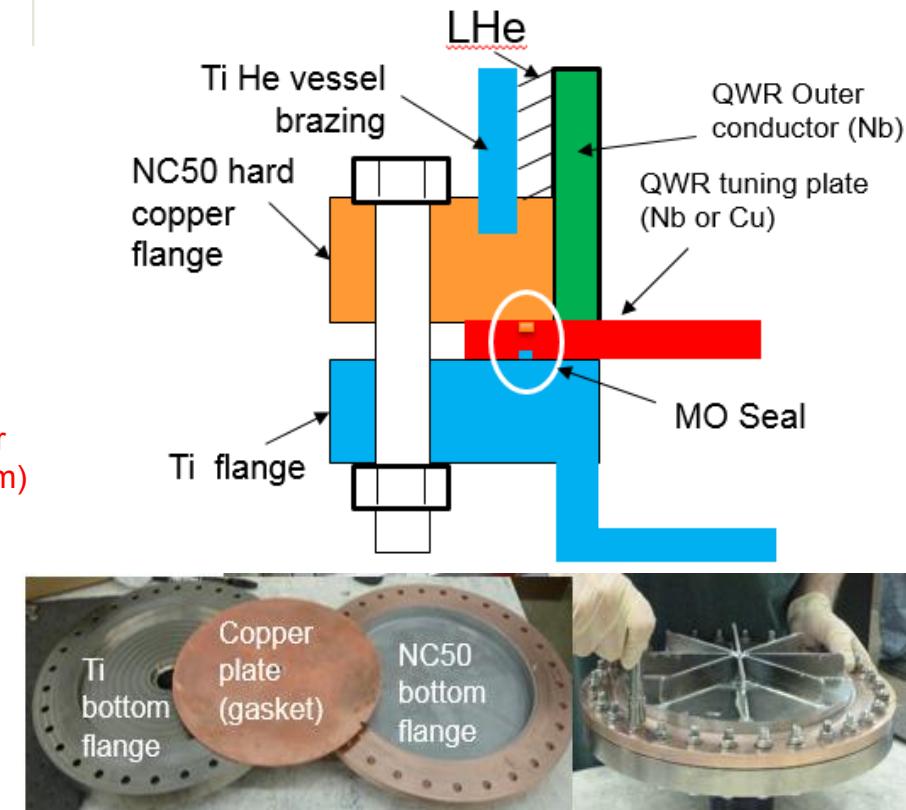
# Redesigned QWR Bottom Flange and Alternative

## Improved cooling, Metal gasket seal flange is also under developing

**Redesigned QWR Flange as FRIB Baseline  
(Indium seal):** Validated already, used  
refurbished ReA3 QWRs

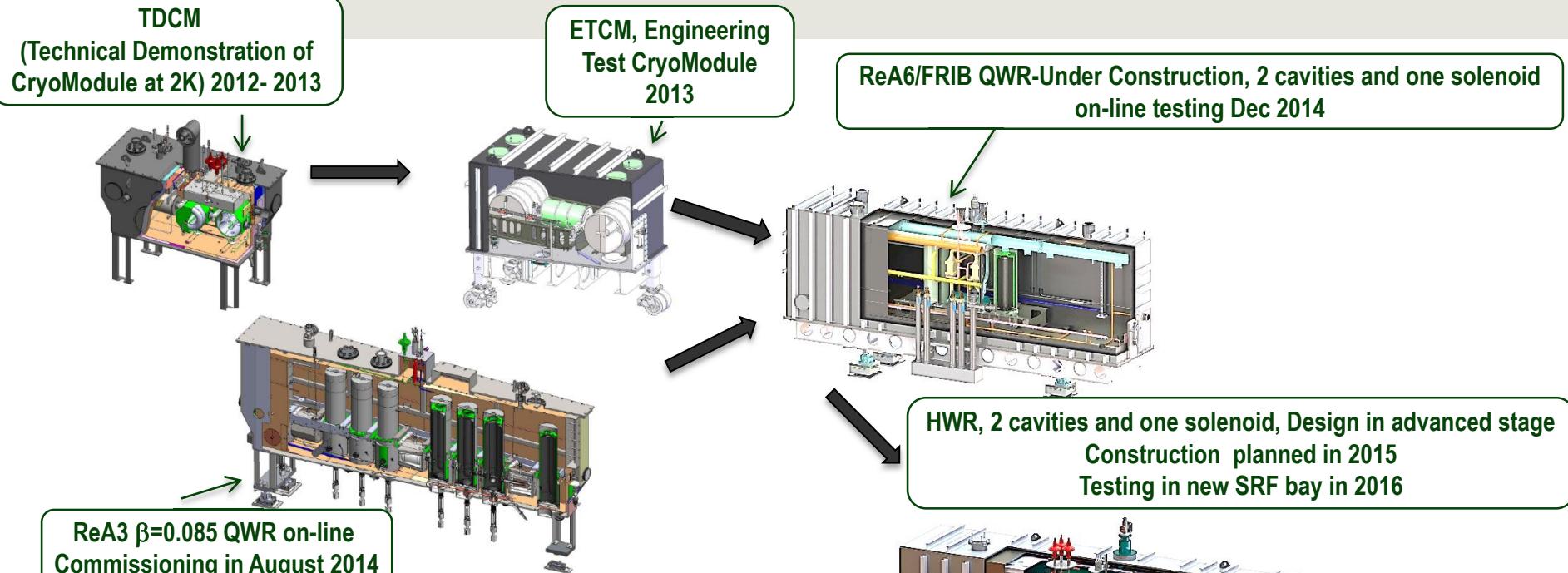


**Alternative (metal gasket seal):  
Under developing**

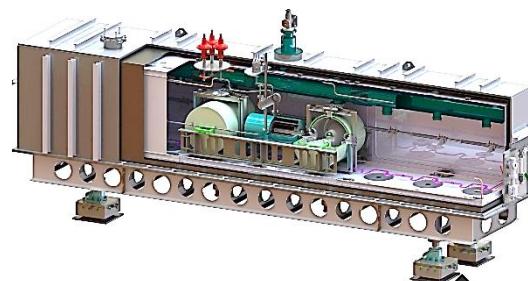


- Vacuum leak tight confirmed
- Good RF contact confirmed by paper pressure test

# Cryomodule Prototyping Approach for FRIB



- **TDCM:** confirm FRIB 2K operation
  - CM construction leak tight at 2K
  - Demonstrate cavity, FPC and microphonics
- **ETCM:** validate bottom-up assembly
  - Validation of alignment tolerance in the bottom-up assembly
- Feedback to future FRIB mass production



FRI<sup>B</sup> first 0.041 CM  
early 2016

# TDCM (Technology Demonstrate Cryomodule)

## Demonstrated 2K operation and verified FRIB design concept

### ▪ Cavity and FPC

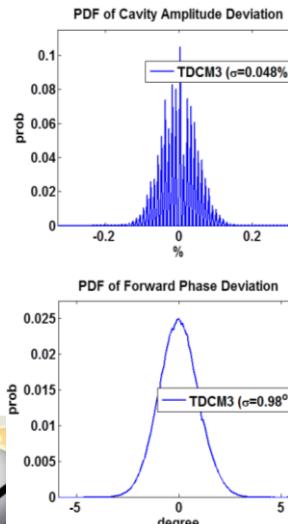
- Cavity performance limited by FE, **need improve assembly procedure**
- Degaussing
- FPC demonstrated 8kW feed and stable operation at 6 - 7kW CW, **MP is an issue**

### ▪ HWR RF bandwidth (Specified: BW=30 Hz, $\Delta f_{pp} \leq 0.5$ BW)

- Fast detuning distribution: Gaussian,  $\sigma \sim 0.5$  Hz,  $\Delta f_{pp} < 6$  Hz  $\equiv \pm 6\sigma < 0.5\text{BW}$ , **satisfied FRIB specification**
- Slow detuning following He pressure

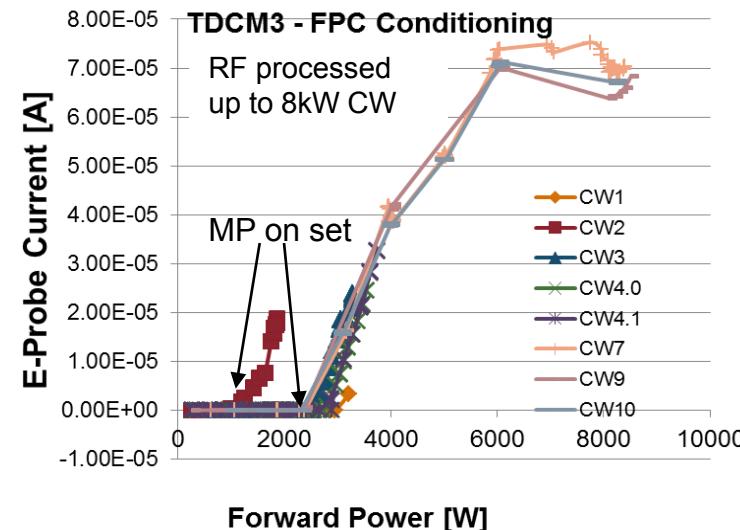
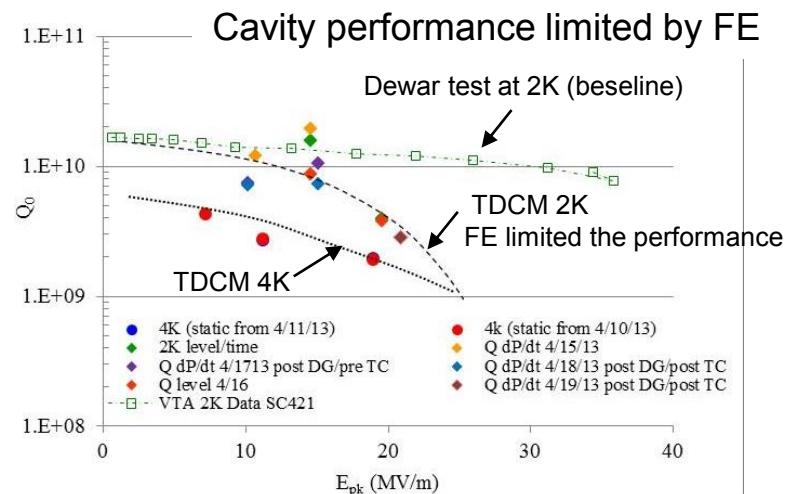
### ▪ 2 K He bath pressure stability

- $\Delta P \leq \pm 0.1$  mbar peak, as in SNS



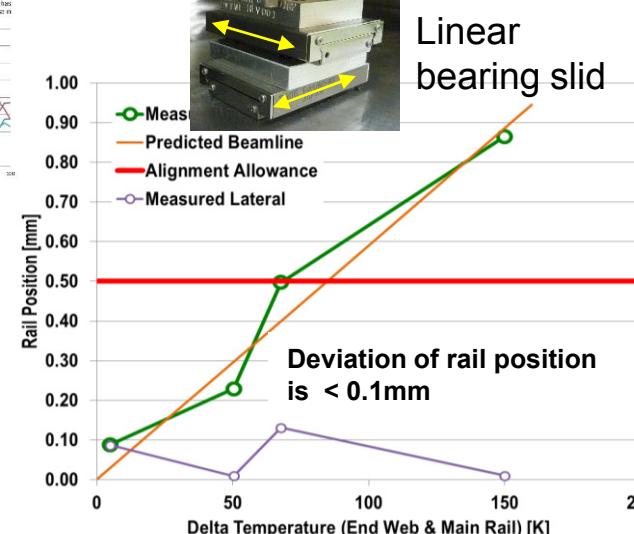
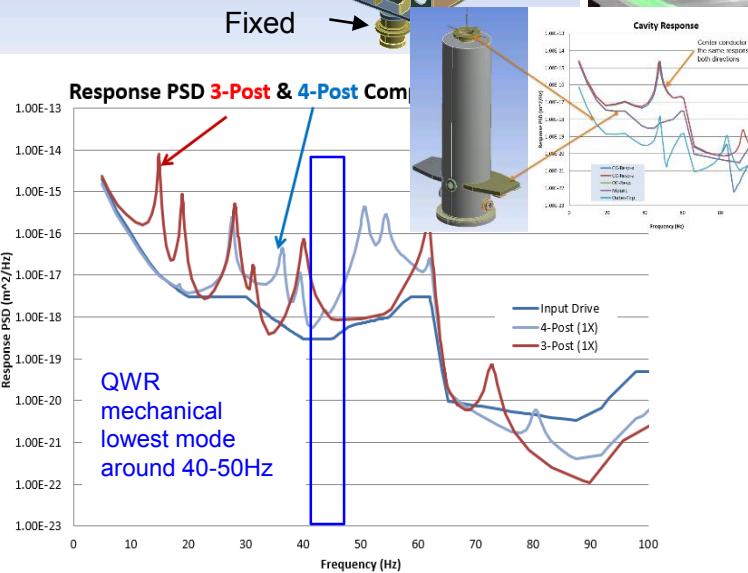
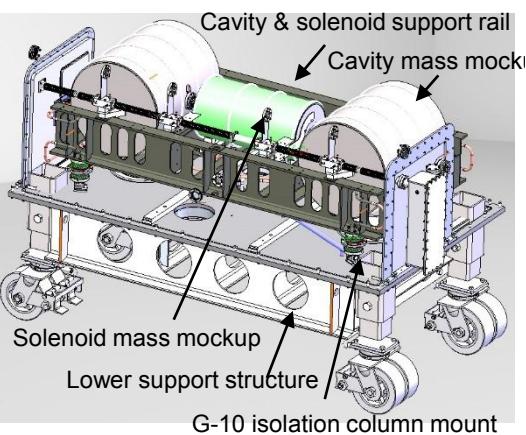
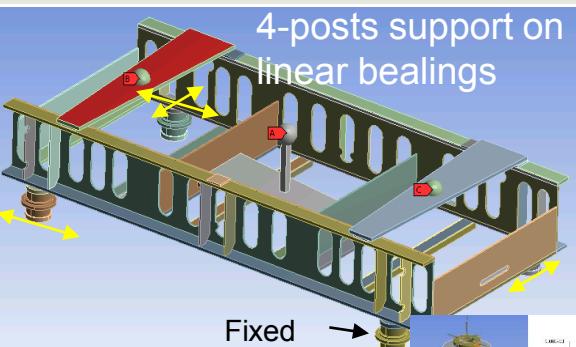
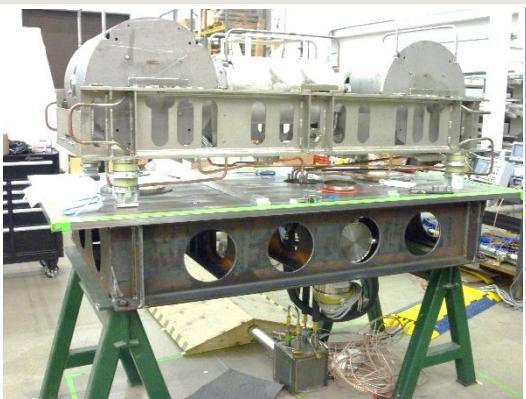
HWR detuning distribution:  
 $\sigma \sim 0.5$  Hz rms  
 Max detuning  $\leq \pm 6$  Hz p-p

**FRIB specifications fulfilled in TDCM**



# ETCM (Engineering Test Cryomodule)

Validated bottom-up cryomodule assembly concept with high alignment accuracy ( $\sim 0.1$  mm)



- Successfully verified cavity self-aligning by linear bearings during liquid nitrogen cool-down & vacuum vessel enclosure
- 4-post support established as design choice based on vibrational response analysis
- Successfully evaluated vibration, test with actual load and realistic configuration
- Divided into three sections for the FRIB QWR support rail to eliminate lower mechanical modes

# Niobium Materials for FRIB

Early procurement, all materials will be delivered by end of 2014

- **FRIB procures of niobium material from three vendors**

- Wah Chang – NbTi flange material
- Tokyo Denkai – RRR250 niobium sheets
- Ningxia – RRR250 niobium sheets and tubes

- **Material specification**

- Dimension check, surface inspection
- RRR > 250 for niobium sheets
- Grain size ASTM#5 ( $64\mu\text{m}$ )
- 0.2% Yield strength > 48.3MPa
- Tensile strength > 96.5MPa
- Elongation > 40% (longitudinal), 35% (transverse)
- Hardness < Hv = 60
- Vender etching

- **FRIB acceptance tests**

- Two samples from per production lot are tested
- Dimensional and surface finish
- Mechanical test (Ultimate, Yield, Elongation, Hardness)
- Metallurgy properties measurement (Grain size, Crystal orientation, Recrystallization)
- RRR/Thermal conductivity

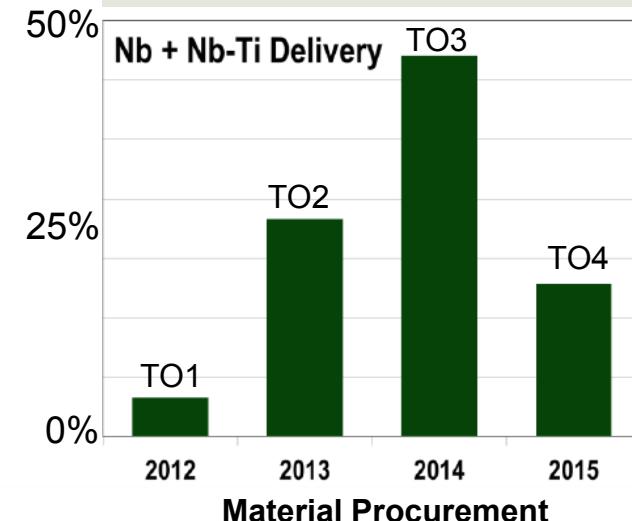
- **Materials are well controlled at FRIB**



NbTi flange material



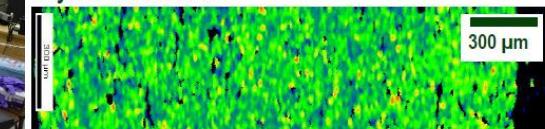
Seamless Nb tubes



Nb sheet material



Crystal Orientation



Misorientation Distribution



# FRIB Unique QA Process Control

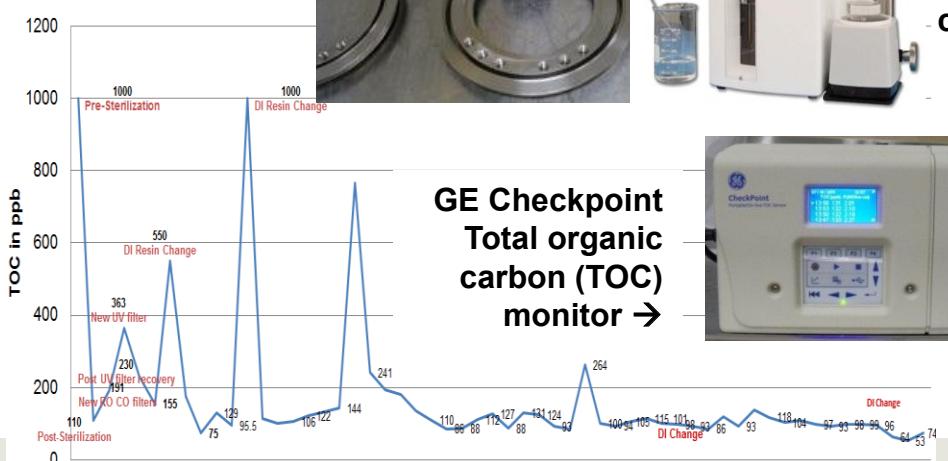
## Particle contamination control based on particle counter

- Established the QA procedure by diagnostic tools developed in the past R&D phase

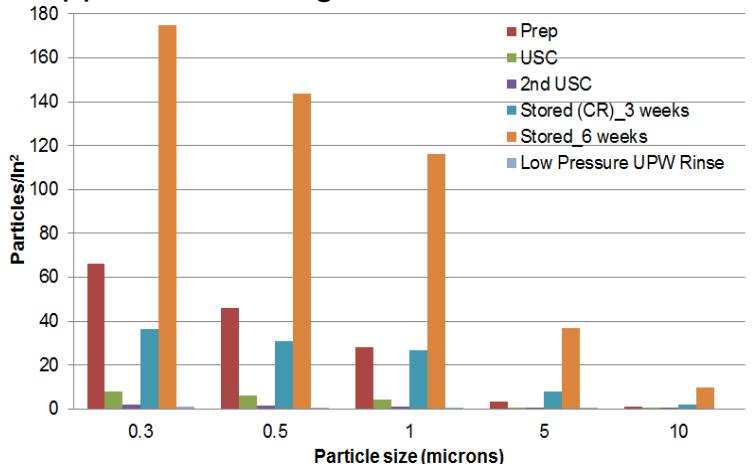
LINAC2012, L. Popielarski and R. Oweiss et al.

- BCP, removed 150 $\mu$ m
  - HPR, 1hr
  - Monitoring particles in the HPR waste water
  - Monitoring particle contamination on flanges during cavity assembly
  - Baking 120°C for 48hr

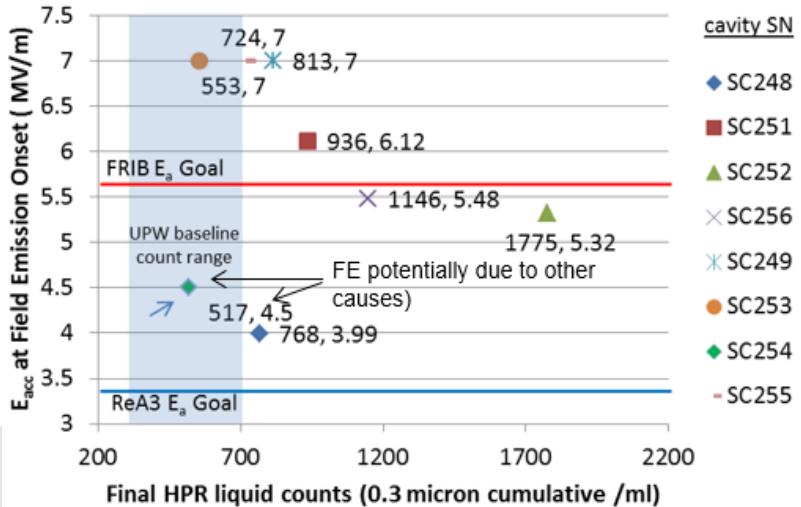
- QA control by particle counter is very effective to reduce FE



A close-up photograph of the CheckPoint Complete-on-site VOC Sensor. The device has a light-colored, rectangular body. On the left side, there is a digital display screen showing the text "VOC SENSORS" and "COMBINED VOC SENSOR". Below the screen is a small keypad with four arrows (up, down, left, right) and a central button. To the right of the keypad, there are two circular ports with labels: "Furnace" and "Exhaust". A power cord is visible on the far right.



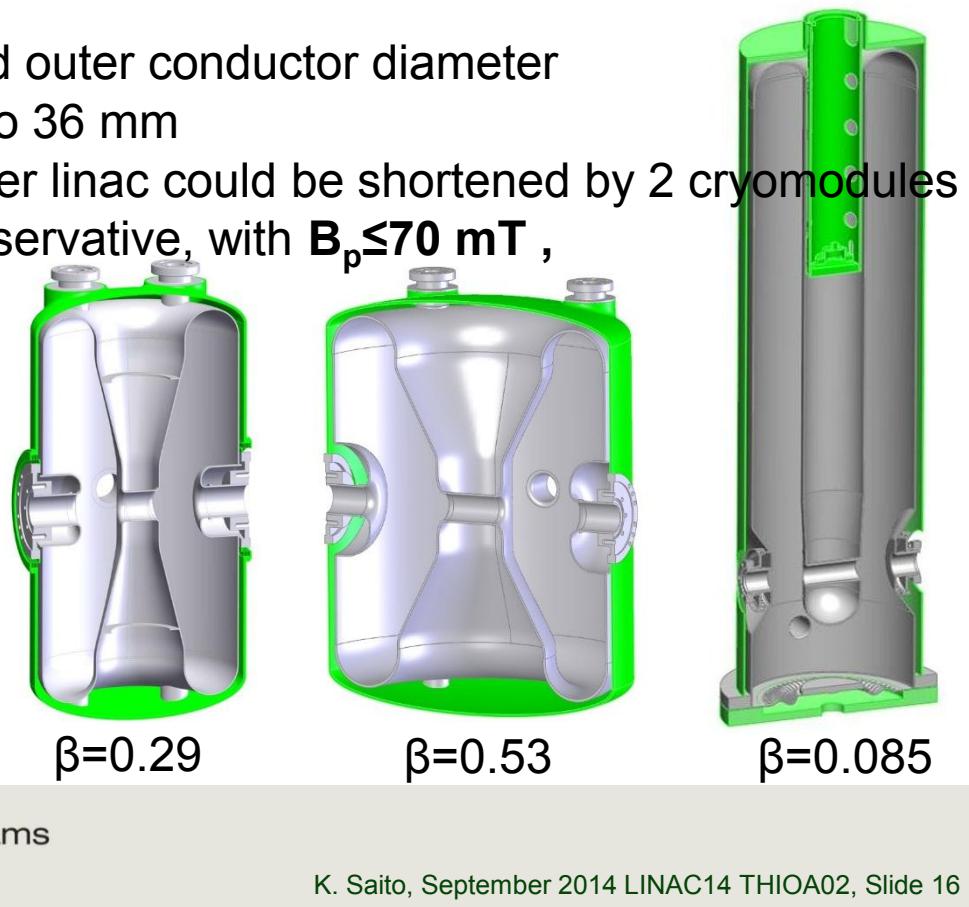
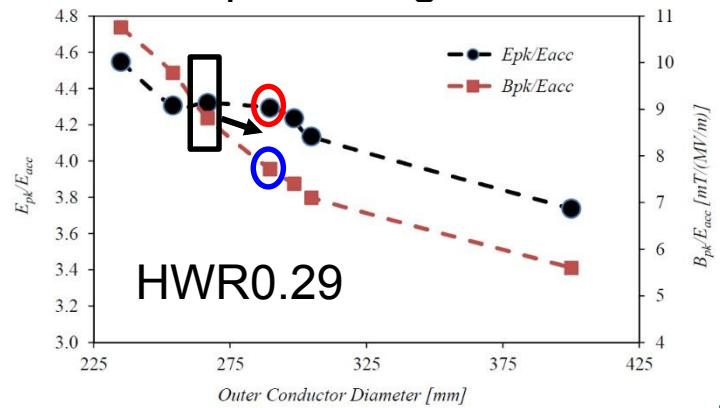
### Good correlation between particle and FE onset



# FRIB Final Cavity Design

## Improved cavity design with lower Hp/Eacc and Ep/Eacc

- The SRF Review Committee in 2011 recommended not to exceed  $E_p=35 \text{ MV/m}$  and  $B_p=70 \text{ mT}$  in operation based on experimental data of 40 QWRs in operation at TRIUMF
- FRIB has adopted this specification to guarantee reliable operation of its linac with a good safety margin
  - lower  $E_p$  &  $B_p$ , higher  $R_{sh}$**  by increased outer conductor diameter
  - Increased aperture of QWRs from 30 to 36 mm
  - Increased operation  $E_{acc}$ : the FRIB driver linac could be shortened by 2 cryomodules
  - FRIB operation gradient now more conservative, with  $B_p \leq 70 \text{ mT}$ ,



cavity	$E_p/E_{acc}$	$B_p/E_{acc}$	$R_{sh}$	$E_{acc}$
QWR085	-9%	-11%	+38%	+10%
HWR29	-3%	-28%	+47%	+10%
HWR53	-17%	-19%	+13%	(+6)%

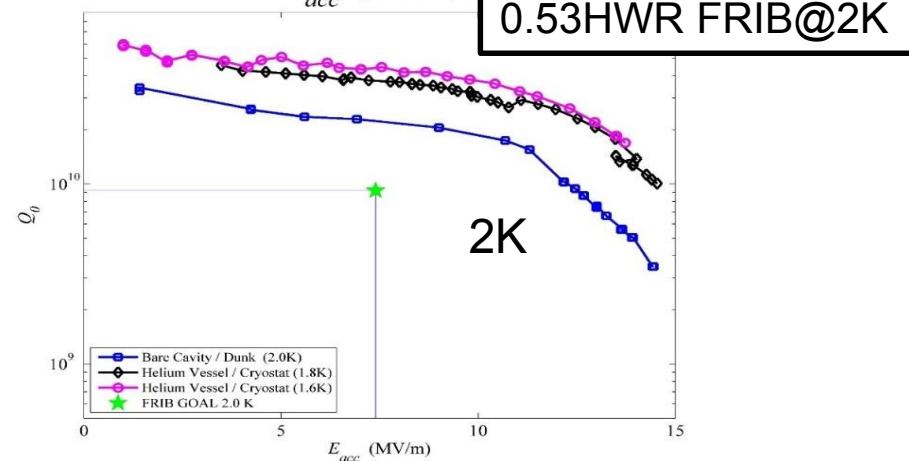
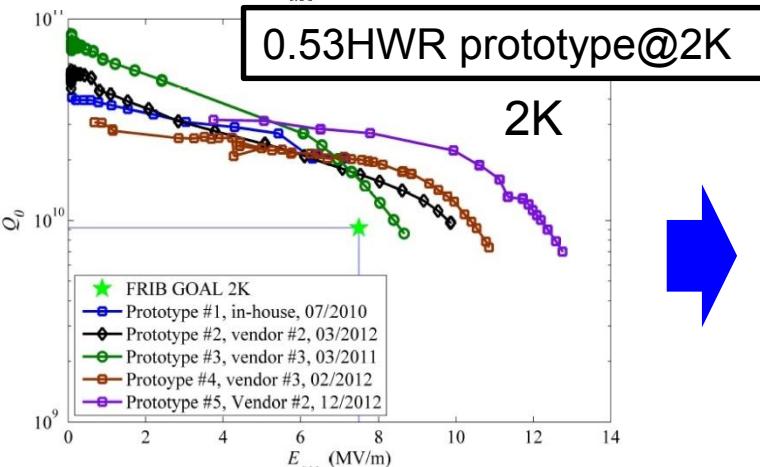
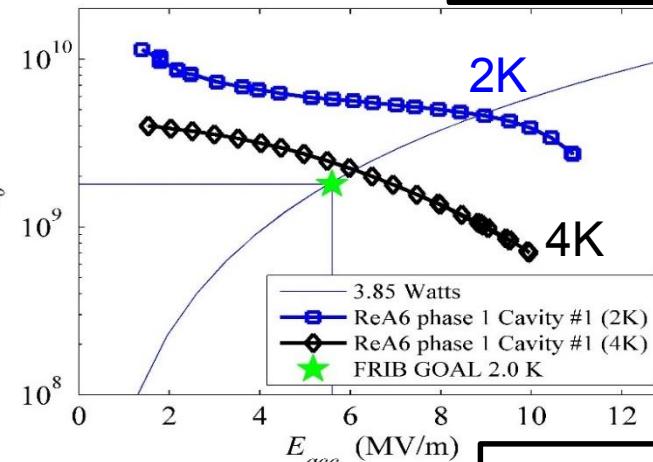
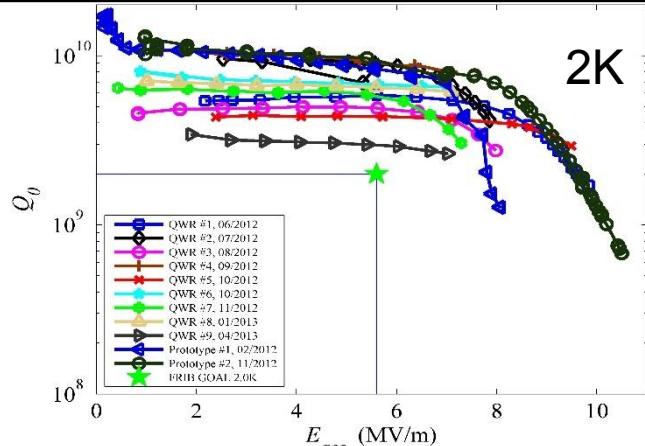
# Validation of the FRIB Final Cavity Design

## Comparison with first prototyped cavity and final design cavity

ReA3 refurbished 0.085QWR@2K

MOPP044, J. Popielarski

FRIB 0.085QWR@2K

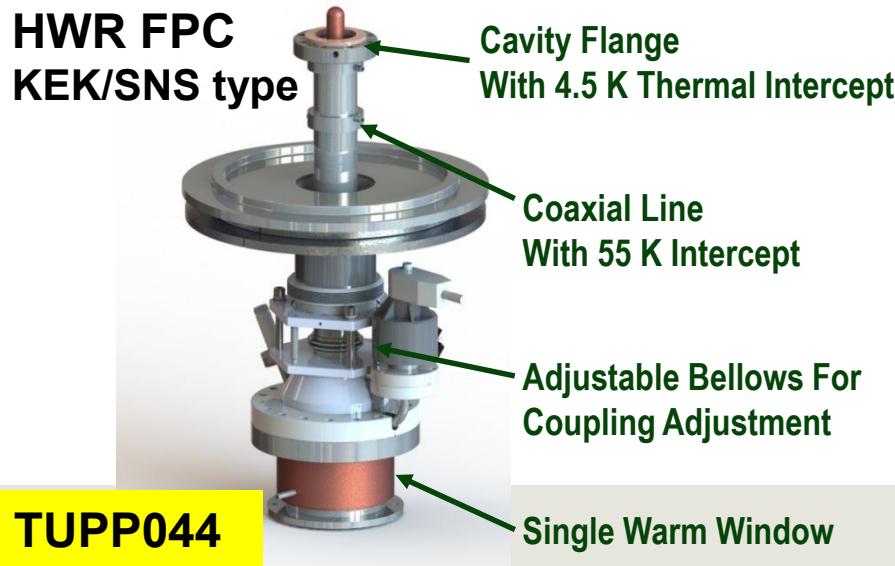
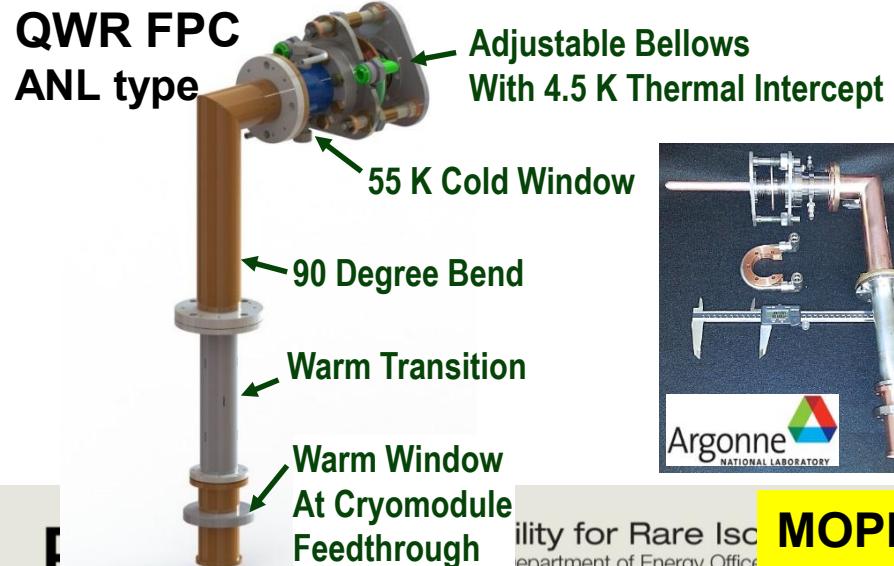
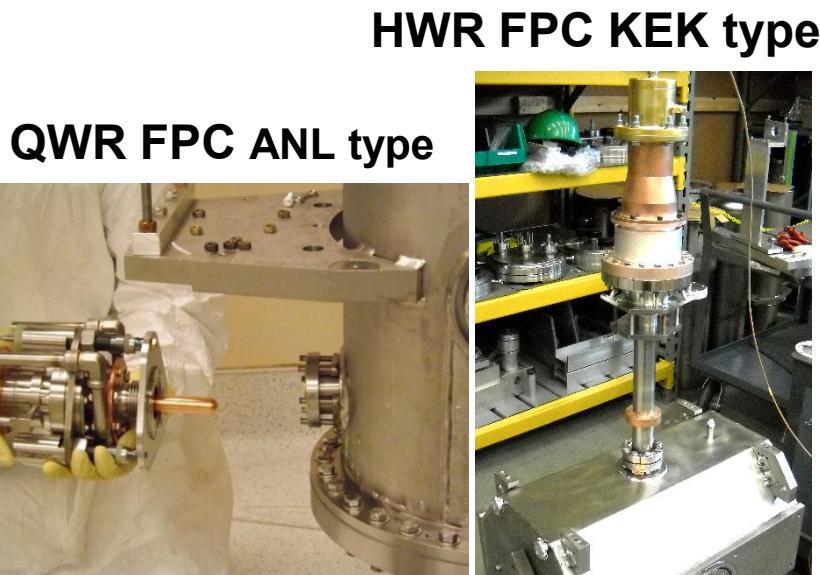


- Mitigated high Q-slope by improved design with lower  $B_p/E_{acc}$
- Improved enhanced performance margin as expected
- All four cavity types have been successfully validated with helium vessel

# FPCs for FRIB Cryomodule

## ANL type for QWR and KEK/SNS type for HWR

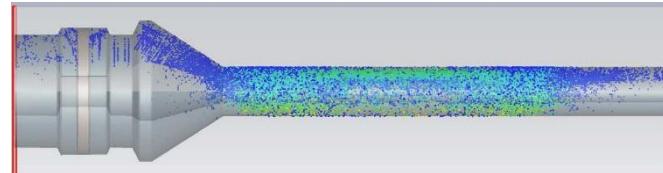
Coupler Type	QWR	HWR
Frequency [MHz]	80.5	322
Line Impedance [ $\Omega$ ]	50	50 <sup>(*)</sup>
Cavity RF Bandwidth [Hz]	40	30
Installed RF Power [kW]	2.5	5
Max. Coupler Power Rating [kW]	4	10
Manual Coupling Adjustment	1/2 To 2 Times Bandwidth	
Coupler Interface	1-5/8" EIA	3-1/8" EIA
Total Heat Load To 2 K At Nominal RF Power [W]	0.13	0.6
Total Heat Load To 4.5 K At Nominal RF Power [W]	1.3	2.7
Total Heat Load To 55 K At Nominal RF Power [W]	7.1	6.2



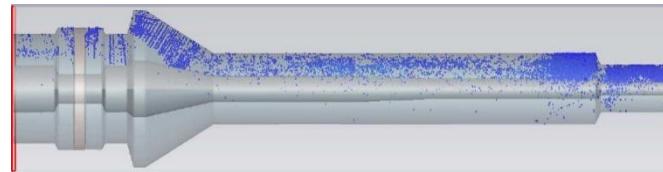
# Alternative FPC: MP Free Coupler

- **The principle of the FPC design**
  - Simple structure: choke free at window
  - Multipacting free: increase impedance, pushed up the MP over the usable range
  - Electron screening for ceramic surface

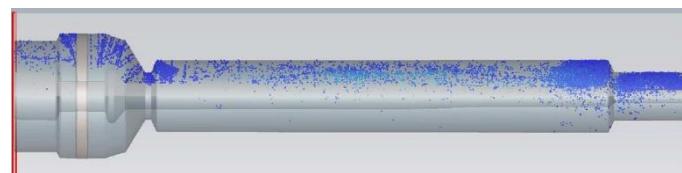
6.75" Baseline (50-84-50-50 Ohm)



8" MP Free (50-84-50-61-75 Ohm)



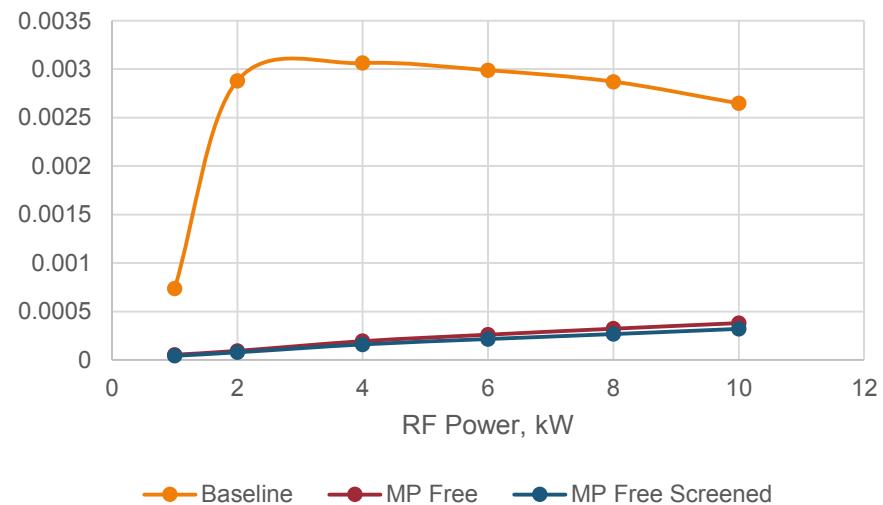
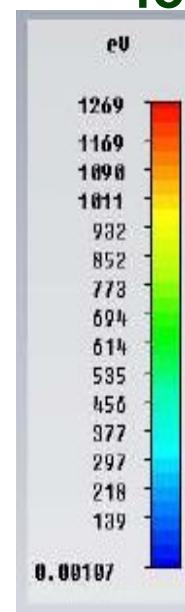
6.75" MP Free (50-84-61-75 Ohm).  
Complete screening



## ▪ Electron emission images at 4 kW

- **The particle sources density kept similar for three geometries**

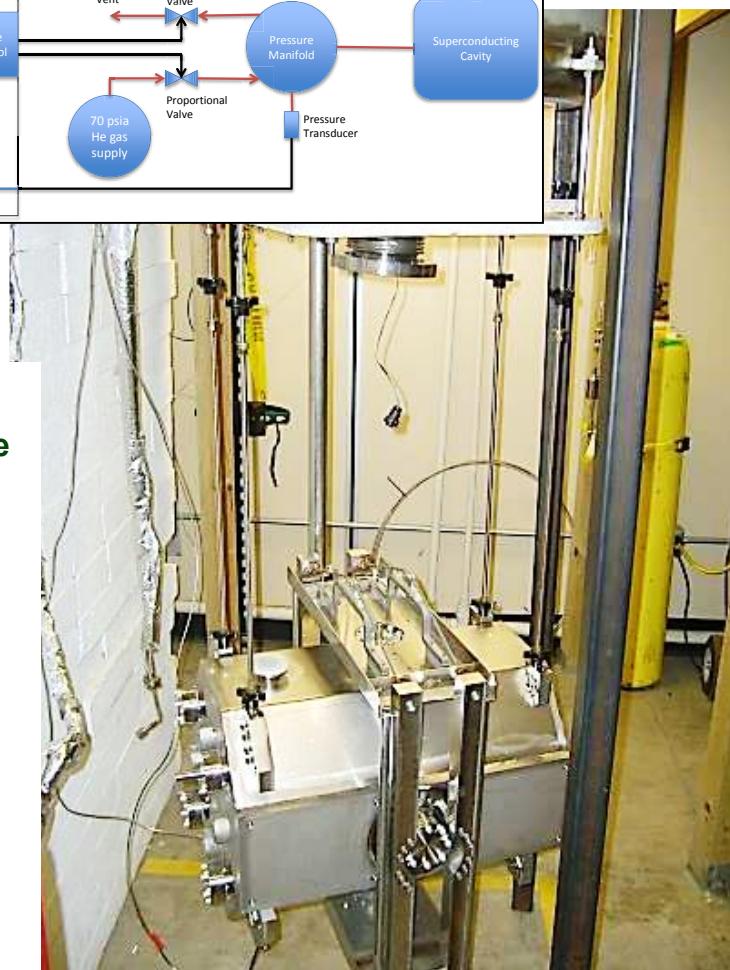
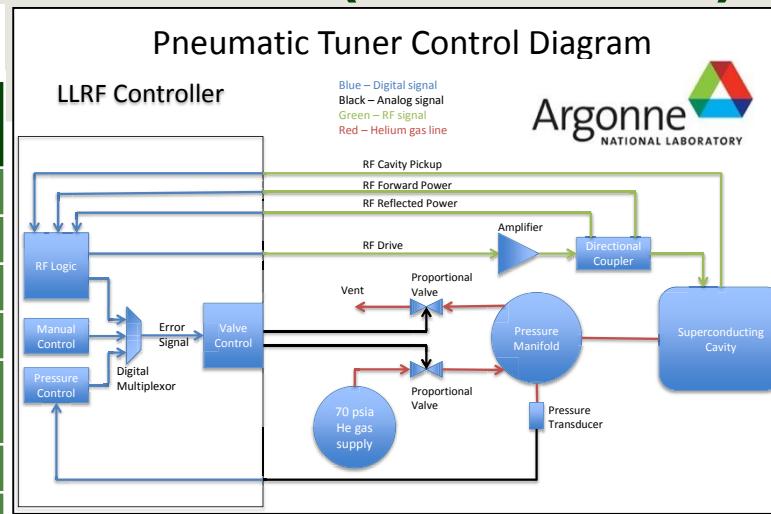
Secondary electrons number for 1 primary electron



# Pneumatic Tuner for HWRs(0.29, 0.53)

## FRIB Tuner Specification

Tuner Type	HWR $\beta=0.53$
Minimum Tuning Range [kHz]	120
Tuning Resolution (2% of Bandwidth) [Hz]	0.6
Maximum Backlash (5% of Bandwidth) [Hz]	1.5
Cavity Tuning Sensitivity (calculated) [kHz/mm]	$\sim 236.2$
Maximum Displacement [mm] port-to-port	-0.5 (*)
Cavity df/dp (Free Tuner) (calculated) [Hz/torr]	$\sim -3.43$
Cavity LFD (Free Tuner) (calculated) [Hz/(MV/m) <sup>2</sup> ]	$\sim -3$



Final 0.53HWR w/vessel LFD =  $-2.5 \text{ Hz}/(\text{MV/m})^2$ , well fits the simulation

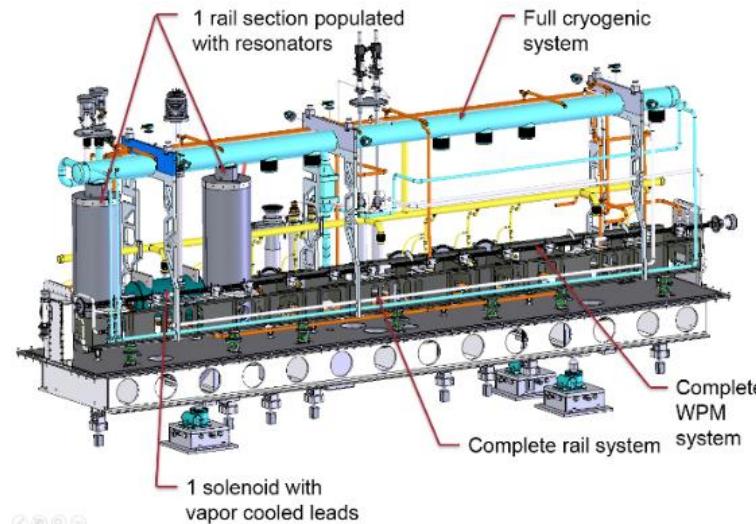
- **Demonstrated Performance in VT**
  - Maximum tuning speed in regulation (phase < 2° peak to peak, amplitude < 2%)
    - » +/- 0.35 Hz/sec
    - » Higher speeds (1 Hz/sec) were possible while detuning within the band width
    - » The background RF noise was higher than expected in this test (12 Hz peak to peak)
  - Maximum tuning speed in self-excited loop (SEL) mode
    - » - 400 Hz/sec (pressure increasing)
    - » + 363 Hz/sec (pressure decreasing)
    - »  $\Delta f/\Delta P = 321 \text{ Hz/psi}$  ( $4.566 \text{ kHz/kgcm}^2$  frequency change from tuner pressure)
- The final pneumatic tuner designs fits final HWR cavities (0.29/0.53).
- Final integrated validation test in vertical Dewar is under preparation

# Integrated Certification Test Plan

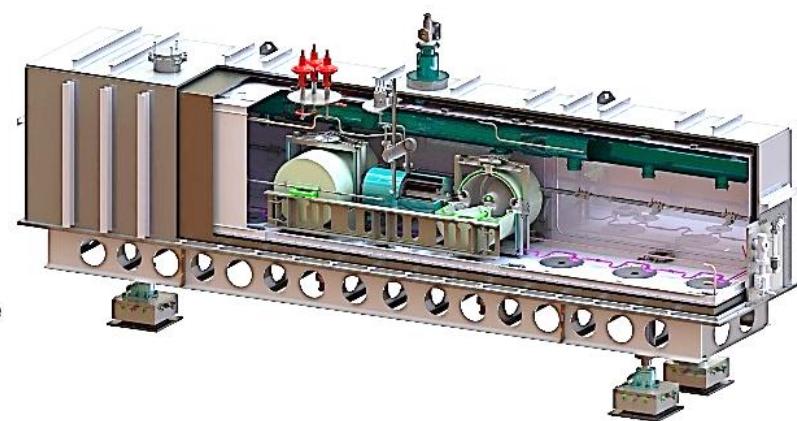
- All components are ready for FRIB production, full integration test (cavity, FPC, tuner) is planned in VT for component long term operation. **THPP047, J. Popielarski**
- ReA6 CM is the first FRIB CM for QWR, of which phase-1 test is to be completed in mid-December 2014.
- The cavity-solenoid interaction will be confirmed in ReA6-1.
- ReA6/FRIB CM full Integrated test is to be done in December 2014.
- 0.53 HWR CM-1 ( two cavity and one solenoid) will be tested 2016



VT integrated Test



ReA6-1



0.53HWR CM-1

# 8T SC Solenoid Prototyping by MSU/KEK Collaboration

Dry winding technique has been confirmed high performance and no training

## ▪ Changed FRIB solenoid specification from 9T to 8T

- Solenoid is not allowed to quench during machine operation from cavity protection point of view, solenoid has to be in stable operation
- Reduced solenoid field from 9T to 8T by changing constant  $\beta(z)$ -function optics to constant beam sized one
- Original FRIB commercial solenoid design has only 0.1K operation margin
- ASAC 2014-12 recommended for the solenoid to have an operation margin as much as 0.5K

## ▪ Designed 8T solenoid package with 0.5K operation temperature margin under KEK/MSU collaboration

## ▪ Prototyped 25cm 8T solenoid package: solenoid + steering dipole coils at KEK

- Pursued cost-effective fabrication method: dry winding technique

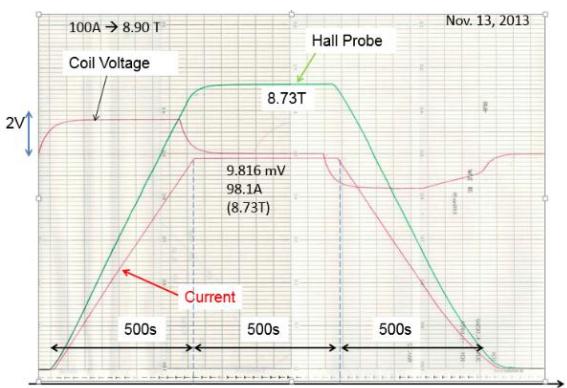
## ▪ Demonstrated the reliable performance for both main solenoid and steering dipole coils

- Solenoid has no quench up to 8.9T and no tanning
- Steering coils have no quench up to 100A (nominal 50A), no training
- No performance change post thermal cycling 12 times (RT to LN<sub>2</sub> temperature)
- Established dry winding technique

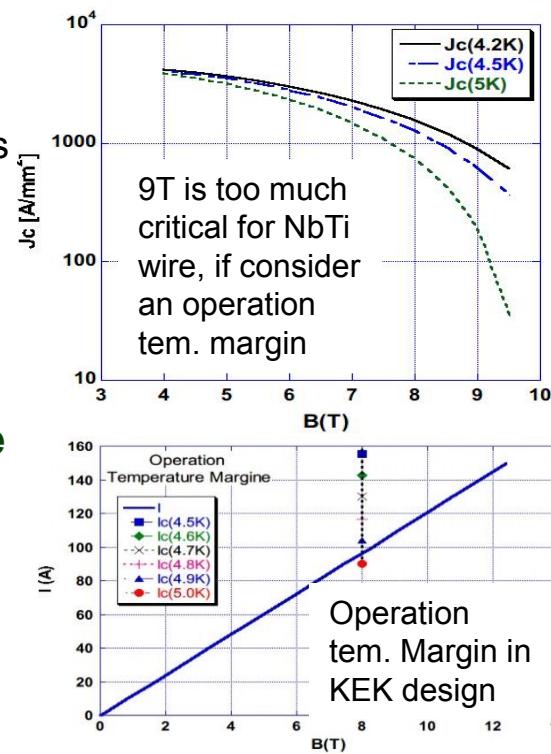


Dry winding, no use epoxy

Completed solenoid



First excitation test



Completed steering coils

Solenoid package

# Cavity/Fringe Field Interaction

A fringe field of 4G causes a Q-drop under FRIB spec. with 0.53HWR when cavity happened quench

- Meissner Shield
  - Cavity performance no change up to 2500G fringe field, if no quench happens

- Cavity performance no change up to 2500G fringe field, if no quench happens

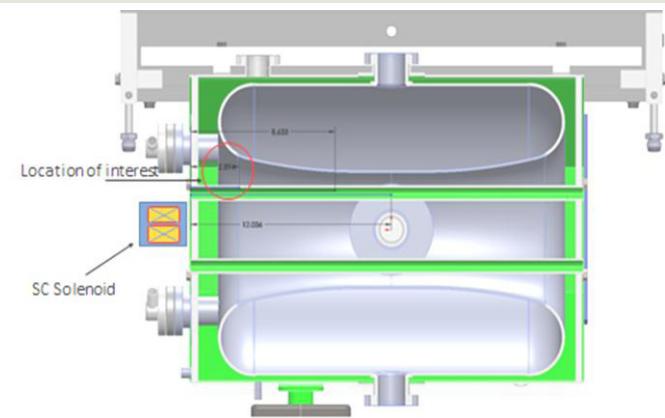
- $Q_o$ - drop by the Quench

- $Q_o$  drops under the FRIB specification (HWR) at  $> \sim 4G$  of fringe field
- Flux trapping by quench is proportional to the increased fringe field strength

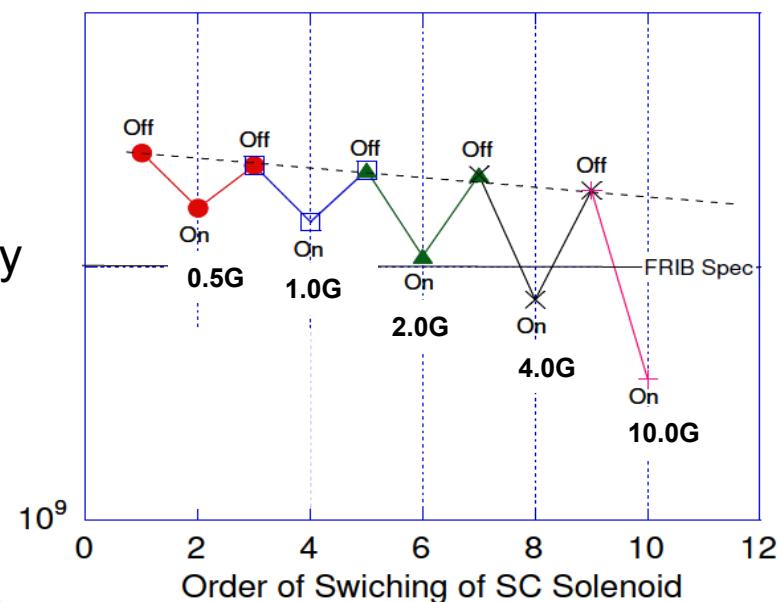
- “Annealing effect” (discovered at FNAL, by T. Khabiboulline, et al.)

- Confirmed “annealing effect” against the  $Q_o$ -drop by a quench under
- “Annealing effect” can be use the  $Q_o$  recovery

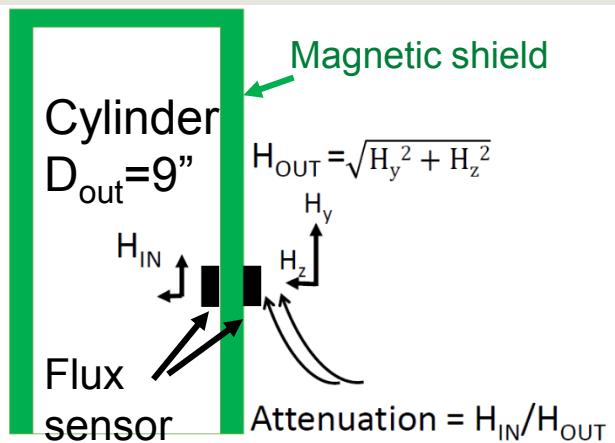
**“Annealing effect”:** when a  $Q_o$ -drop happened by cavity quench, switch off the solenoid and repeat RF processing, then  $Q_o$  recovers (FNAL).



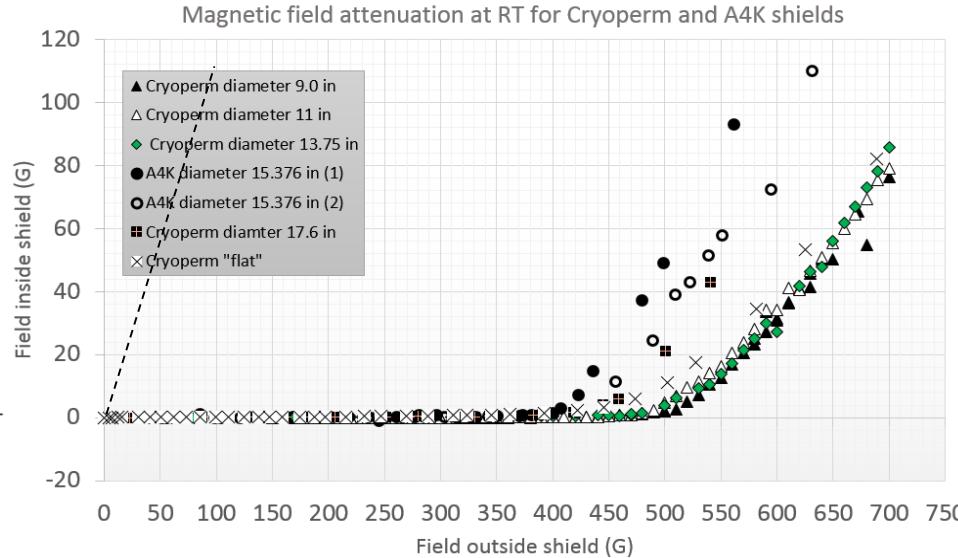
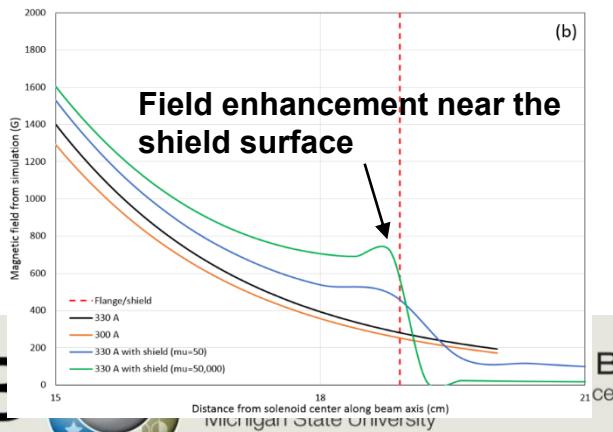
$Q_o$ -drop and Annealing effect @ Eacc=7.5MV/m



# Saturation Field Measurement at FRIB



- The saturation field, which is defined at the external field produced 1G inside shield was measured.
- Saturation field is 365 at R.T. for A4K for instance
- Field enhancement on the shield surface by a factor 2

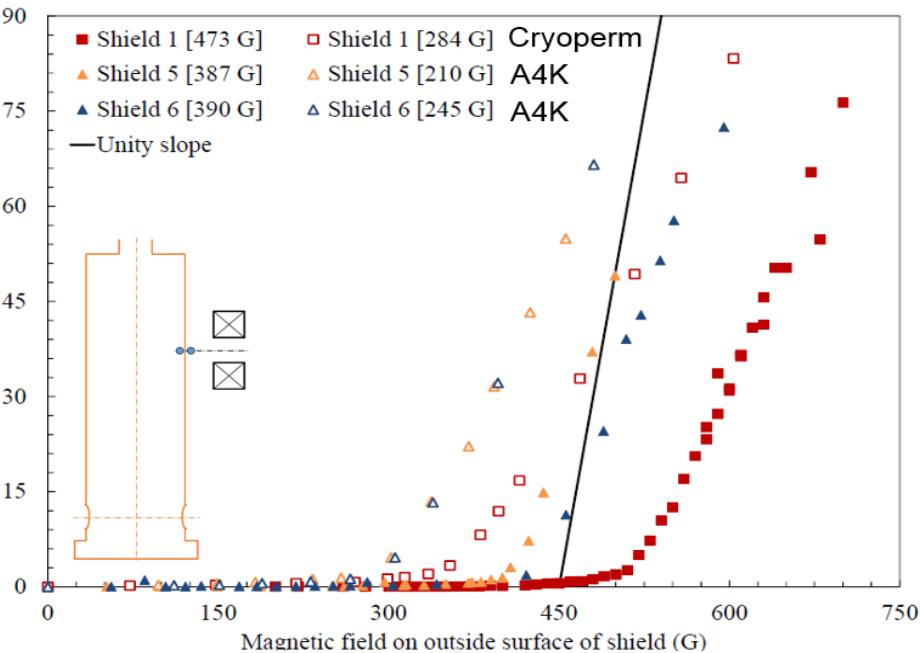


Material	Thickness (mm)	Diameter (cm)	Height (cm)	Saturation* (G)
Cryoperm	1.0	34.9	30.5	472
Cryoperm	1.0	21.6	99.1	470
Cryoperm	1.0	27.9	70.6	475
Cryoperm	1.0	44.7	38.9	450
Cryoperm	1.0	Flat		390
A4K (ReA6#1)	1.0	39.0	86.4	368
A4K (ReA6#2)	1.0	39.0	86.4	365

\* Saturation field is defined at 1G increase

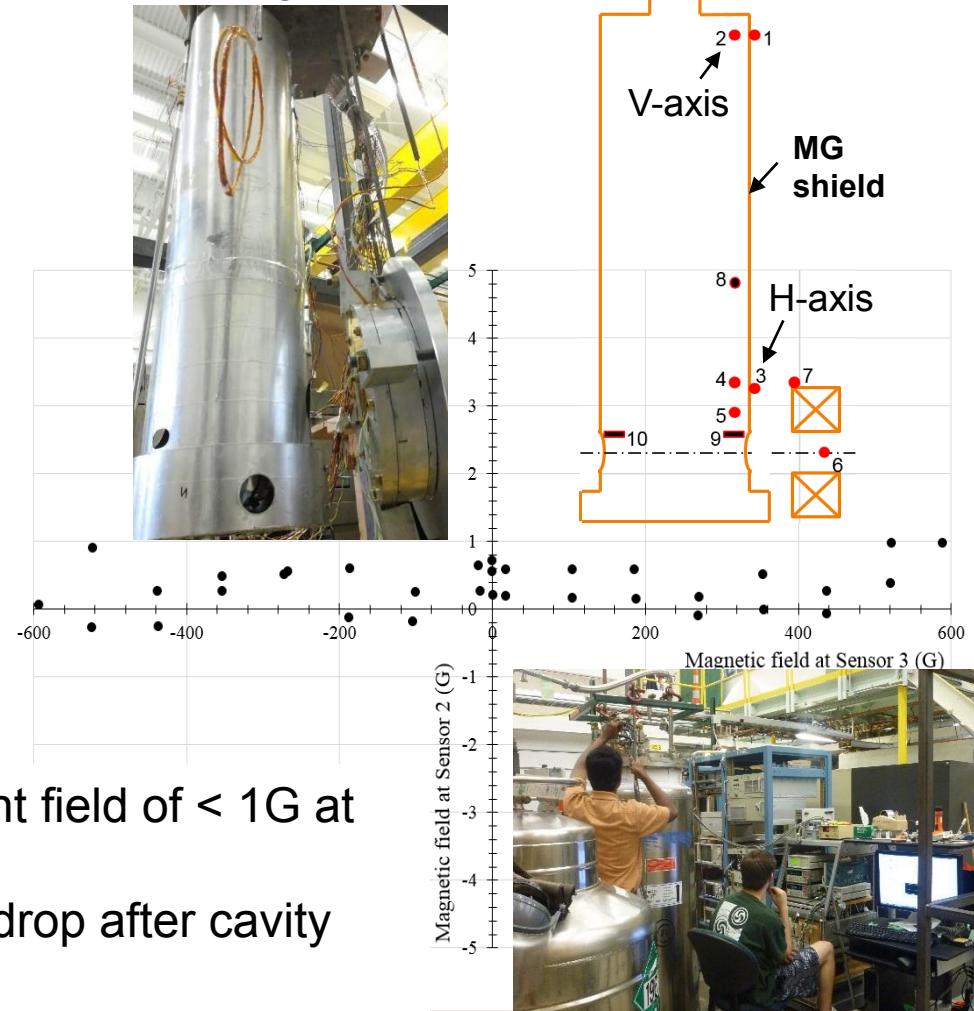
# Cold Measurement of Magnetic Shield Property

Saturation Field Measurement at 10K



$$\text{Atten}_{\text{cryo}} \approx 0.68 \cdot \text{Atten}_{\text{RT}}$$

Field Strength Inside Shield

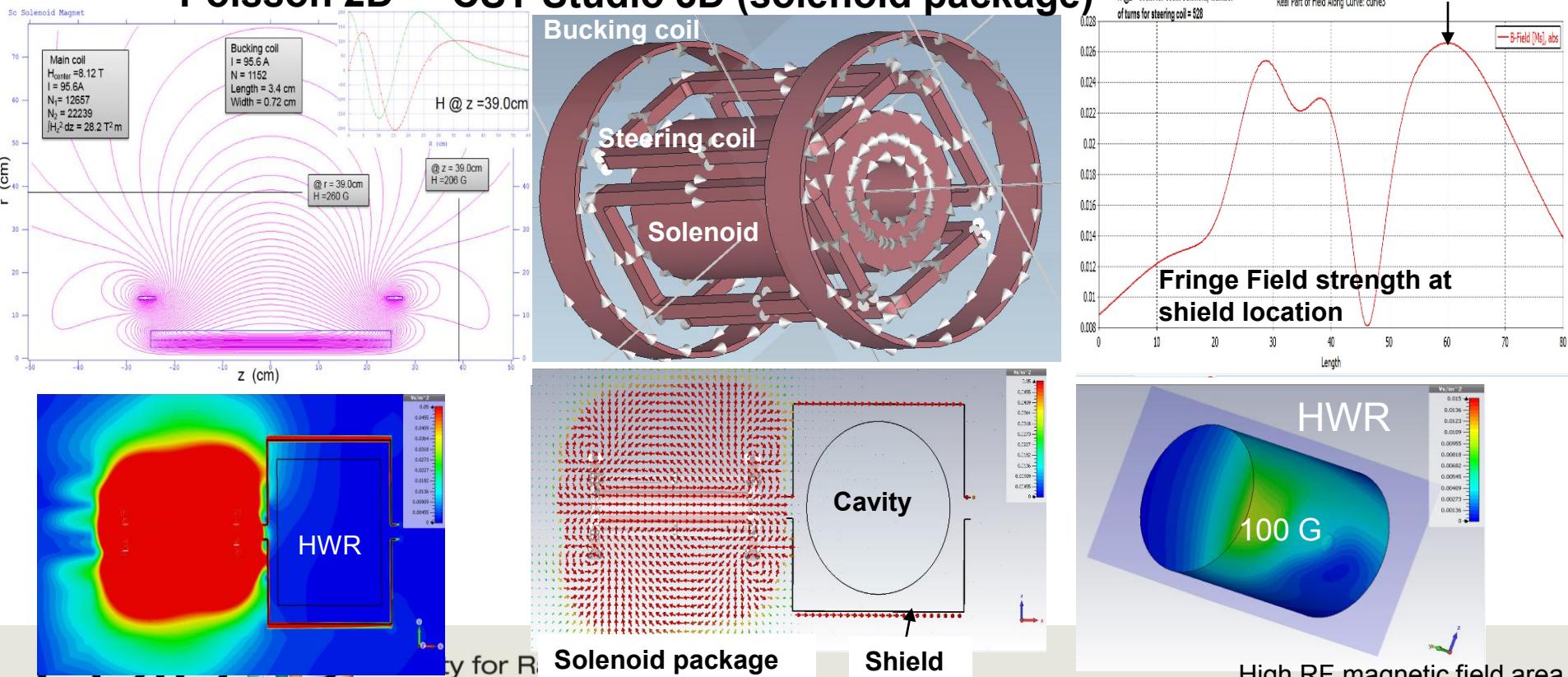


- Fringe field of 600G produces a remanent field of < 1G at high RF magnetic field area of QWR
- QWR will be no problem even for the Q-drop after cavity quench

# Fringe Field Simulation on the Cavity Wall

- Iron yoke free solenoid design has been completed with bucking coil
- 3D simulation by CST Studio shows the fringe field of 270G on the magnetic shield
- Fringe field of 100G exposes the high RF magnetic area
- Backup plan is being developing for Q-drop after quench, Meissner shield by niobium foil around the helium vessel might be a cure, which will be studied in the integration test

Poisson 2D    CST Studio 3D (solenoid package)



# Summary

- FRIB SRF components have been all designed and prototyped and successfully validated.
- Integration test at vertical Dewar is under preparation for final validation
- Cavity/fringe field interaction is well understood and a backup plan is under developing against the Q-drop at quench for reliable FRIB operation
- Cryomodule prototyping is going very steadily
- SRF highbay has been constructed and the infrastructure are being installed. Accelerator system construction will start October 2014