

September 3, 2014

Chopping High-Intensity Ion Beams at FRANZ

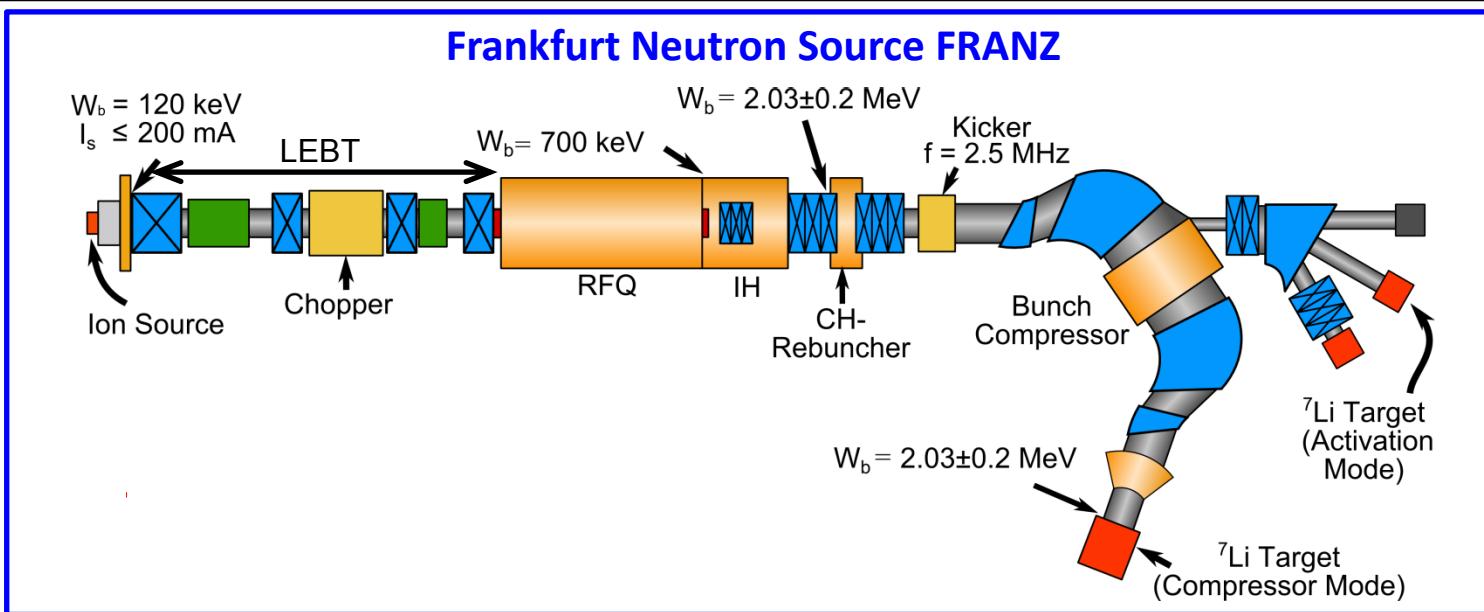
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O. Payir, U. Ratzinger, P. Schneider
IAP, Goethe-Universität Frankfurt am Main



Outline

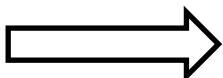
- 1) Introduction: The FRANZ facility
- 2) Chopper System
 - a) ExB Chopper Concept
 - b) Numerical Simulations
 - c) Experimental Results
- 3) Conclusion

Introduction: FRANZ



Goal (*Compressor Mode*):

- Deliver a high (peak) neutron flux,
- produced via the $^7\text{Li}(p,n)^7\text{Be}$ reaction,
- for the energy-dependent measurements of n-capture cross sections (using TOF).

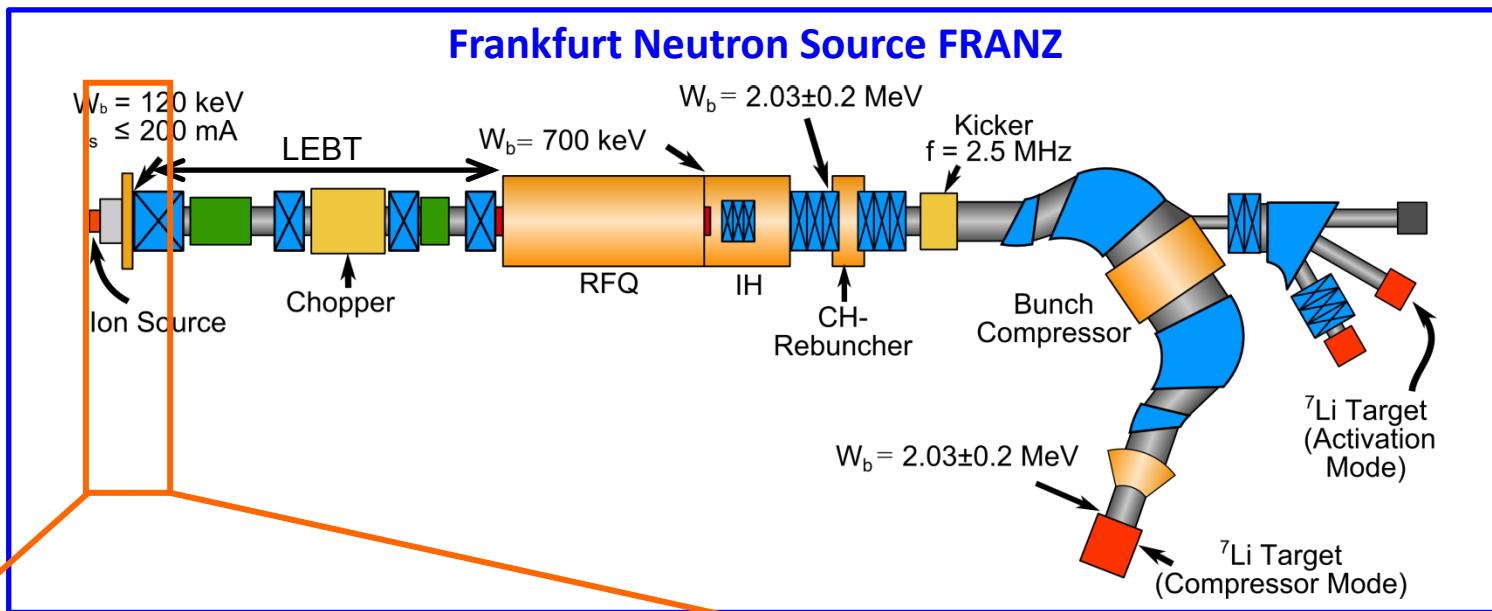


This requires a primary proton beam

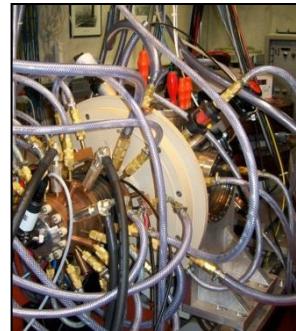
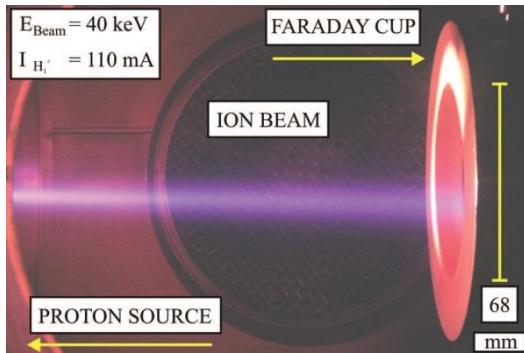
- with high intensities (50-200 mA),
- at 2 MeV beam energy,
- with a challenging time structure (1 ns, 257 kHz).



Introduction: FRANZ



High-Current Ion Source

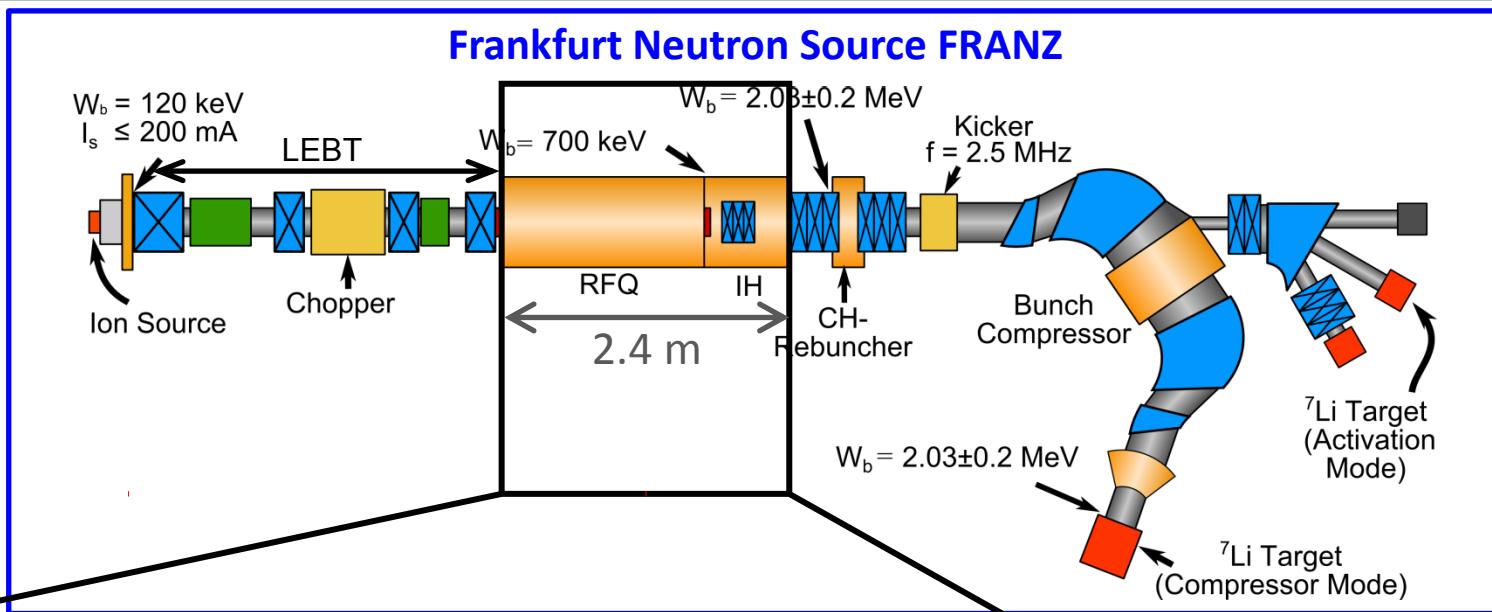


© K. Volk, W. Schweizer

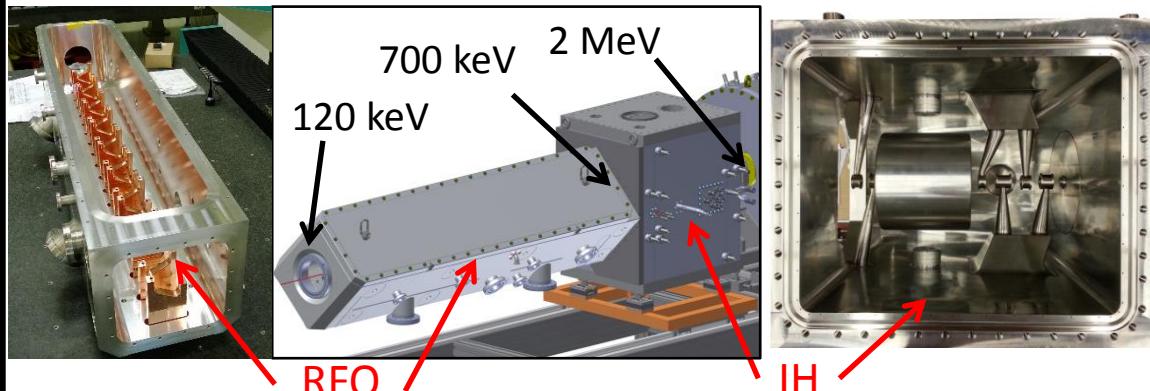
- Arc-discharge driven ion source
- Proton current: 50 mA (240 mA)
- DC operation
- Proton fraction > 90 %
- Beam energy: 120 keV
- Triode extraction system



Introduction: FRANZ



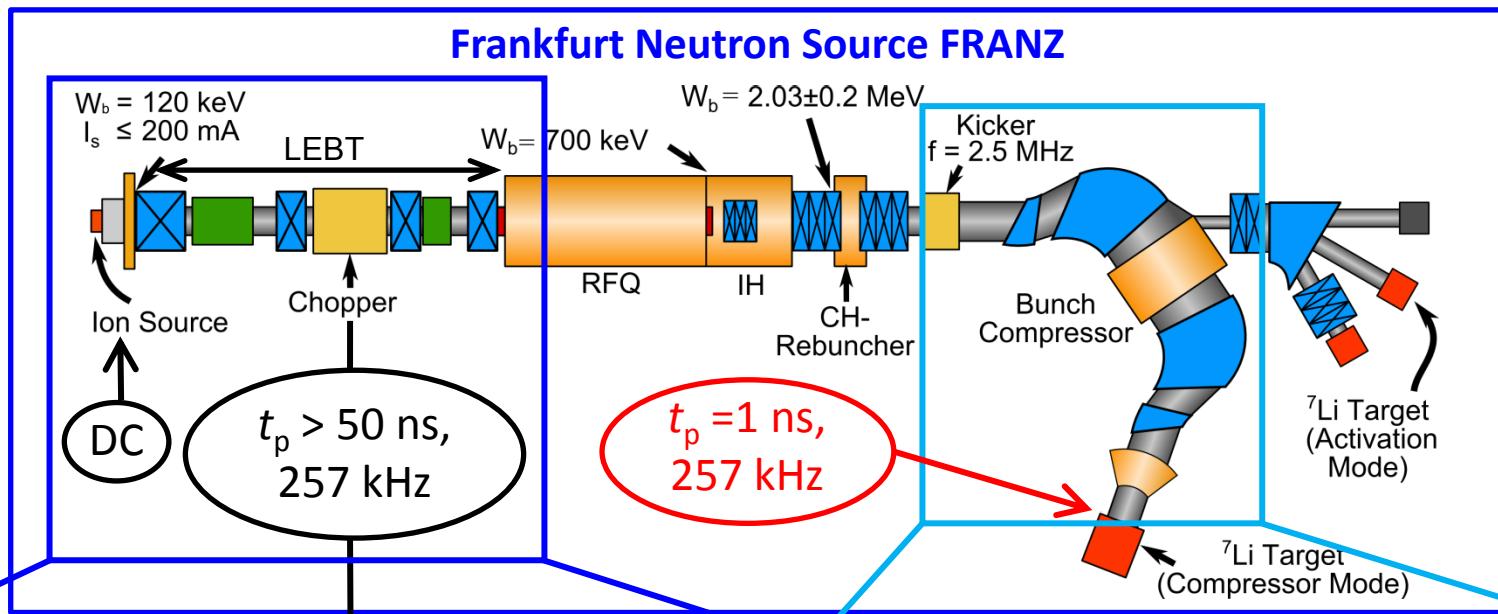
2 MeV Linac Section



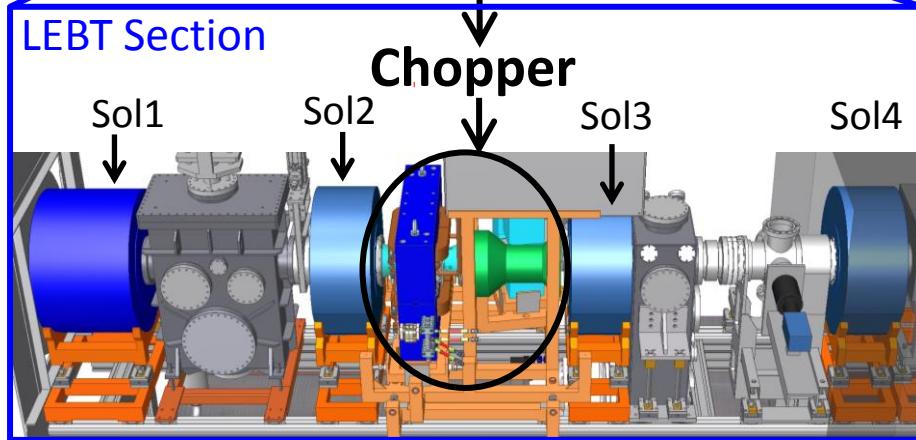
- CW operated
- $f_{rf} = 175 \text{ MHz}$
- RFQ under construction
- IH to be copper plated
- RFQ test module tested with $P_{rf} \approx 115 \text{ kW/m}$



Introduction: FRANZ

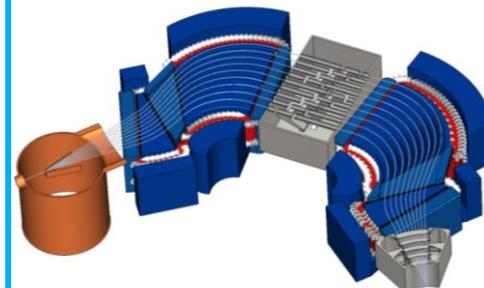


LEBT Section



Chopper

Bunch Compressor



- Mobley Type
- Electric Kicker ($f = 2.5 \text{ MHz}$)
- Magnetic Guiding System
- Rebuncher Cavities

ExB Chopper: Motivation

Requirements: Chopping a dc beam at

- *low energy* (120 keV)
- *high intensity* (50 mA)
- *high repetition rate* (257 kHz),
- *producing a short beam pulse*: 50 ns / 3.9 μ s.

Electric Deflection

Disadvantages: Risk of voltage breakdowns, especially at high beam intensities and especially for high duty cycles for the electric deflection field.

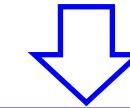
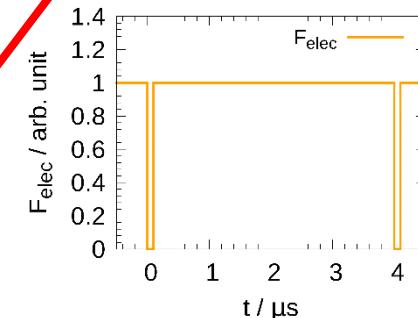
Magnetic Deflection

Disadvantages: High power consumption, especially at high repetition rates.

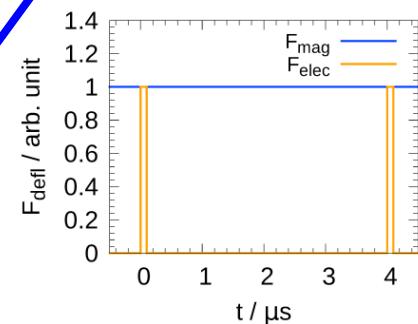
Concept

Combining pulsed electric and static magnetic deflection in an ExB (Wien-filter) field configuration.

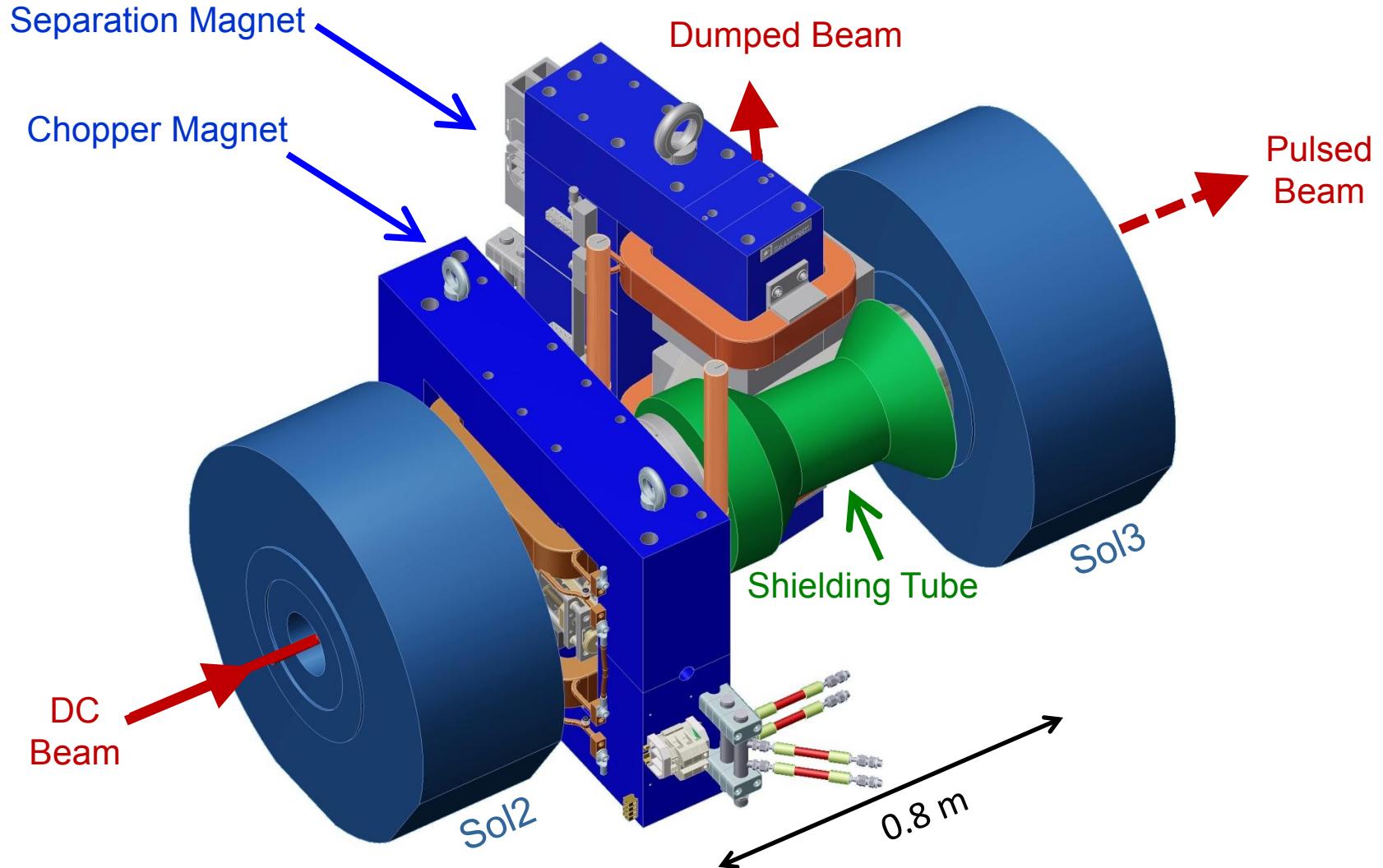
High duty cycle for electric field.



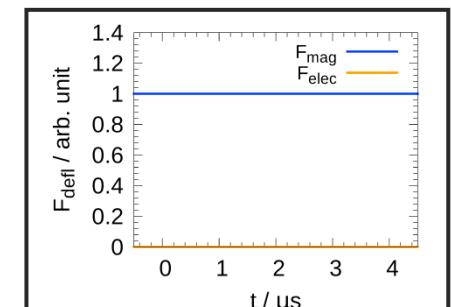
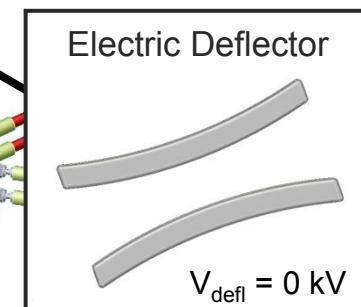
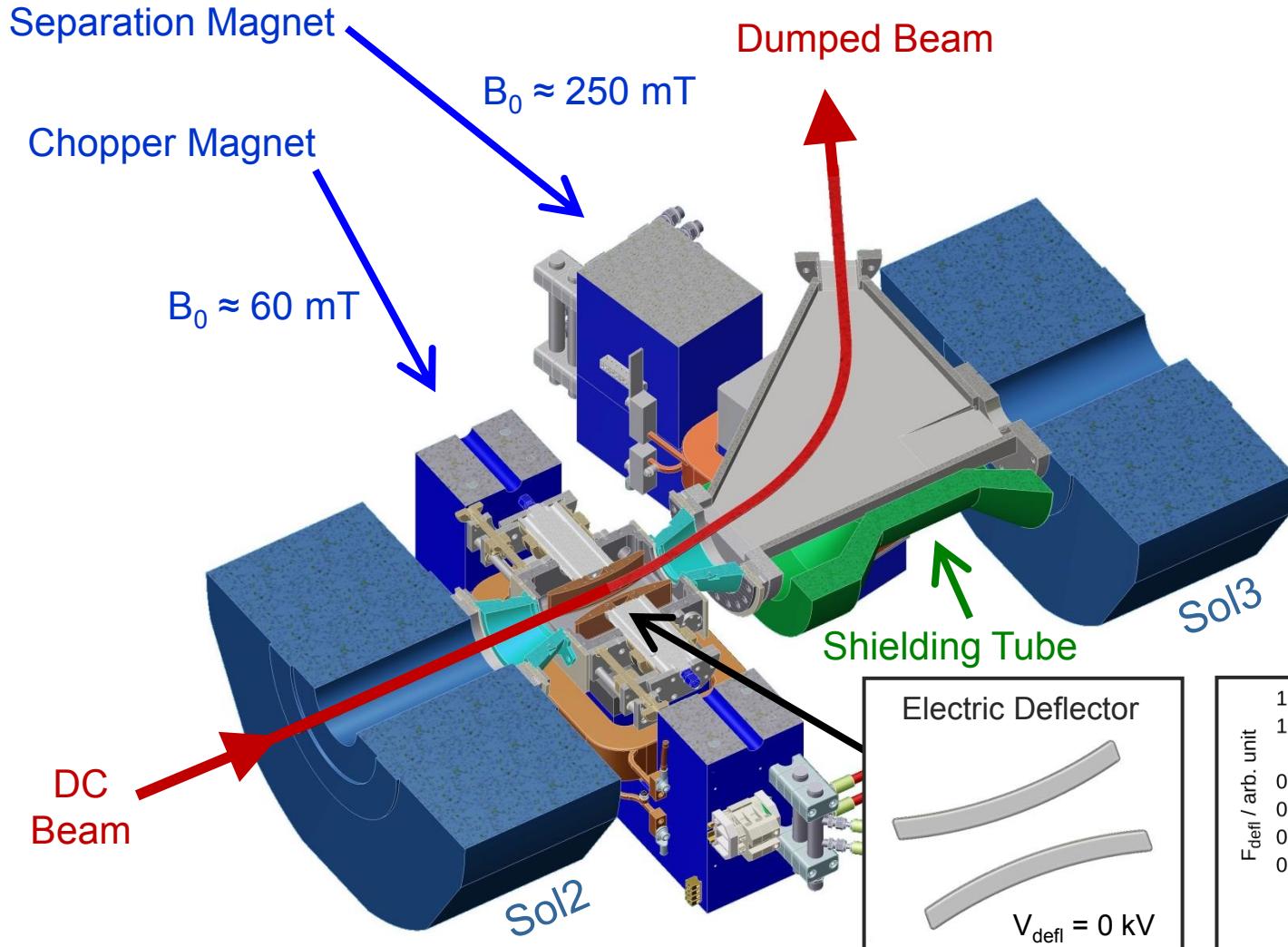
Low duty cycle for electric field.



ExB Chopper: Concept



ExB Chopper: Concept



ExB Chopper: Concept

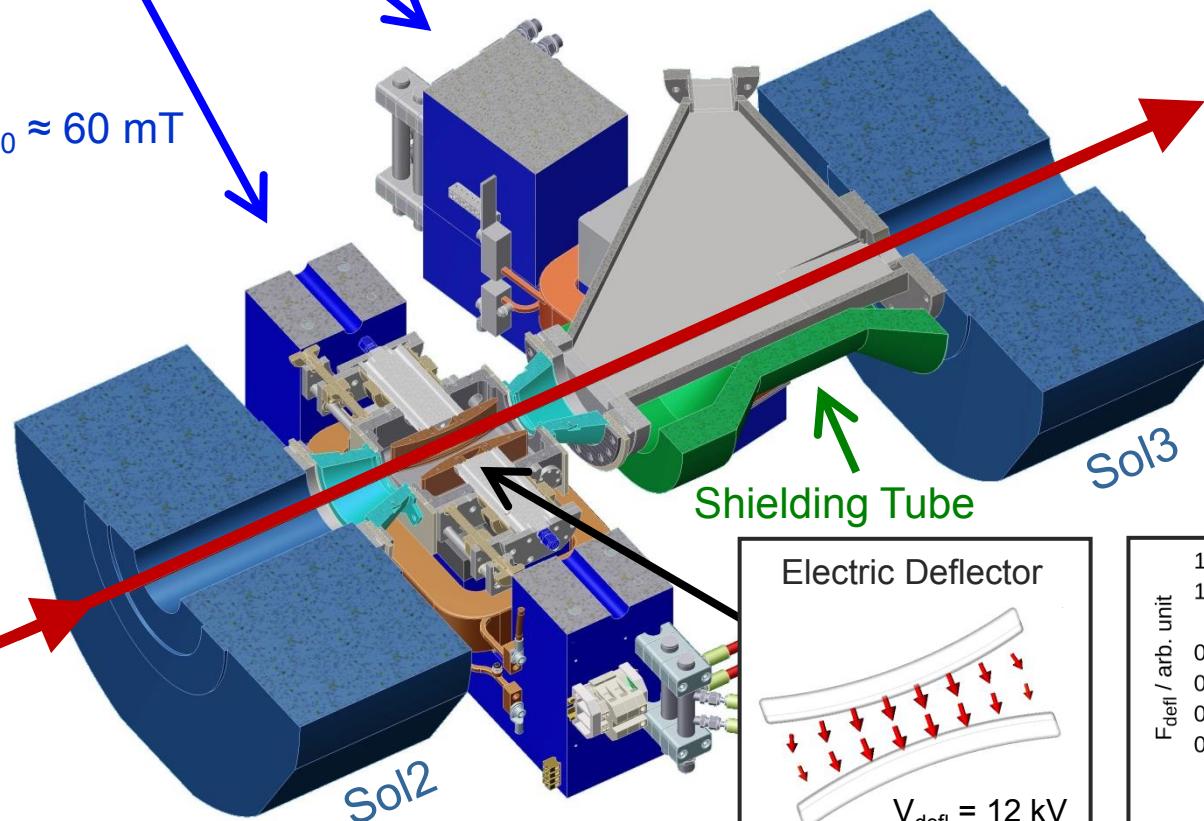
Separation Magnet

$B_0 \approx 250$ mT

Chopper Magnet

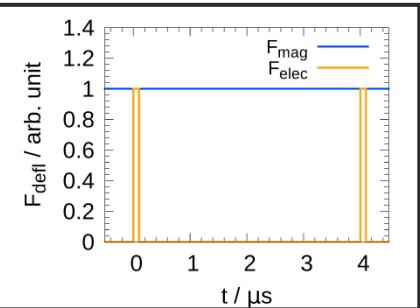
$B_0 \approx 60$ mT

DC Beam



$$\int (\vec{F}_{\text{elec}} + \vec{F}_{\text{mag}}) \ dz \stackrel{!}{=} 0$$

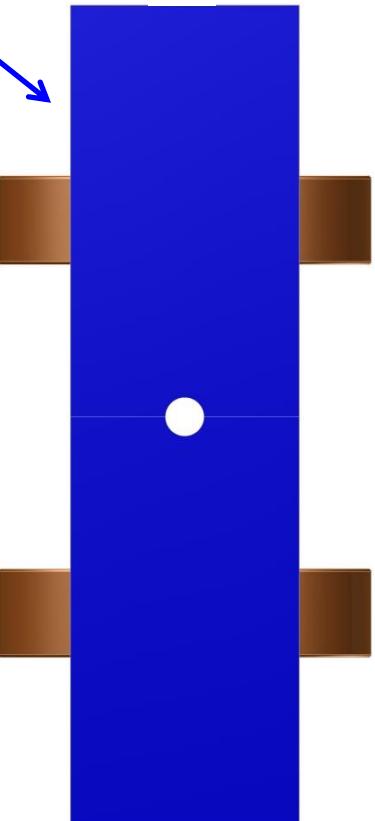
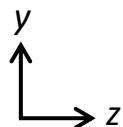
Pulsed Beam,
 $f_{\text{rep}} = 257$ kHz,
 $\tau = 50$ ns ... 350 ns



Beam Dynamics in Static E×B Fields

Longitudinal Matching of Deflection Forces

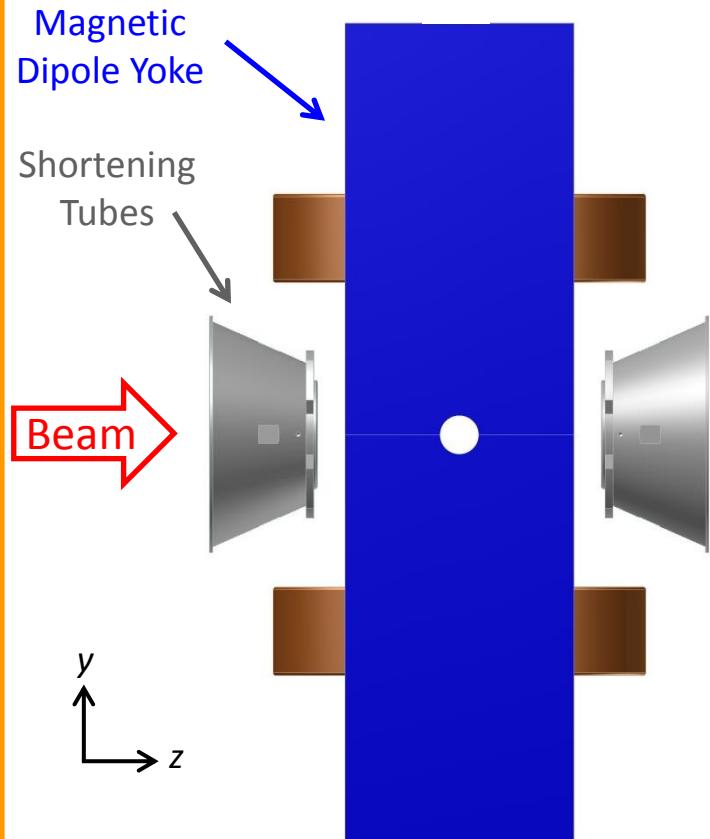
Magnetic
Dipole Yoke





Beam Dynamics in Static E×B Fields

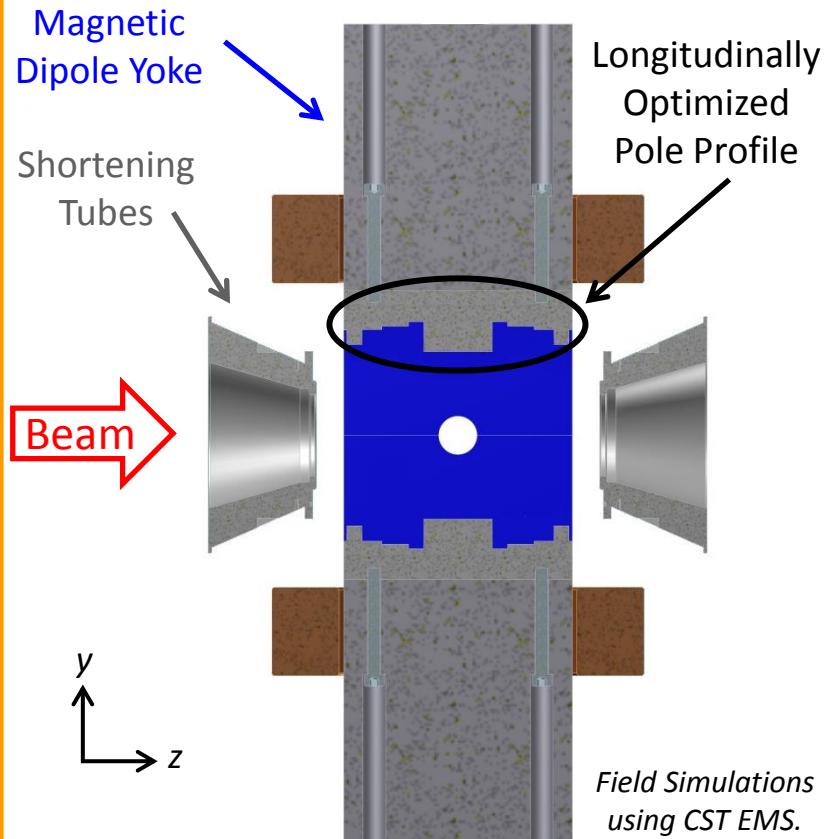
Longitudinal Matching of Deflection Forces





Beam Dynamics in Static E×B Fields

Longitudinal Matching of Deflection Forces

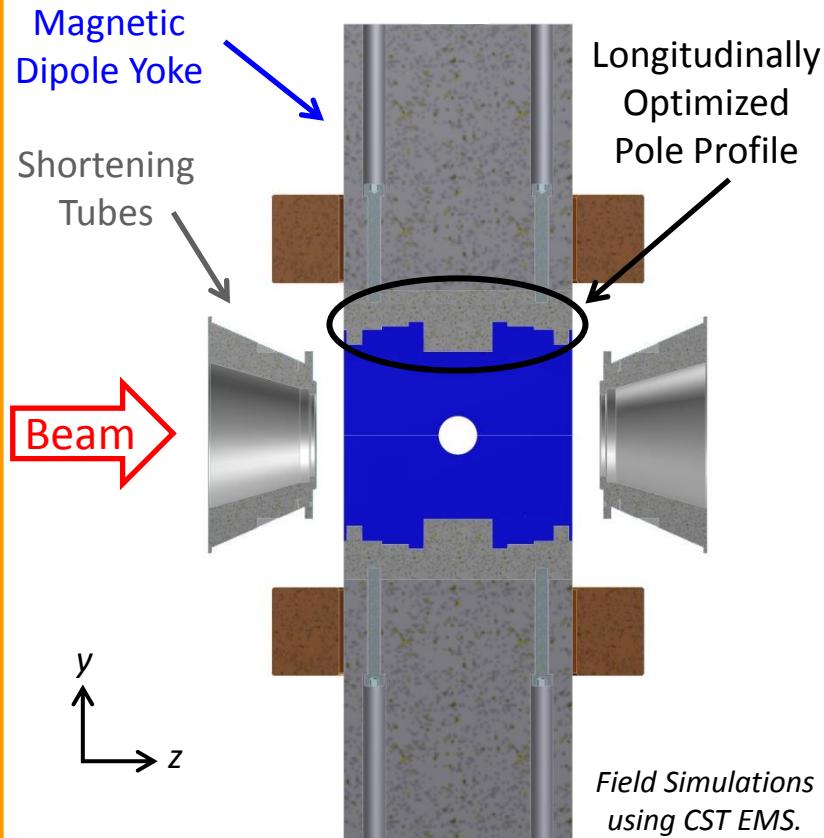


Transverse Matching of Deflection Forces

- Minimizing horizontal beam movement
- Minimizing position offset

Beam Dynamics in Static E×B Fields

Longitudinal Matching of Deflection Forces

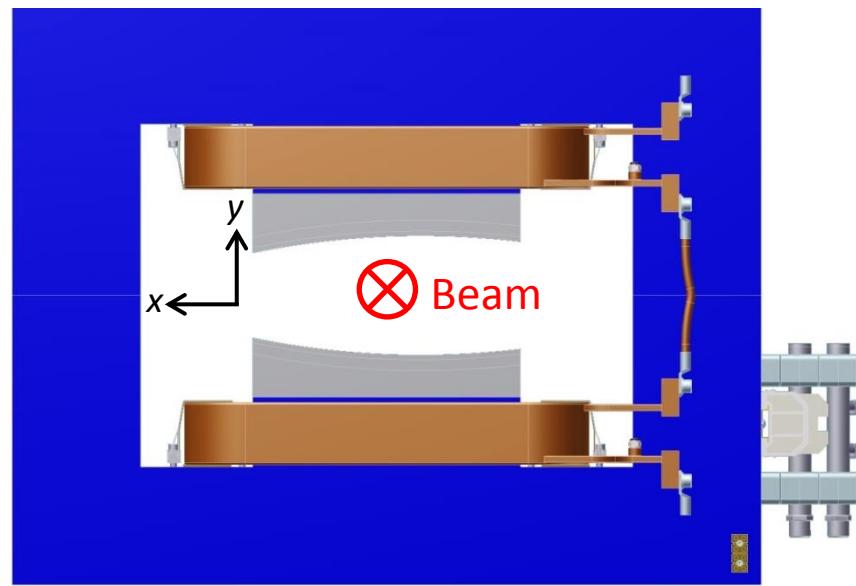


Transverse Matching of Deflection Forces

Optimized Pole Profile:

$$y(x) = \frac{1}{2} h_{gap} \cdot \frac{1}{\sqrt{1 - b \cdot \frac{E_x}{V_{acc}} \cdot x}} \cdot c \cdot x^2$$

Field Homogenization
Compensation of Velocity Change



- Minimizing horizontal beam movement
- Minimizing position offset

- Focusing in both transverse planes
- Preserving cylindrical symmetry

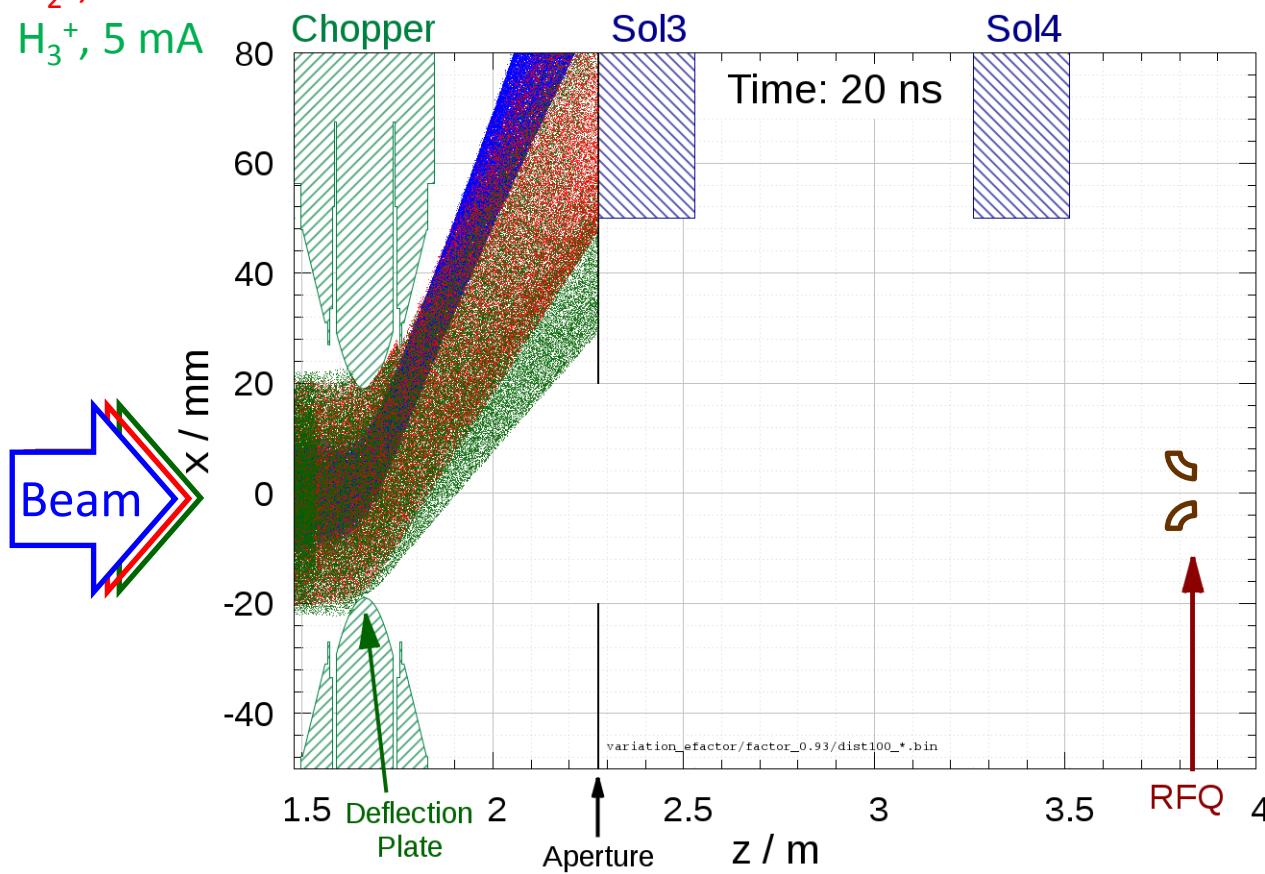


Beam Shaping Simulation

p , 50 mA

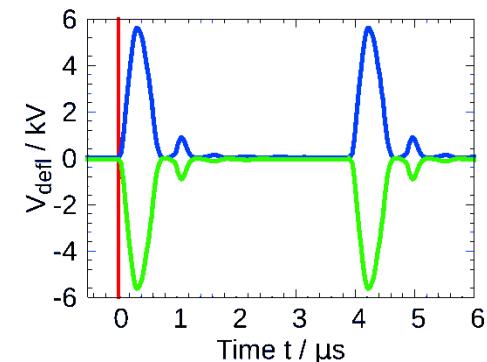
H_2^+ , 5 mA

H_3^+ , 5 mA



Input Data

- $W_b = 120 \text{ keV}$
- $I_{\text{proton}} = 50 \text{ mA}$
- Matched Input Distribution
- 3d E -field of deflect. plates
- 3d B -field of chopper magnet
- 3d B -field of solenoids
- Measured HV Pulse



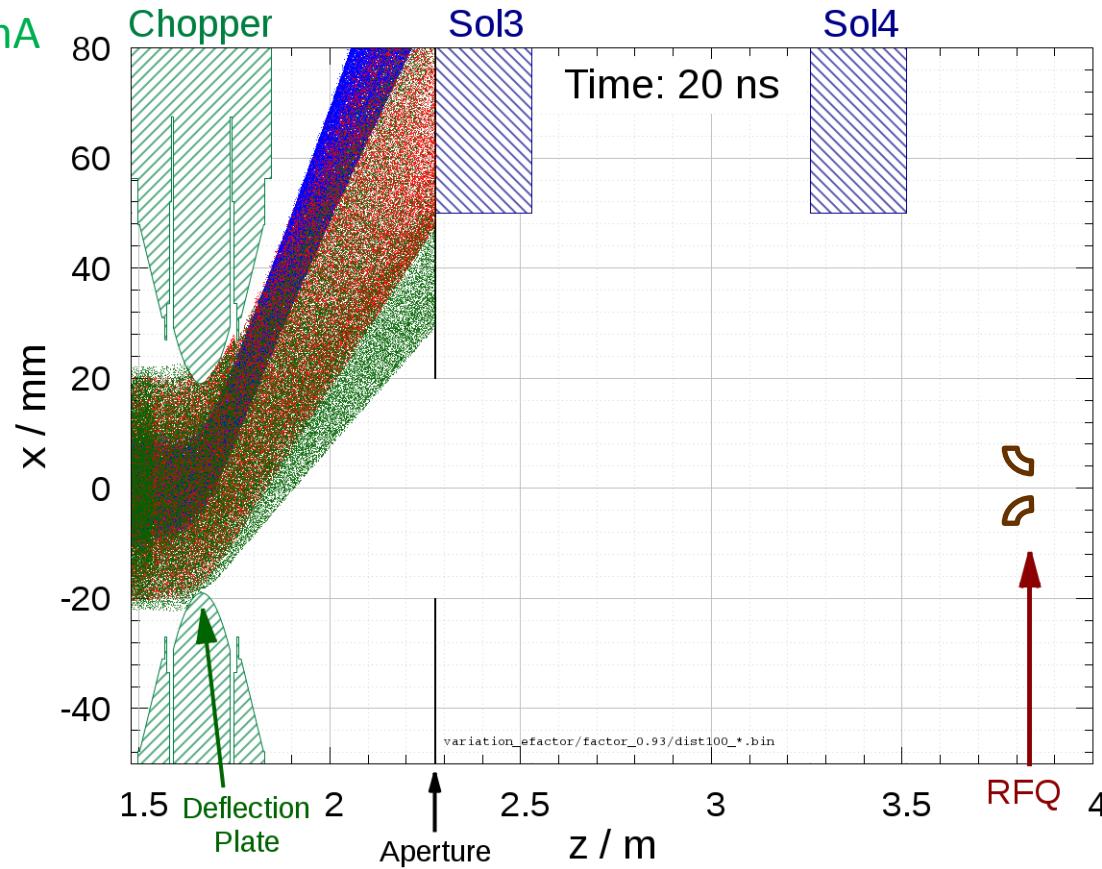


Beam Shaping Simulation

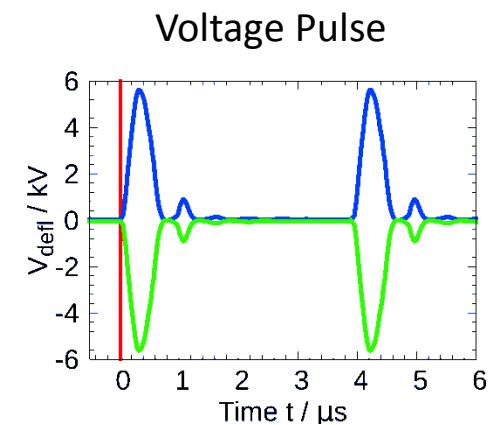
p , 50 mA

H_2^+ , 5 mA

H_3^+ , 5 mA



Beam dynamics calculations using PIC-Code Bender.



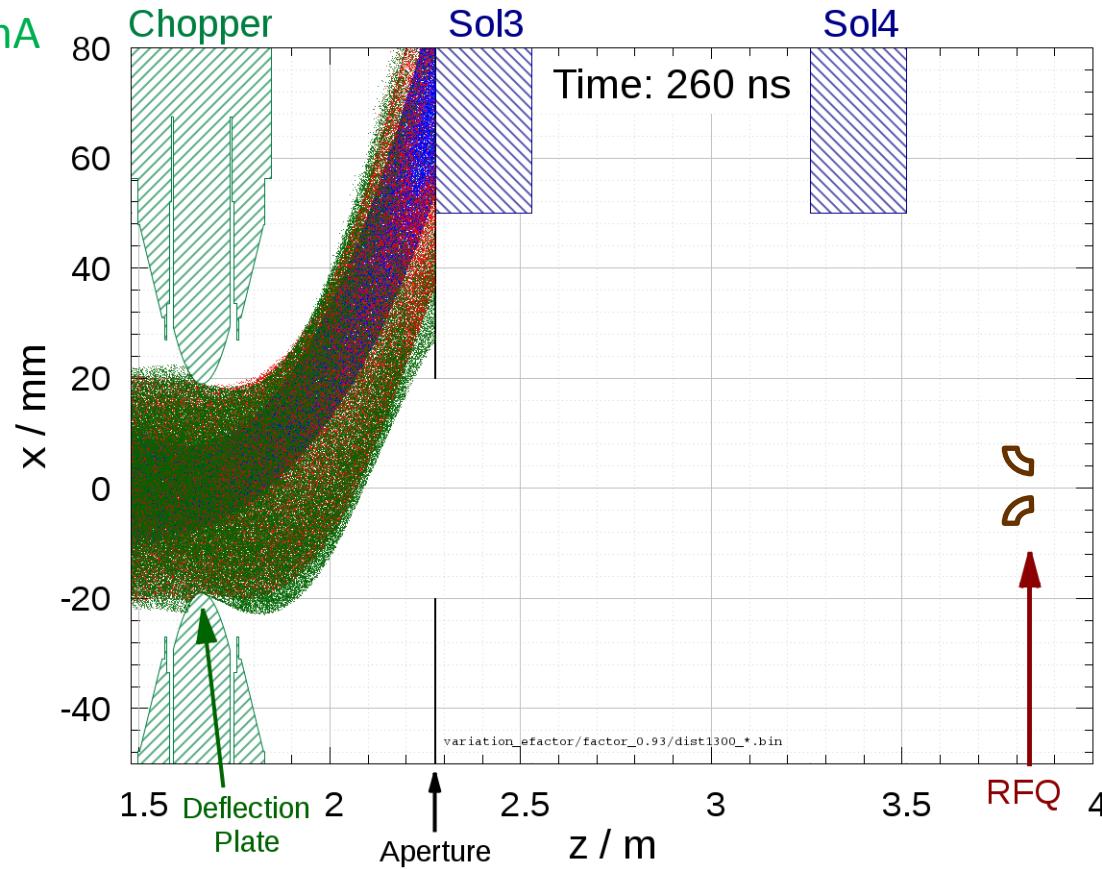


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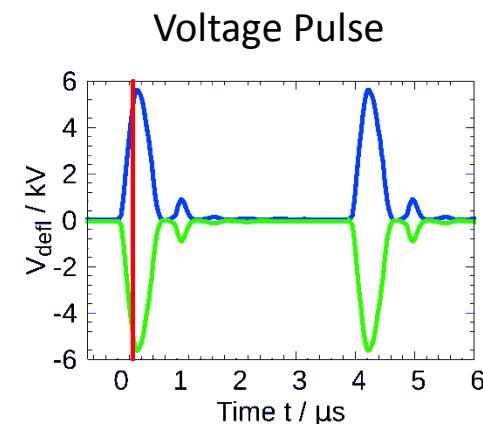
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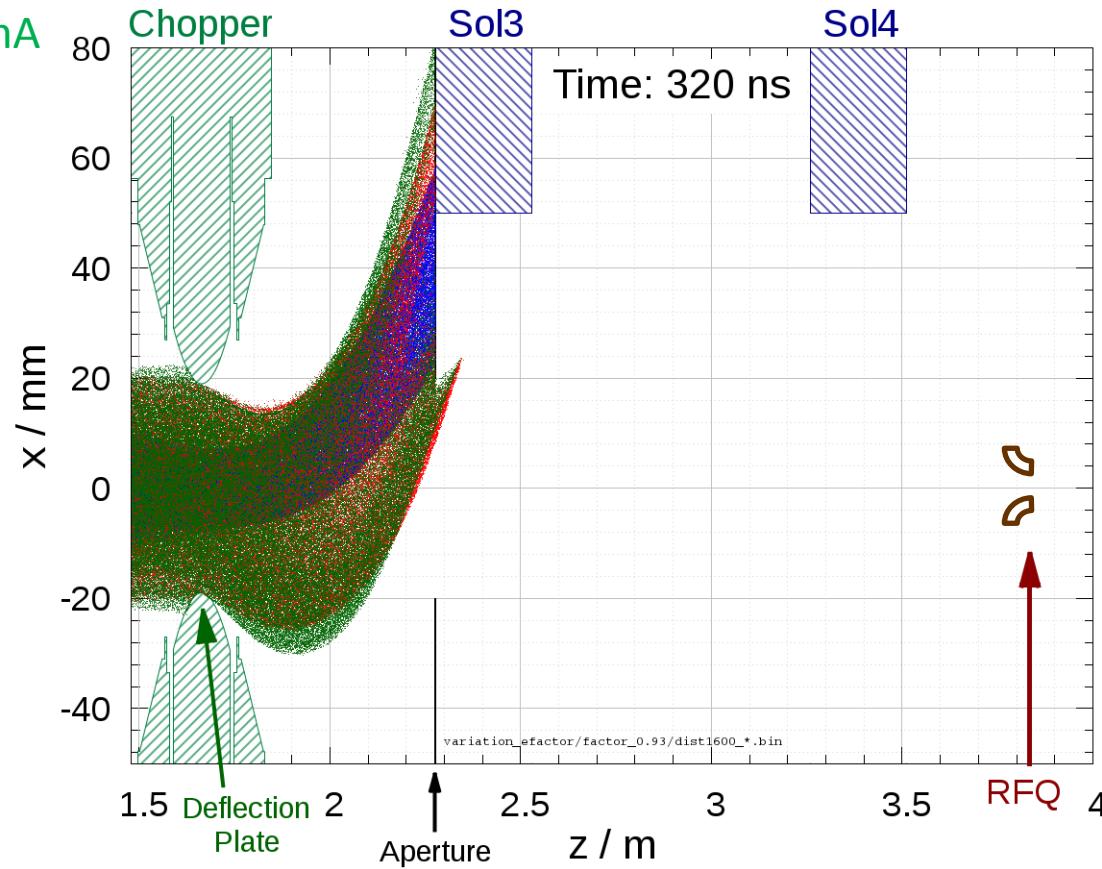


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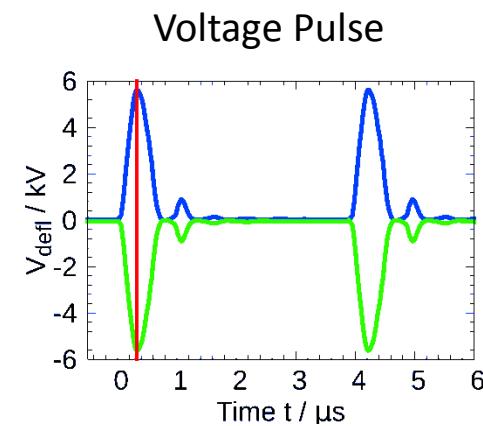
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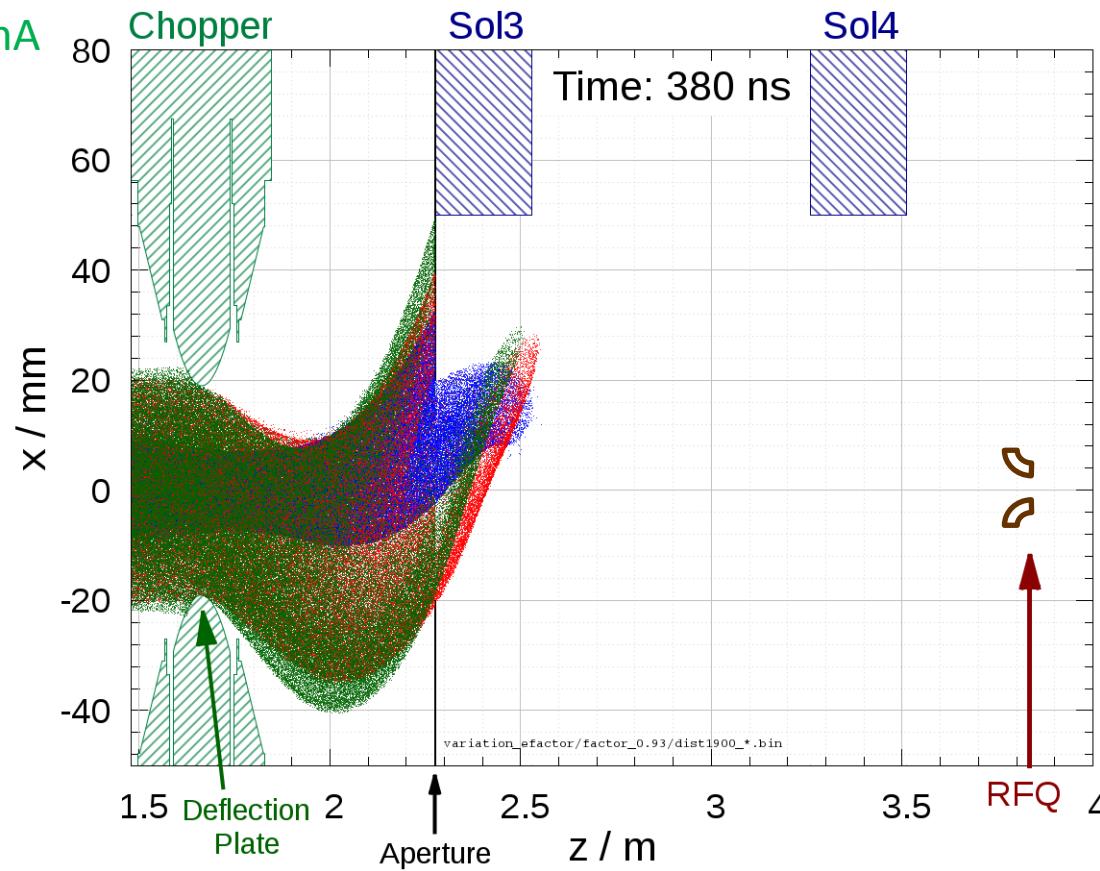


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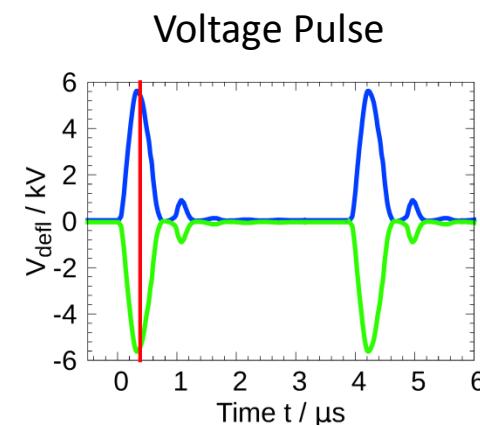
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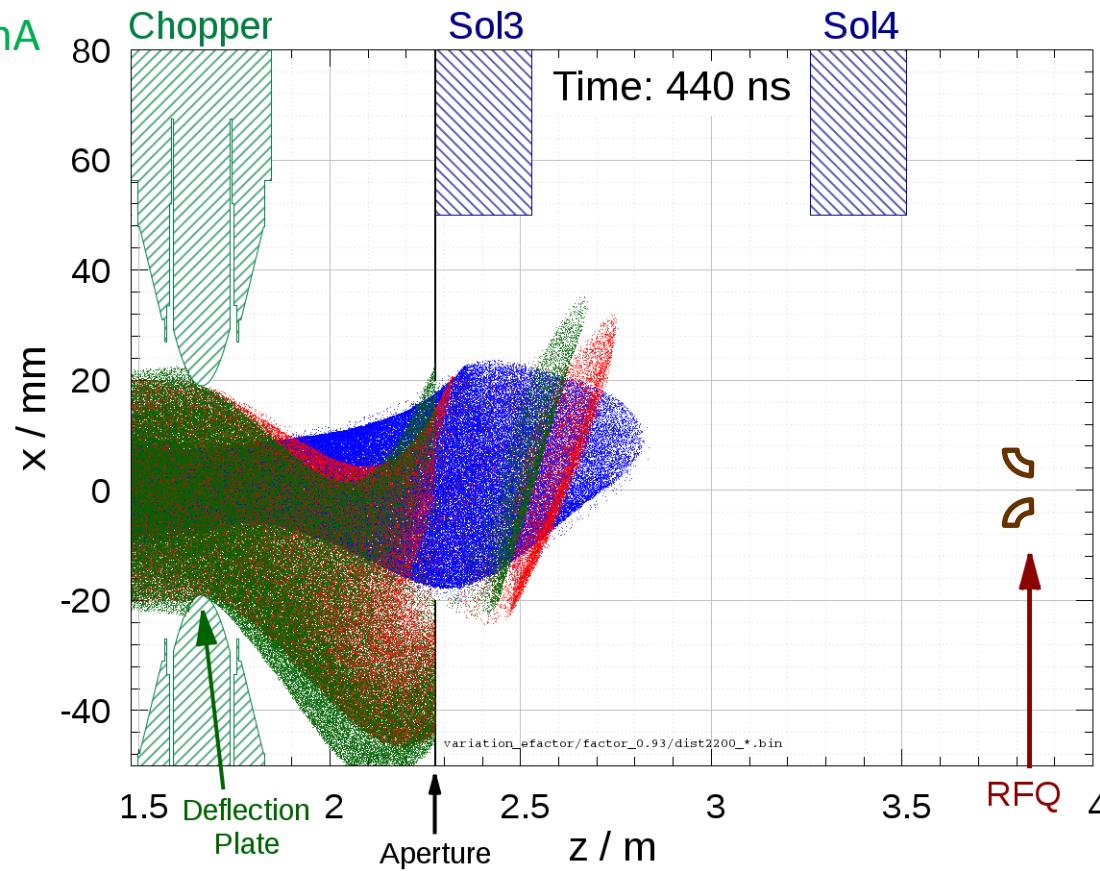


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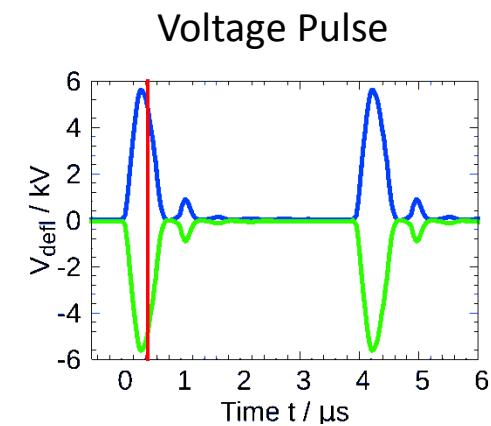
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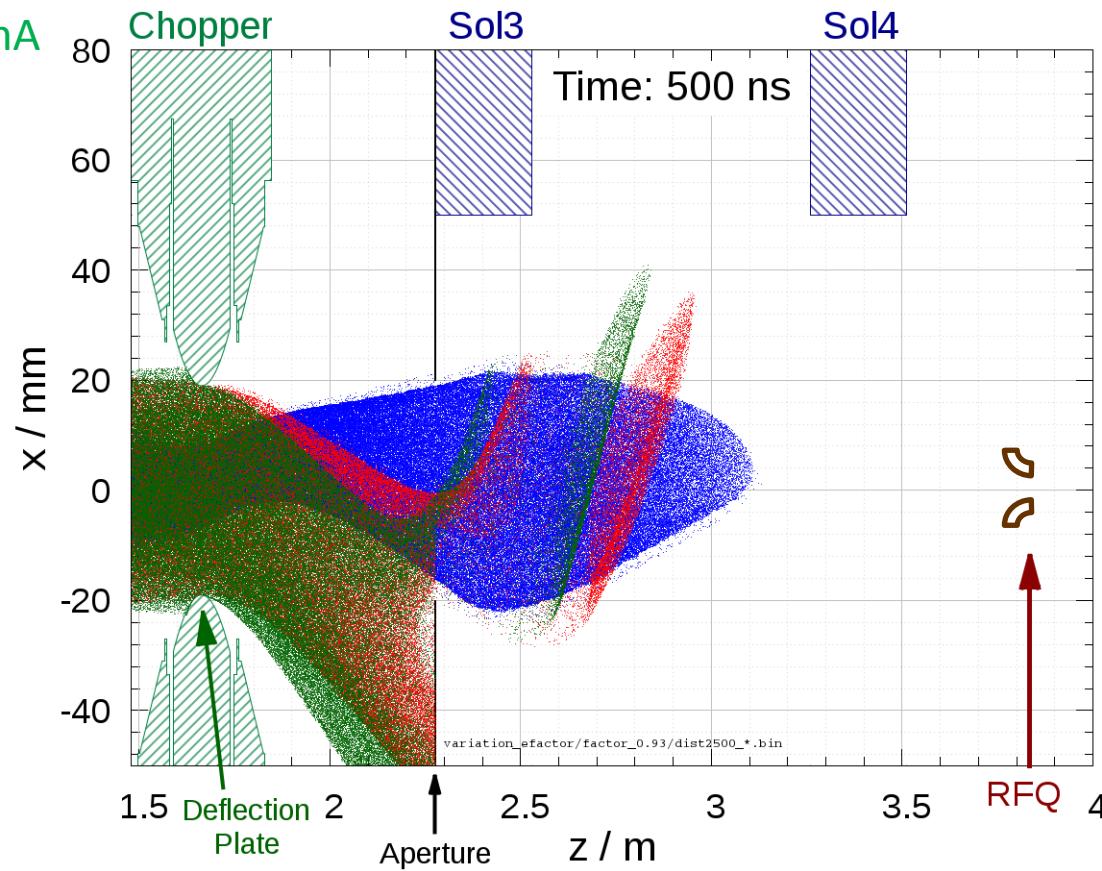


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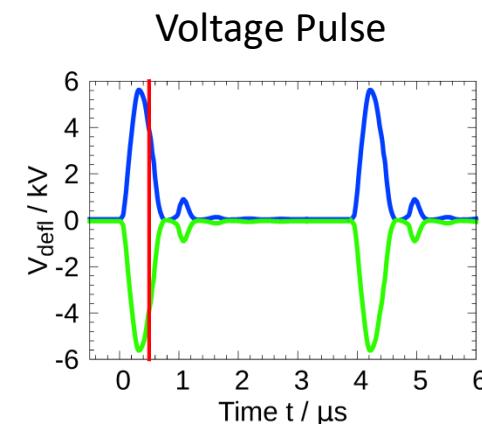
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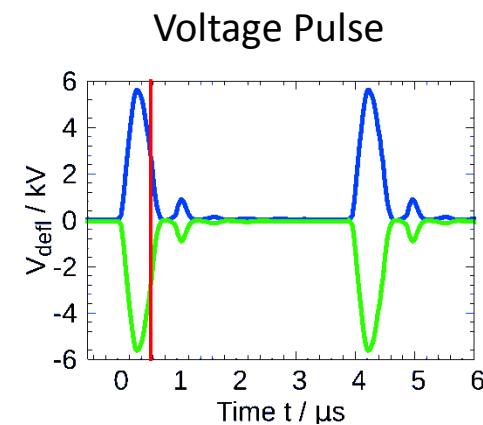
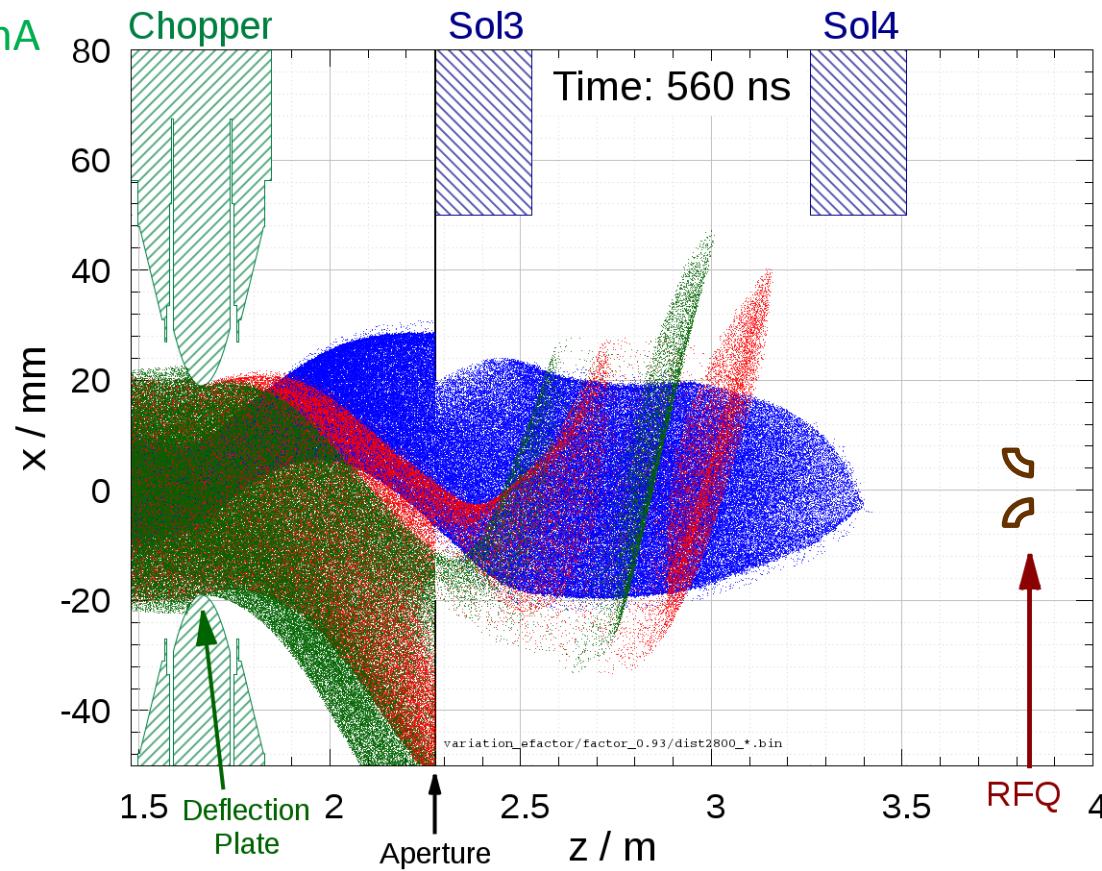


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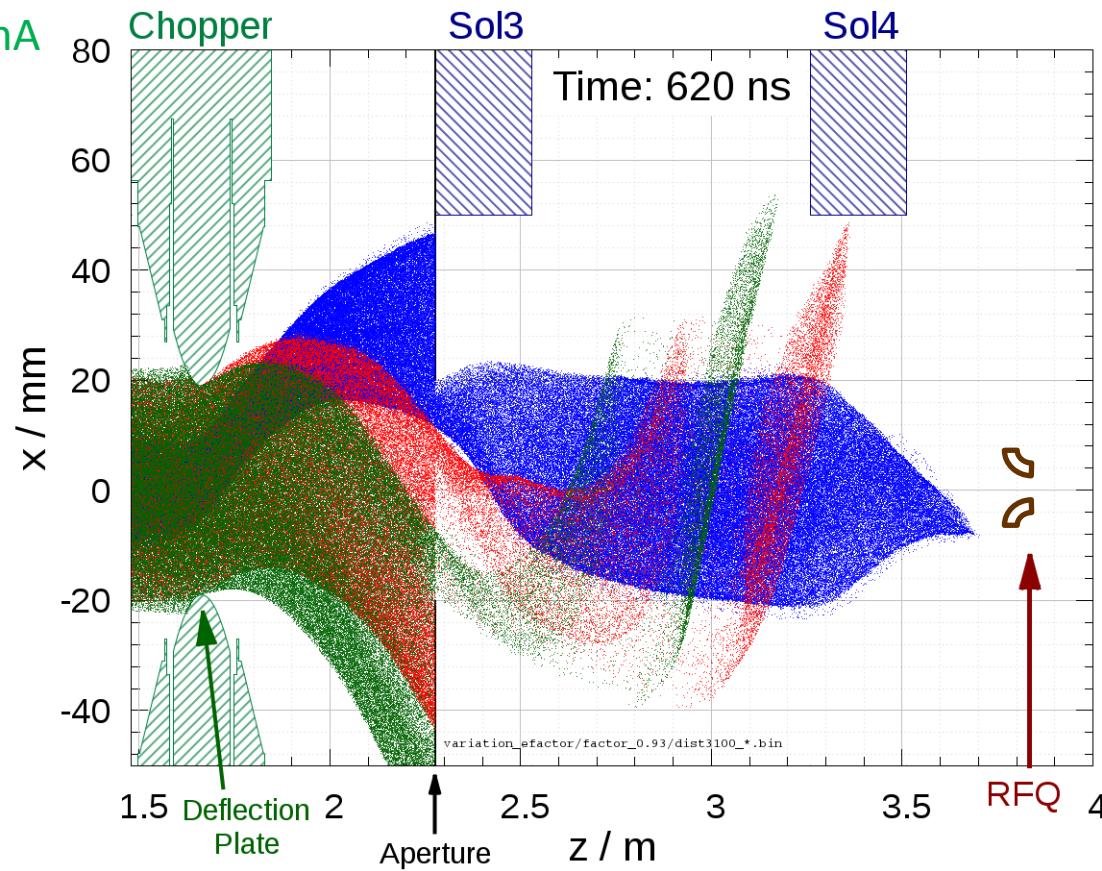


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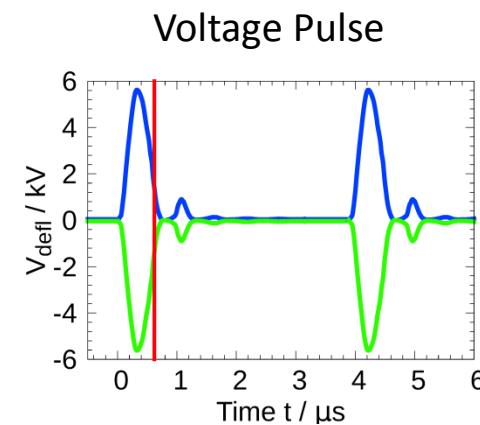
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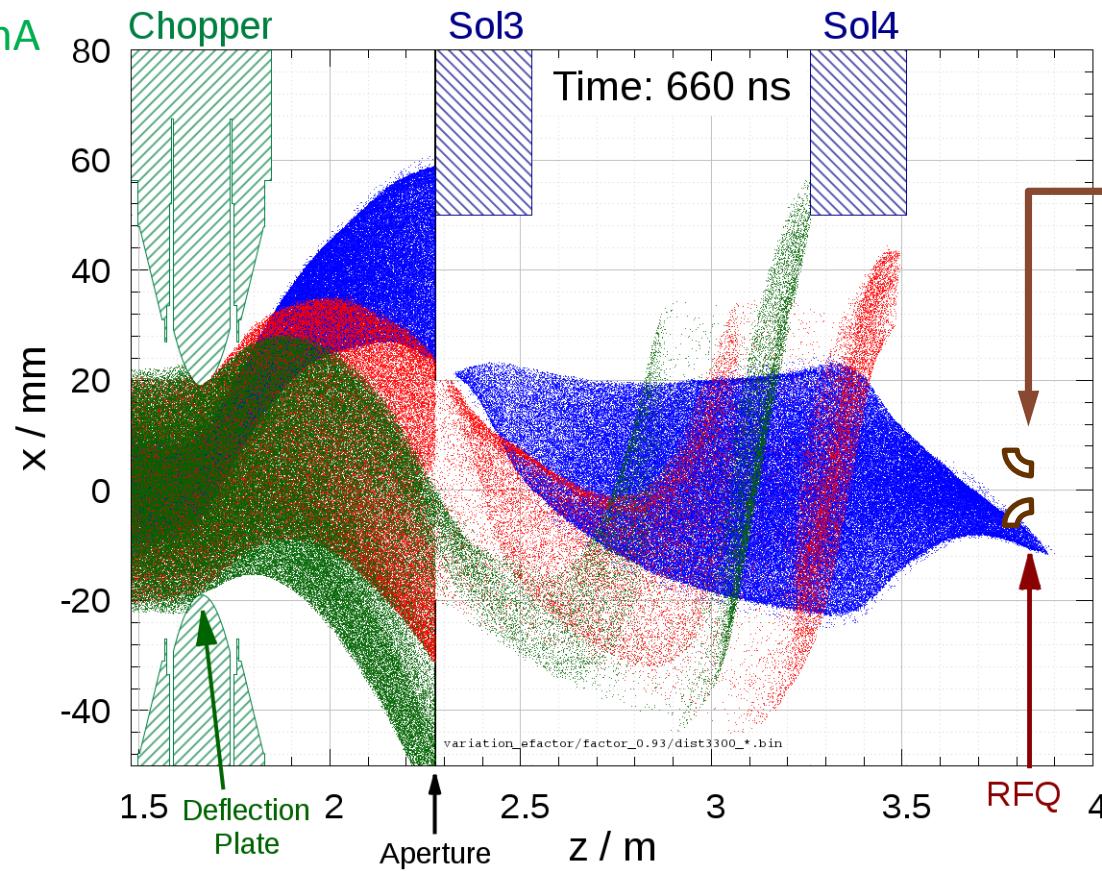


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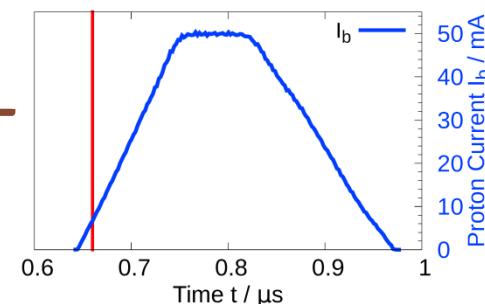
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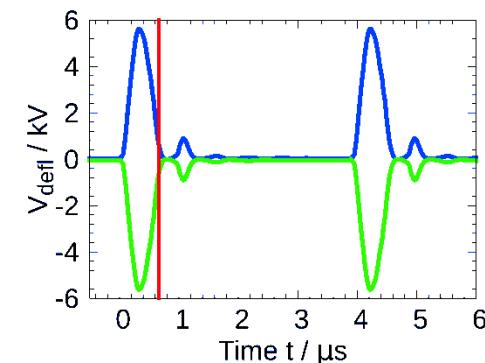
H_3^+ , 5 mA



Beam Pulse



Voltage Pulse



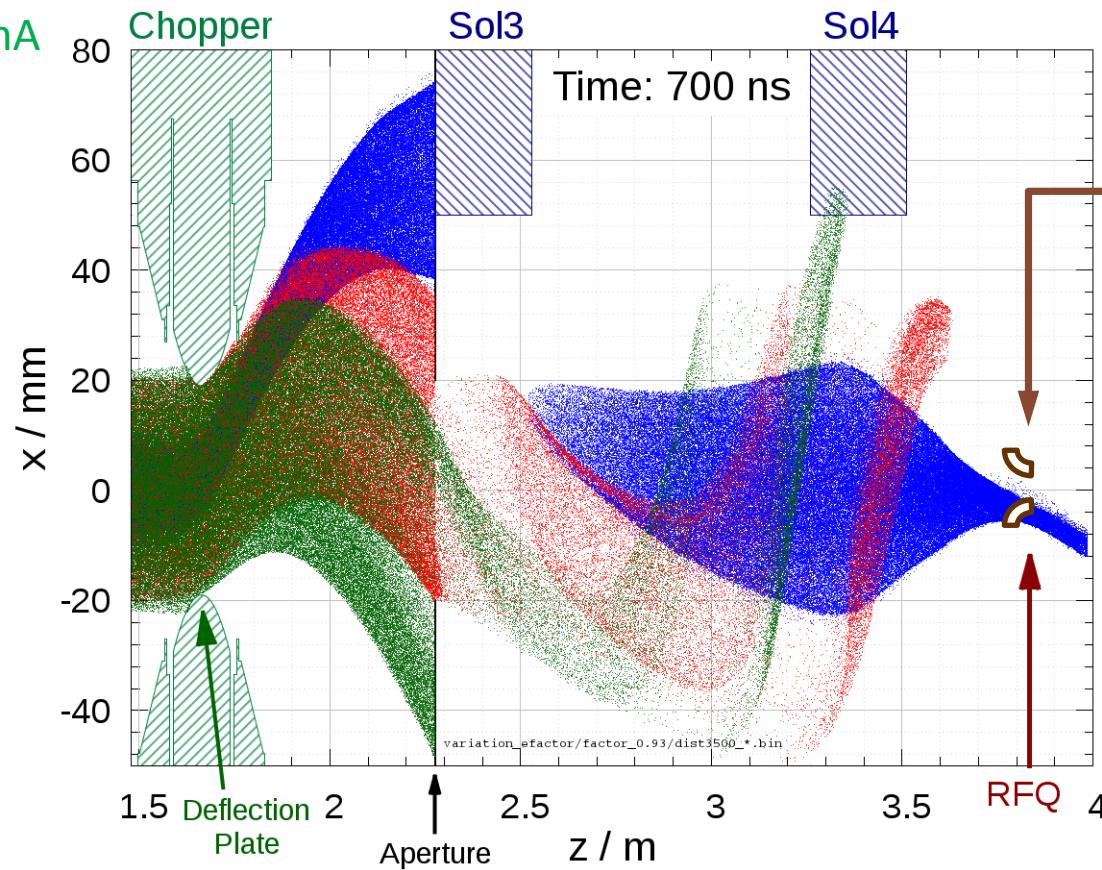


Beam Shaping Simulation

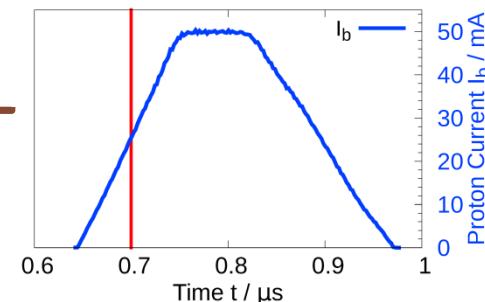
p , 50 mA

H_2^+ , 5 mA

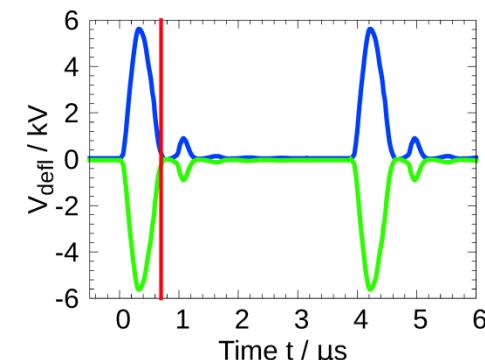
H_3^+ , 5 mA



Beam Pulse



Voltage Pulse



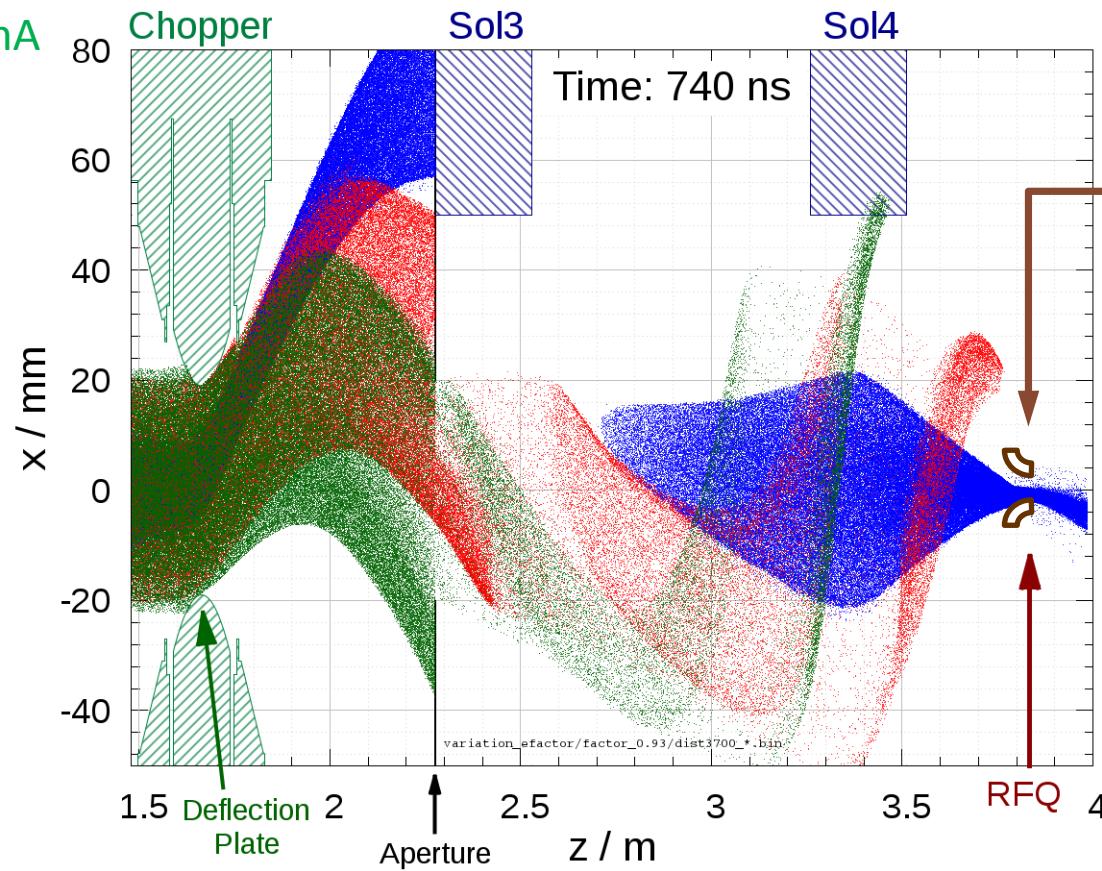


Beam Shaping Simulation

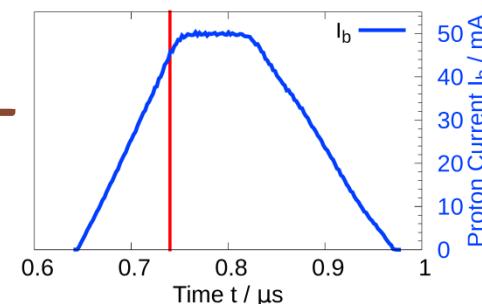
p , 50 mA

H_2^+ , 5 mA

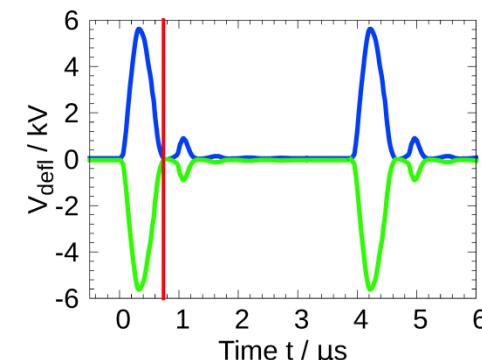
H_3^+ , 5 mA



Beam Pulse



Voltage Pulse



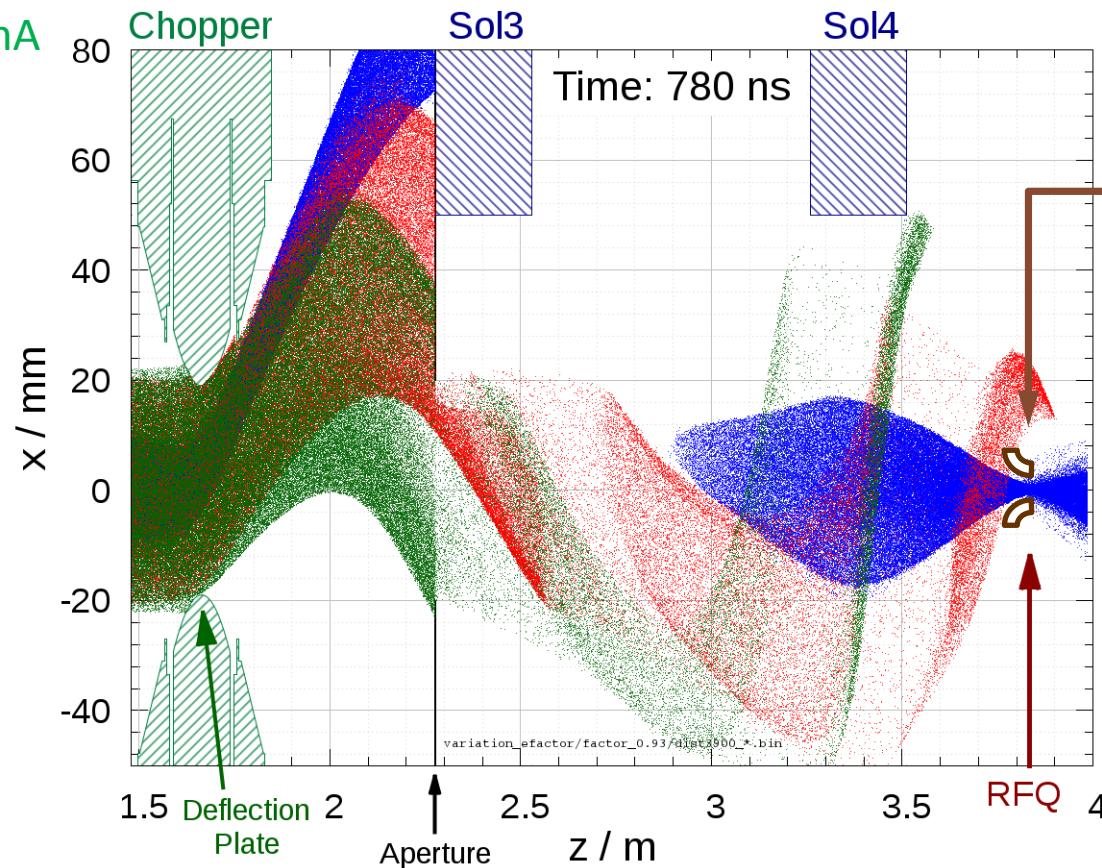


Beam Shaping Simulation

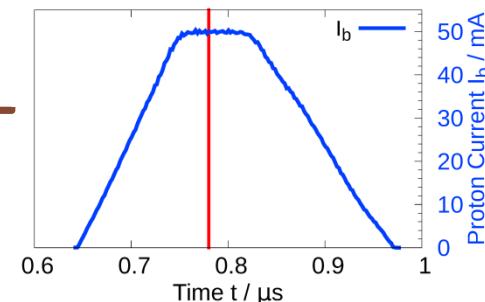
p, 50 mA

H₂⁺, 5 mA

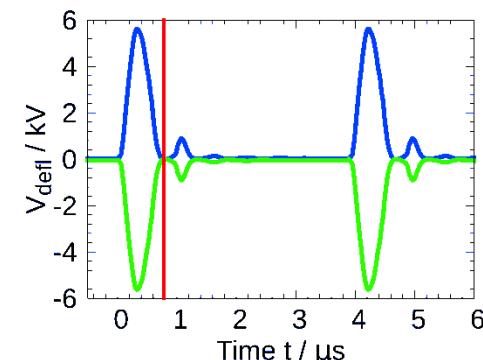
H₃⁺, 5 mA



Beam Pulse

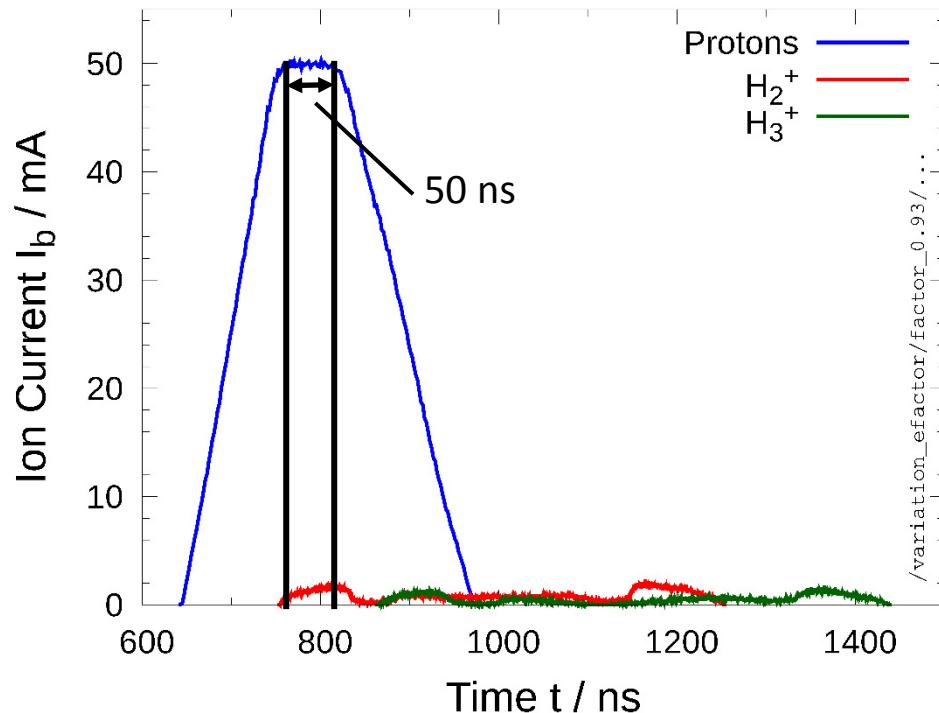


Voltage Pulse



Beam Shaping Simulation

Simulated Pulse Shape
at the RFQ Entrance



Results of Numerical Simulations:

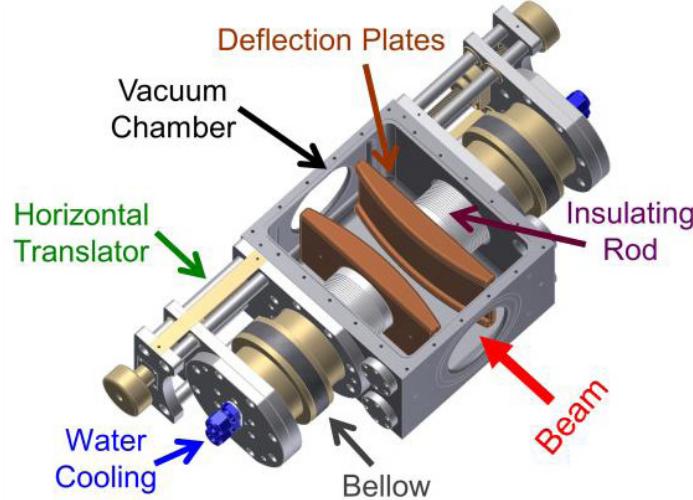
- Time requirements fulfilled.
- 50 ns flat top:
 - Position offset below ± 0.3 mm (necessary condition: *longitudinal* matching of deflection forces).
- Low emittance.
- Cylindrical symmetry preserved (necessary condition: *transverse* matching of deflection forces).
- Low transmission for H_2^+ and H_3^+ ions (pulsed velocity filter).

Simulated without collimator system in front of the RFQ.

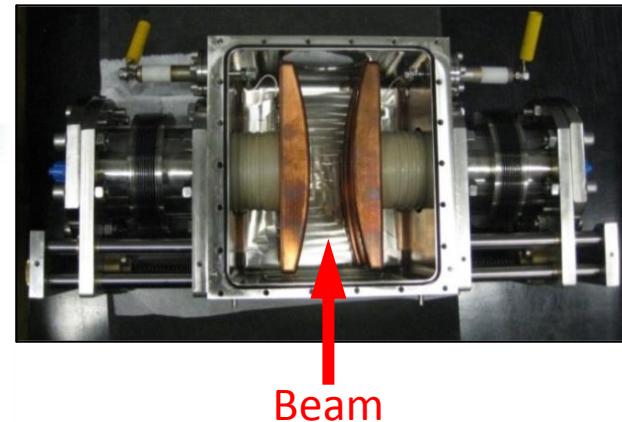
Chopper Hardware Design

Electric Deflector

$$\begin{aligned}V_0 &= \pm 6 \text{ kV} \\f_{\text{rep}} &= 257 \text{ kHz} \\l_{\text{plate}} &= 15 \text{ cm} \\h_{\text{plate}} &= 8 \text{ cm}\end{aligned}$$



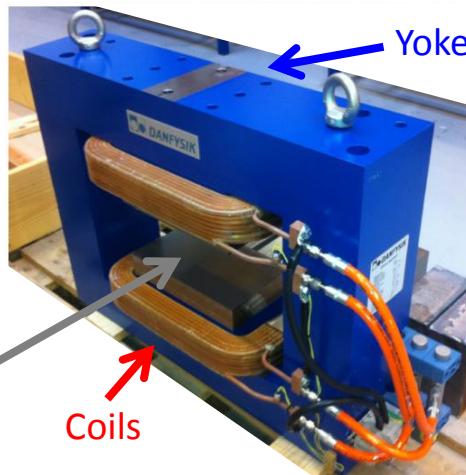
Deflection Chamber



Magnetic Dipole

$$\begin{aligned}B_0 &= 130 \text{ mT} \\I_{\text{coil}} &= 130 \text{ A} \\l_{\text{dipole}} &= 15 \text{ cm} \\h_{\text{gap}} &= 11 \text{ cm}\end{aligned}$$

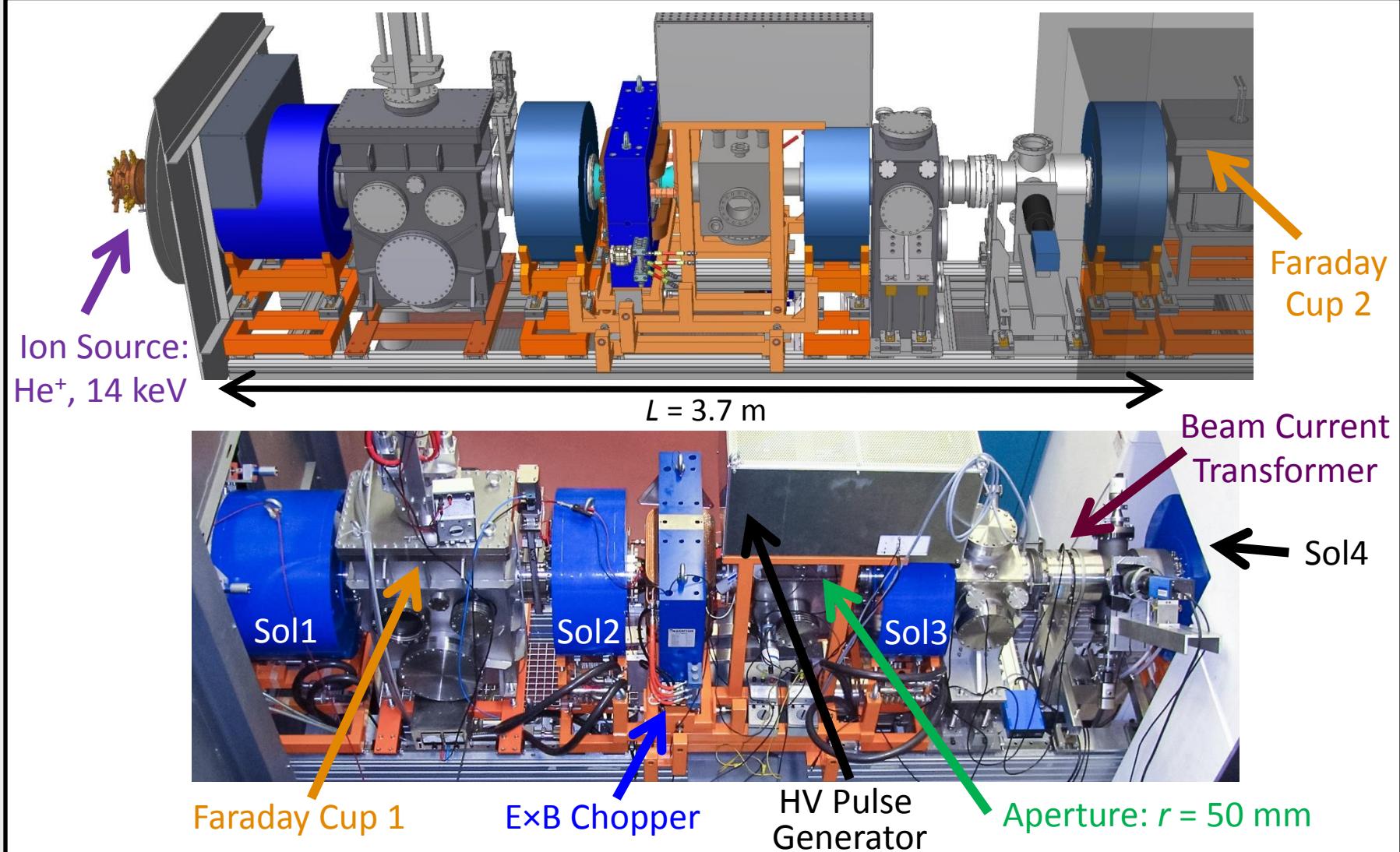
Exchangeable
Pole Plates



Deflection Chamber in Dipole



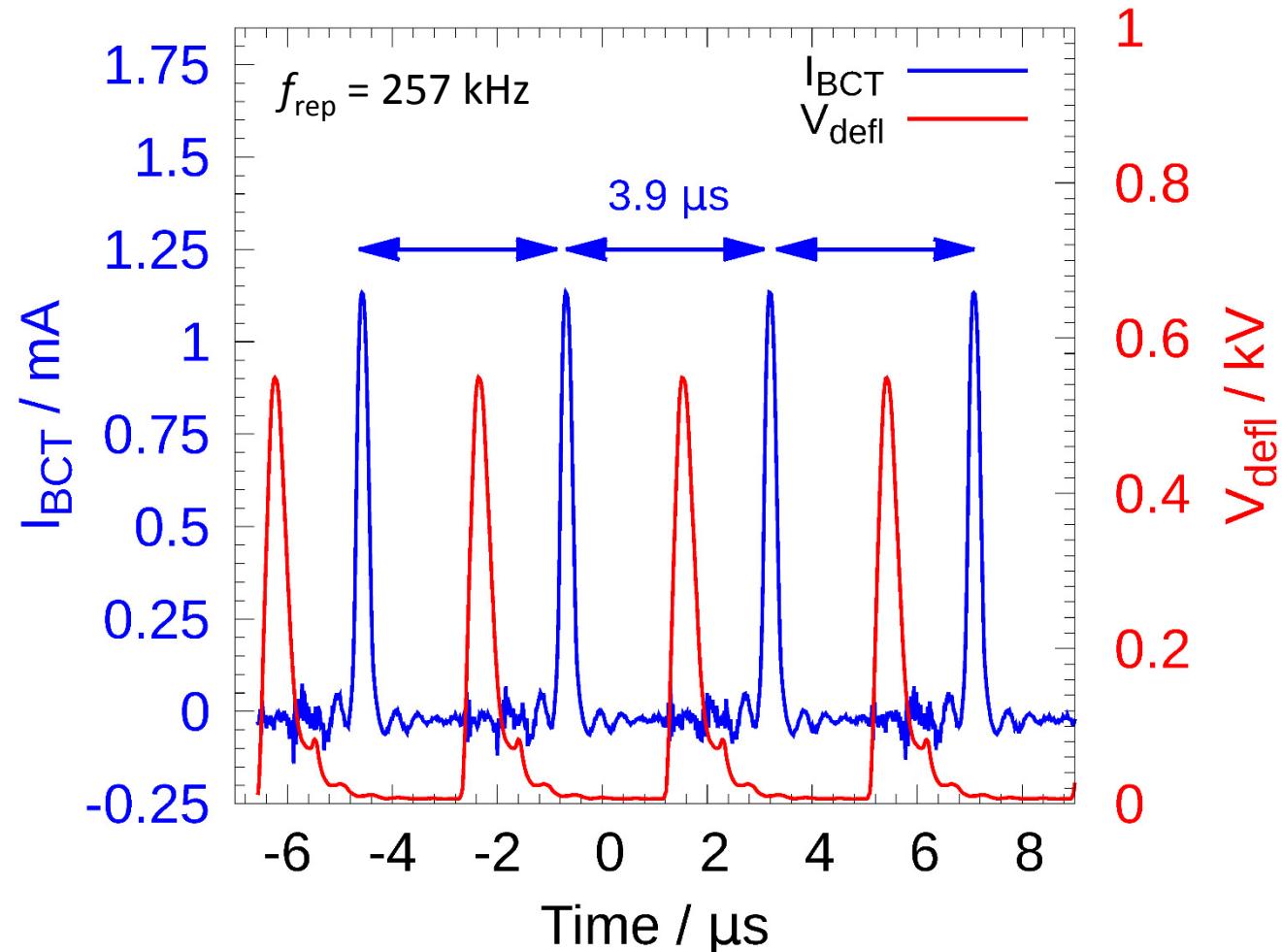
Experimental Setup: FRANZ LEBT



Measurements: Repetition Rate

- Beam chopping at 257 kHz experimentally achieved.
- Ratio of Pulsed to DC Beam Current of $95.2\% \pm 1.6\%$ achieved.

He^+ , 14 keV
 $r_{\text{aperture}} = 50 \text{ mm}$
 $I_{\text{dipole}} = 40.0 \text{ A}$



Measurements: Pulse Shape

- Reliable chopping and transport was achieved even for high-perveance beams.

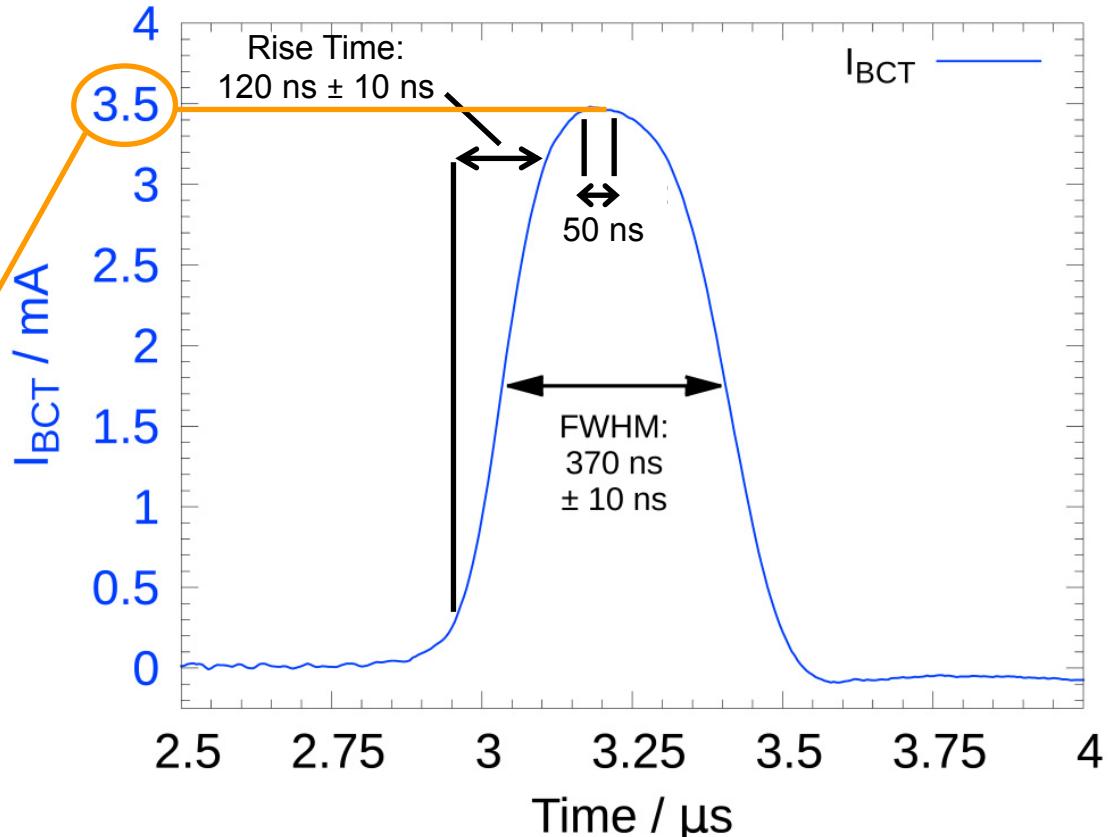
Gen. perveance K equivalent to 175 mA, p, 120 keV.

$$K = \frac{1}{4\pi\epsilon_0} \sqrt{\frac{m_p}{2q}} \frac{I_b}{V_{acc}^{3/2}}$$

He^+ , 14 keV

$r_{\text{aperture}} = 50 \text{ mm}$

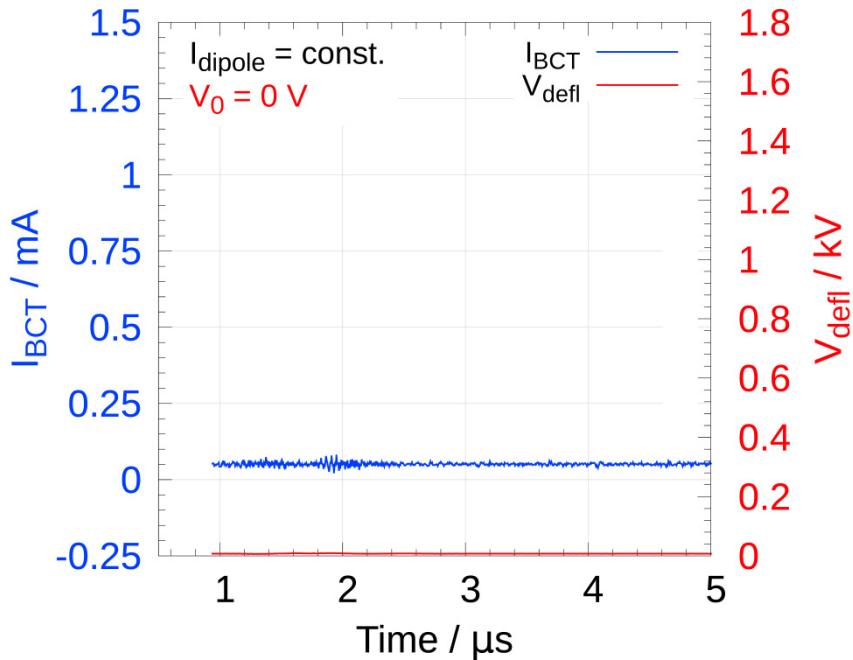
$I_{\text{dipole}} = 40.0 \text{ A}$





IAP

Measurements: Variation of Wien Ratio

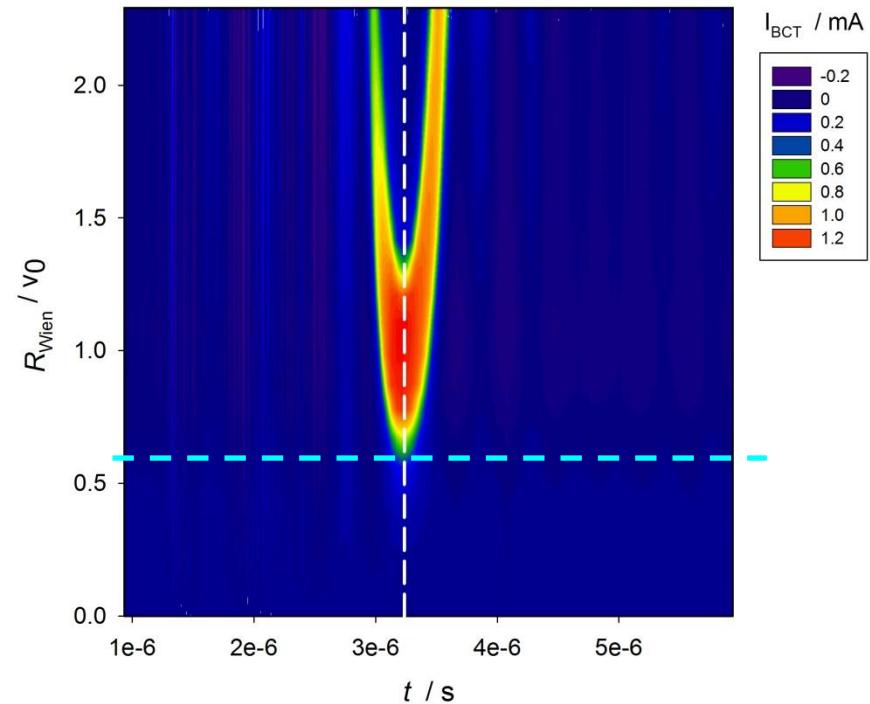
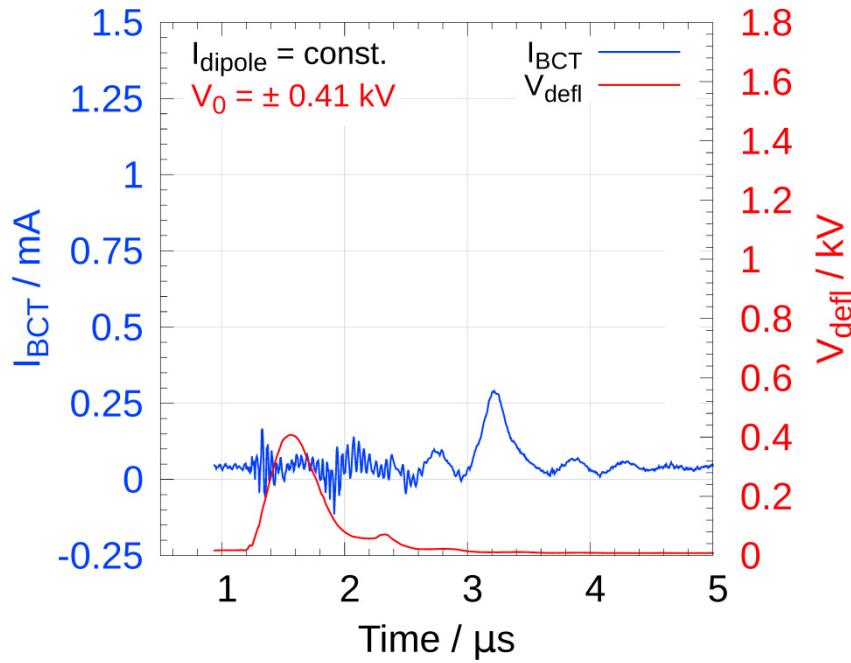


He^+ , 14 keV
 $r_{\text{aperture}} = 50 \text{ mm}$
 $I_{\text{dipole}} = 40.0 \text{ A}$

$$R_{\text{Wien}} = \frac{\int E_x dz \cdot f_{\text{tof}}}{\int B_y dz}$$

sweep → E_x
const. → B_y

Measurements: Variation of Wien Ratio

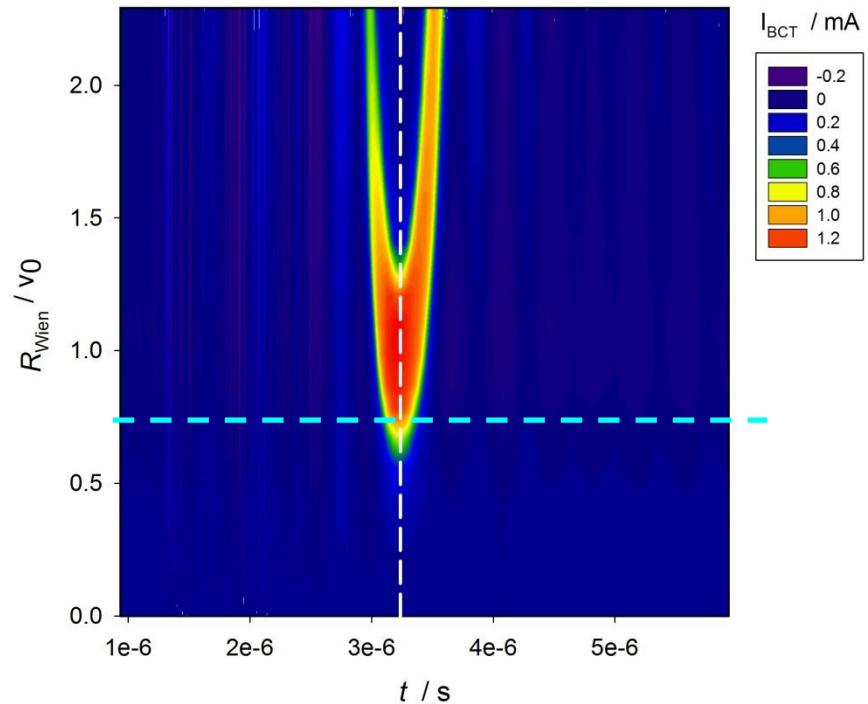
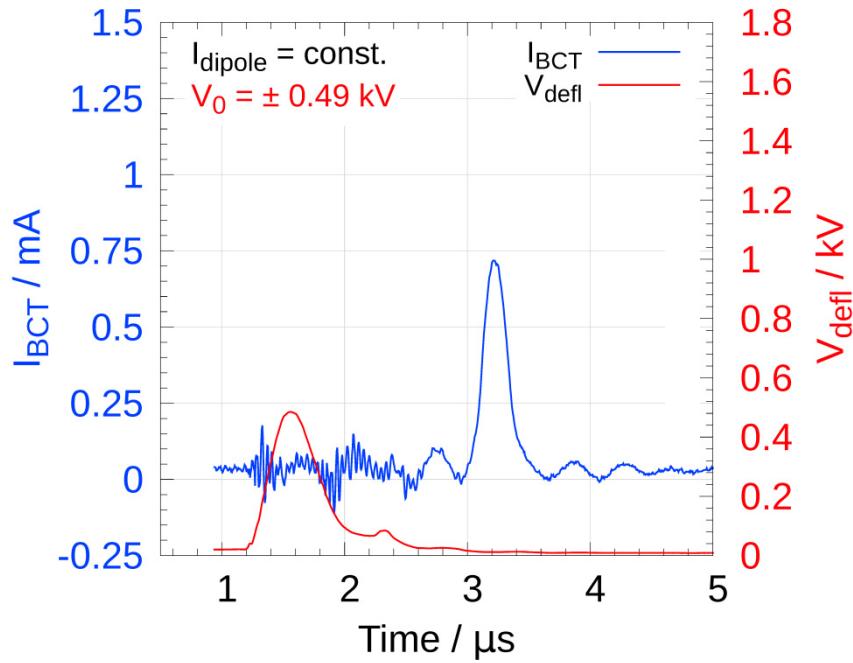


He^+ , 14 keV
 $r_{\text{aperture}} = 50 \text{ mm}$
 $I_{\text{dipole}} = 40.0 \text{ A}$

$$R_{\text{Wien}} = \frac{\int E_x dz \cdot f_{\text{tof}}}{\int B_y dz}$$

sweep → E_x
const. → B_y

Measurements: Variation of Wien Ratio

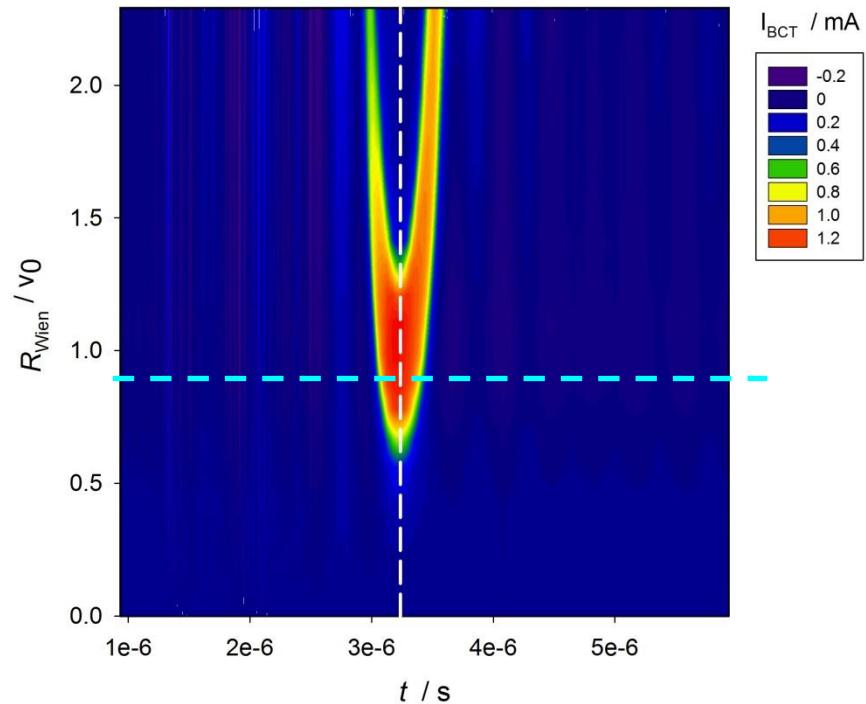
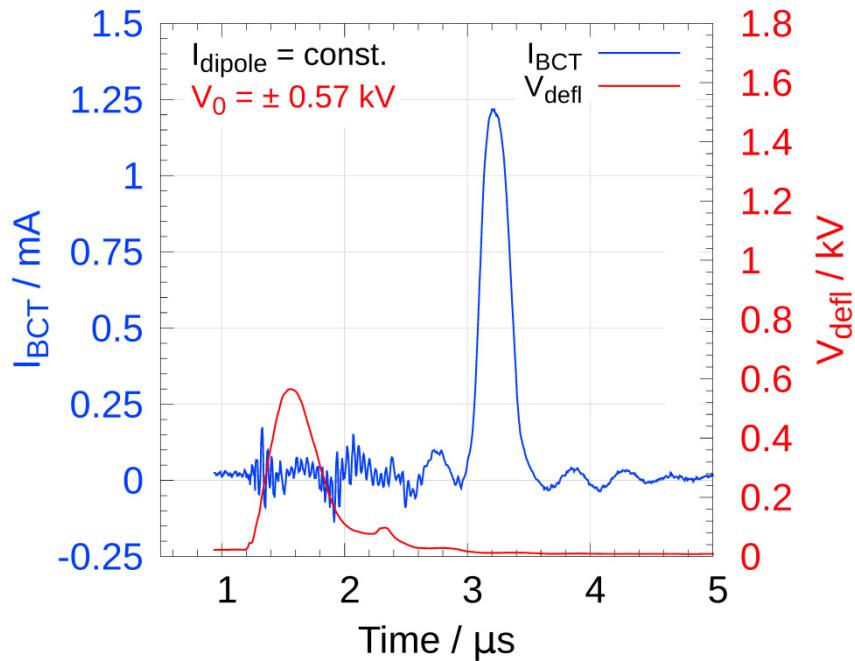


He^+ , 14 keV
 $r_{\text{aperture}} = 50 \text{ mm}$
 $I_{\text{dipole}} = 40.0 \text{ A}$

$$R_{\text{Wien}} = \frac{\int E_x dz \cdot f_{\text{tof}}}{\int B_y dz}$$

sweep
const.

Measurements: Variation of Wien Ratio



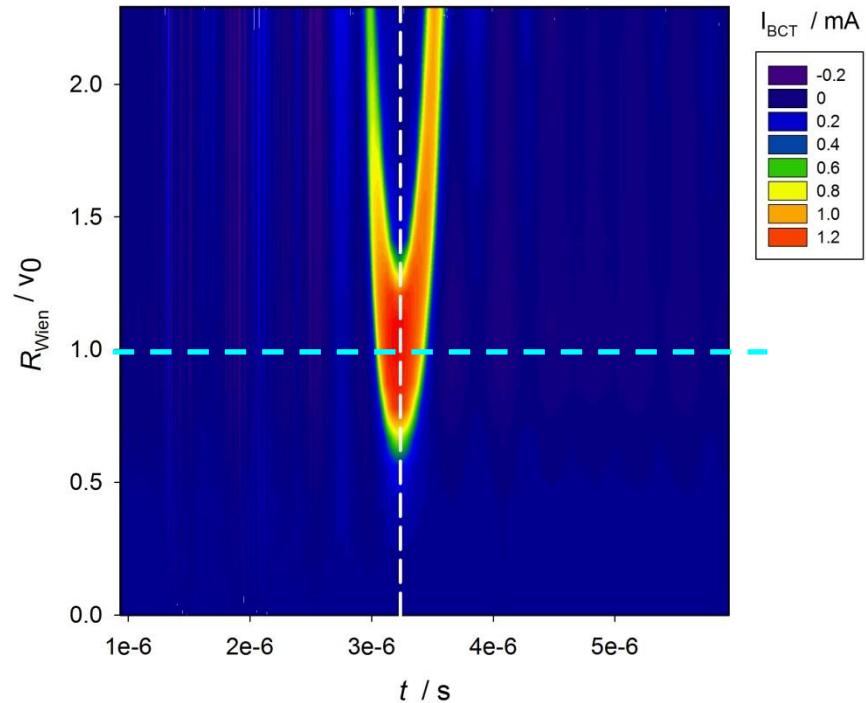
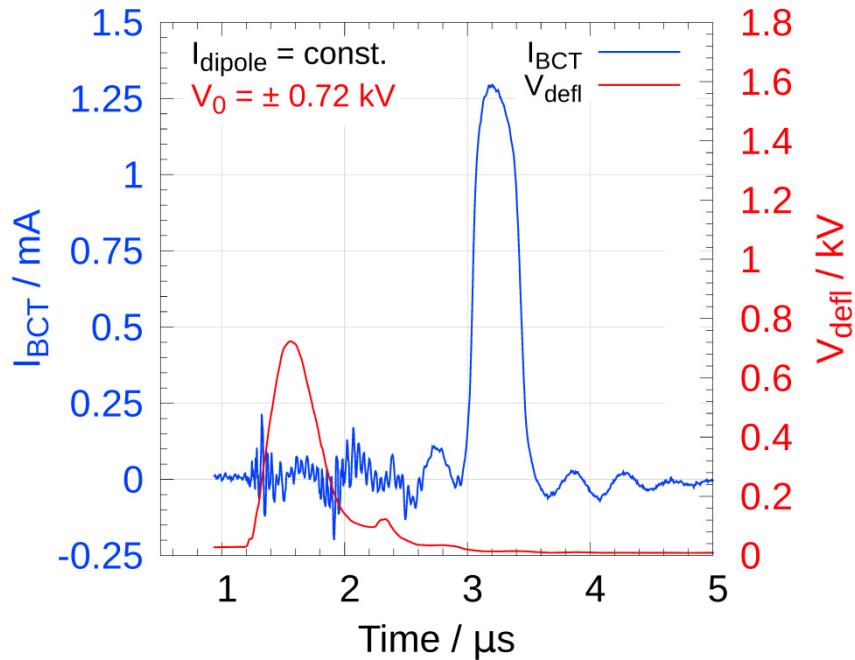
He^+ , 14 keV
 $r_{\text{aperture}} = 50 \text{ mm}$
 $I_{\text{dipole}} = 40.0 \text{ A}$

$$R_{Wien} = \frac{\int E_x dz \cdot f_{\text{tof}}}{\int B_y dz}$$

sweep → E_x

const. → B_y

Measurements: Variation of Wien Ratio

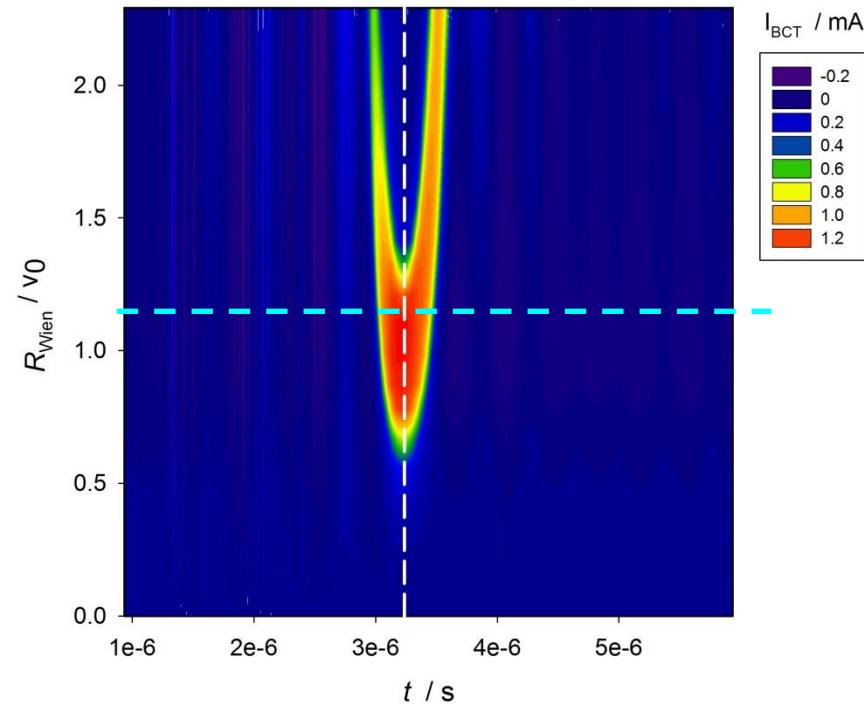
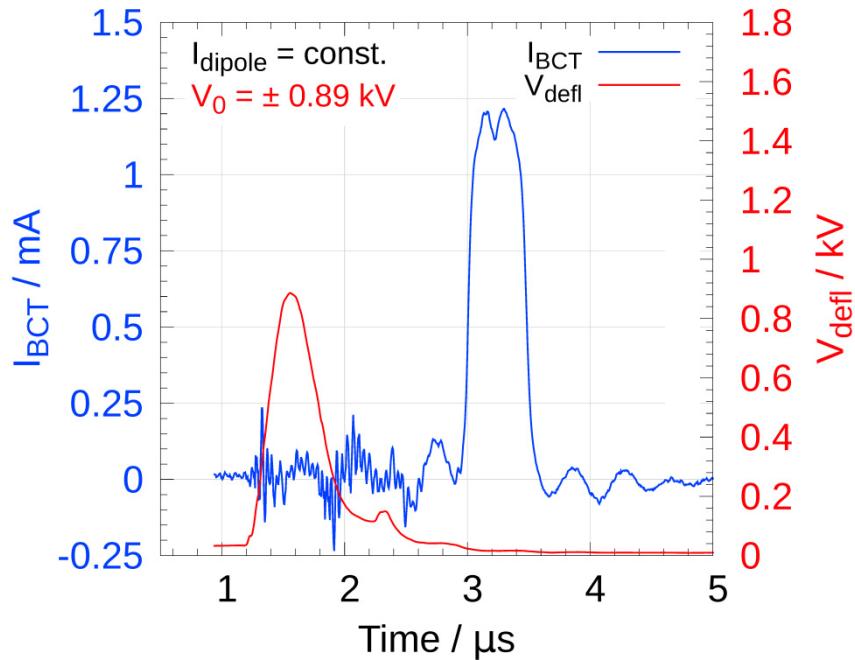


He^+ , 14 keV
 $r_{\text{aperture}} = 50 \text{ mm}$
 $I_{\text{dipole}} = 40.0 \text{ A}$

$$R_{\text{Wien}} = \frac{\int E_x dz \cdot f_{\text{tof}}}{\int B_y dz}$$

sweep → E_x
const. → B_y

Measurements: Variation of Wien Ratio

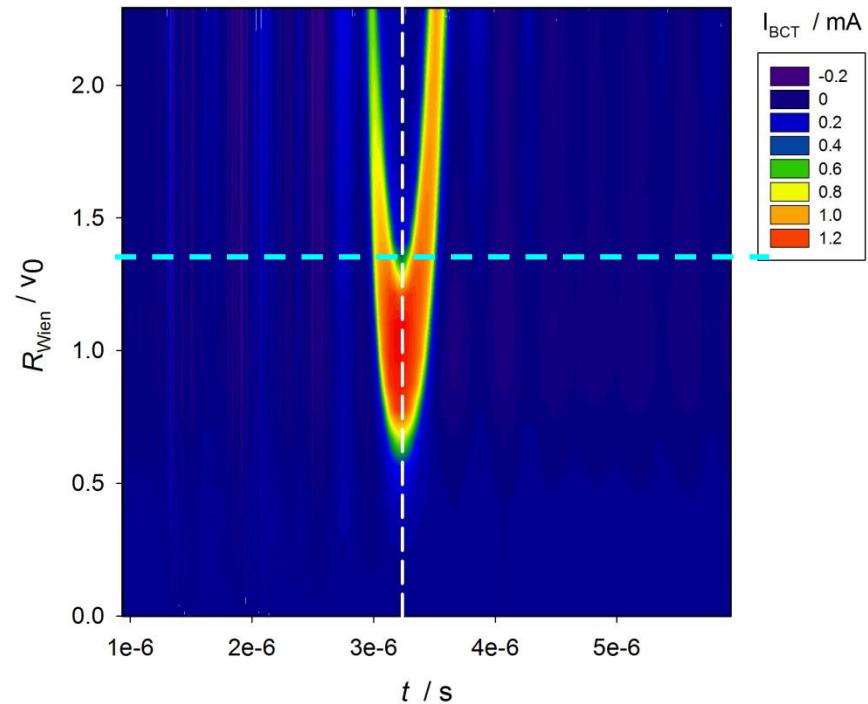
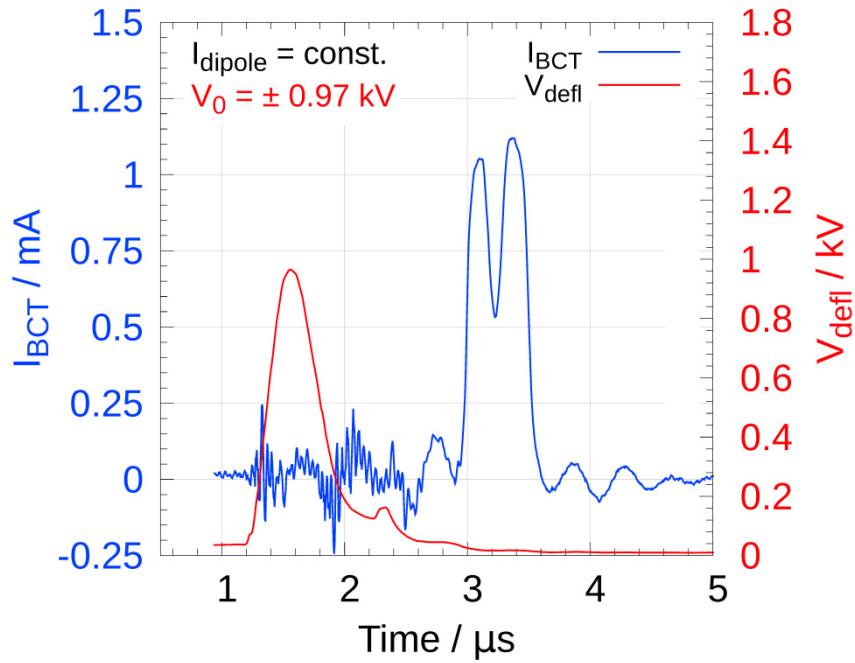


He^+ , 14 keV
 $r_{\text{aperture}} = 50 \text{ mm}$
 $I_{\text{dipole}} = 40.0 \text{ A}$

$$R_{\text{Wien}} = \frac{\int E_x dz \cdot f_{\text{tof}}}{\int B_y dz}$$

sweep → $E_x dz$
const. → $B_y dz$

Measurements: Variation of Wien Ratio

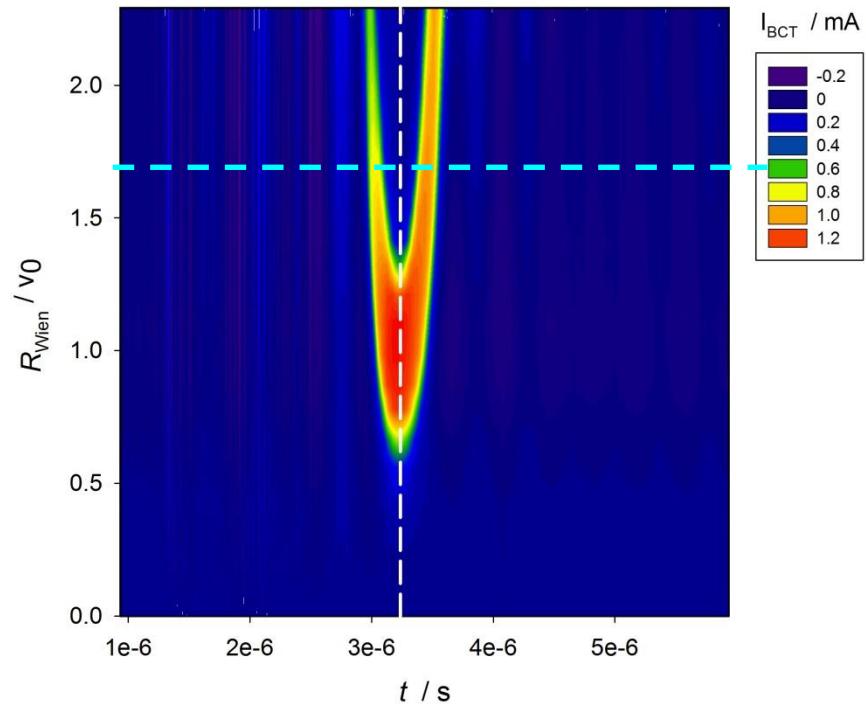
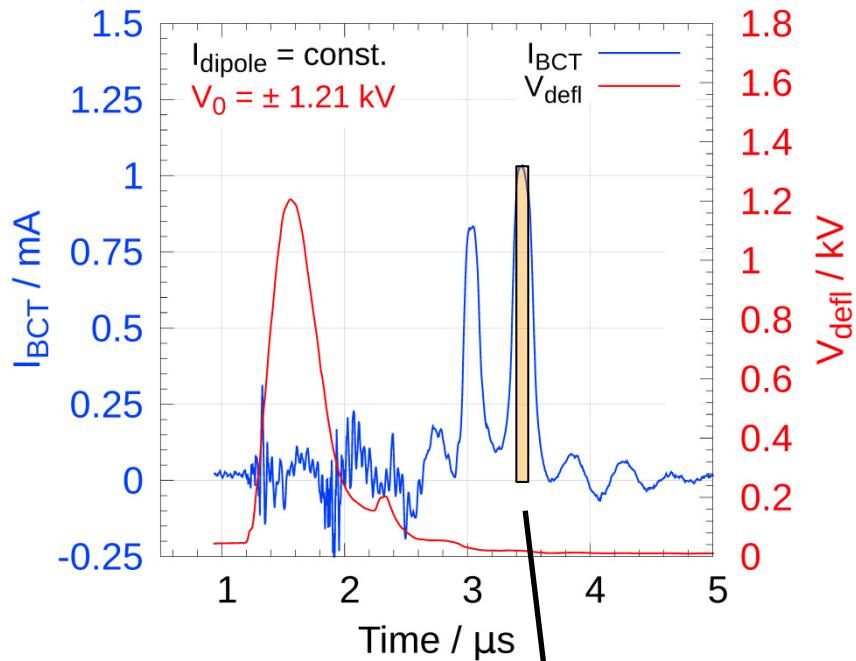


He^+ , 14 keV
 $r_{\text{aperture}} = 50 \text{ mm}$
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$$R_{\text{Wien}} = \frac{\int E_x dz \cdot f_{\text{tof}}}{\int B_y dz}$$

sweep → $E_x dz$
const. → $B_y dz$

Measurements: Variation of Wien Ratio



He^+ , 14 keV
 $r_{\text{aperture}} = 50 \text{ mm}$
 $I_{\text{dipole}} = 40.0 \text{ A}$

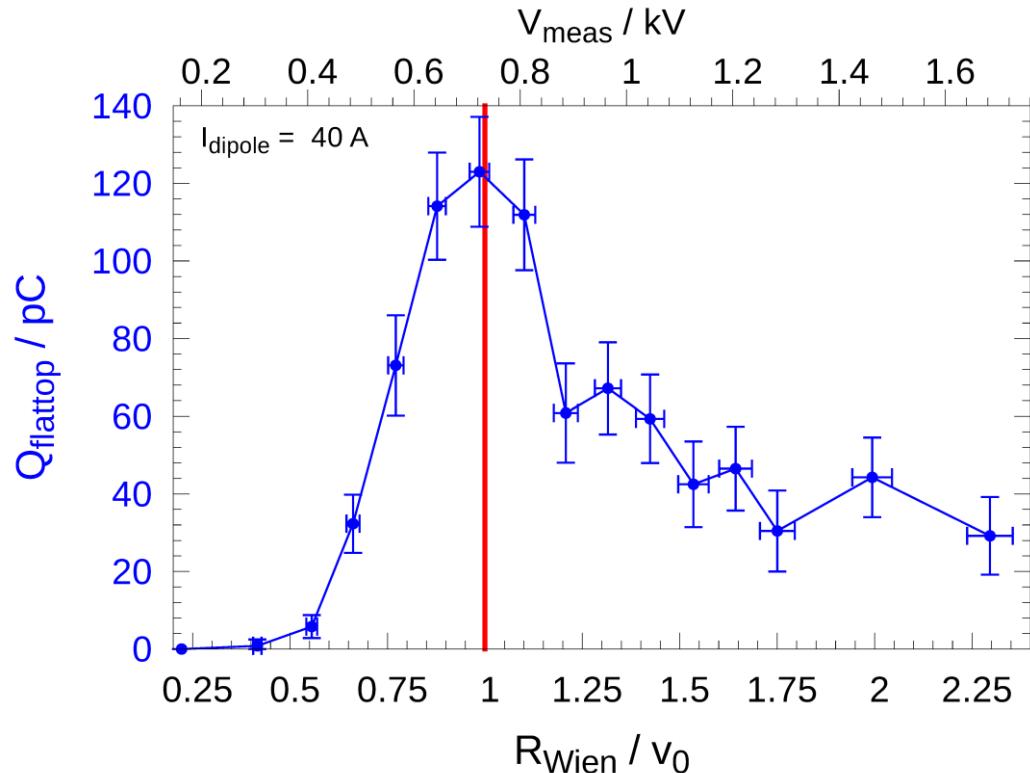
$$Q_{\text{flattop}} = I_{BCT}^{\max} \cdot t_{\text{flattop}}$$

$$R_{\text{Wien}} = \frac{\int E_x dz \cdot f_{\text{tof}}}{\int B_y dz}$$

sweep → $E_x dz$
const. → $B_y dz$

Measurements: Variation of Wien Ratio

- Highest flat-top charge achieved for the theoretically derived Wien condition.
- Adequate matching of electric and magnetic deflection forces.



He^+ , 14 keV
 $r_{\text{aperture}} = 50 \text{ mm}$
 $I_{\text{dipole}} = 40.0 \text{ A}$

$$Q_{\text{flattop}} = I_{\text{BCT}}^{\max} \cdot t_{\text{flattop}}$$

$$R_{\text{Wien}} = \frac{\int E_x dz \cdot f_{\text{tof}}}{\int B_y dz}$$

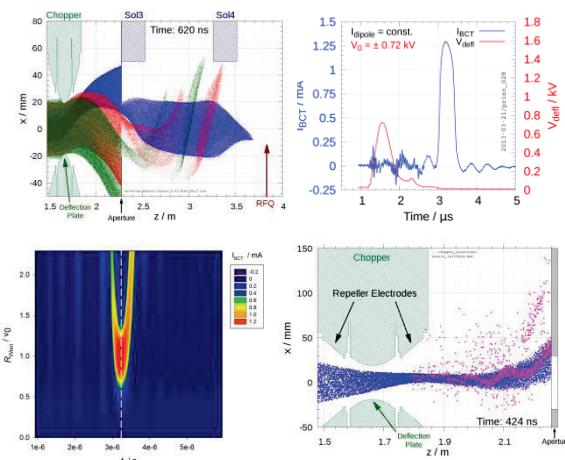
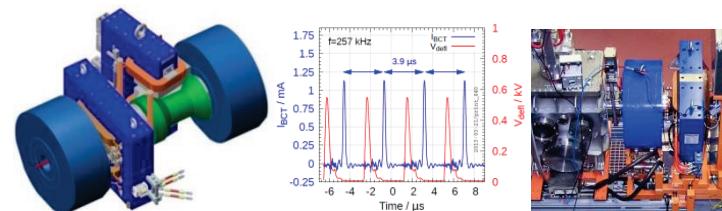
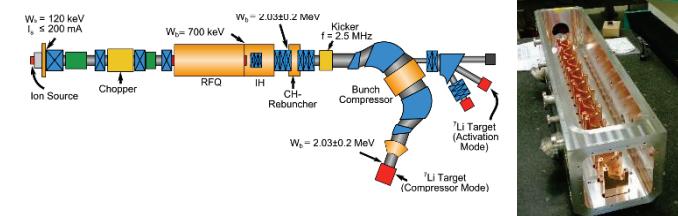
sweep → circled E_x

const. → circled B_y



Conclusion

- Accelerator-driven neutron source FRANZ currently under construction.
- ExB chopper and LEBT section have been commissioned with beam: ready for pulsed & dc operation.
- *ExB chopper + LEBT = low-energy test stand:*
 - Transport of high-perveance beams...
 - ...in dc or in pulsed mode...
 - ...using different beam fractions...
 - ...with or without space-charge compensation...
 - ...including electron-ion interaction.





IAP



Thank you for your attention!