

# FIVE CELL METHOD OF TUNING BIPERIODIC LINEAR STANDING WAVE $\pi/2$ ACCELERATING STRUCTURES\*

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## Abstract

The five parameter method of tuning of biperiodic  $\pi/2$  linear accelerating structure is presented. The method consists in analytical calculation of the five parameters determining the dispersion relation of such structure: two eigen frequencies  $f_a$  and  $f_c$  of accelerating and coupling cavities, the first coupling coefficient  $k_{ac}$  and two second coupling coefficients  $k_{aa}$  and  $k_{cc}$ , using five measured dispersion frequencies. Usually the process of tuning is based on sets of 3 cavities however, to include directly also the second coupling coefficients  $k_{aa}$  and  $k_{cc}$ , one should consider sets composed of five cells. Using the dispersion relation, a set of five equations for five unknowns is obtained. This set is solved by successive elimination of unknowns by expressing them in terms of  $F_a = f_a/f_{\pi/2}$ . For  $F_a$  one obtains biquadratic equation. Coefficients of this equation are expressed as functions of measured quantities: dispersion phases and frequencies. Knowing  $F_a$  all other parameters are easily calculated together with the Stop Band  $SB = |f_a - f_c|$ . In this way, on each step of building up the structure one can control precision of measurements and the Stop Band.

## INTRODUCTION

The well known advantages of standing wave biperiodic accelerating structure operating in the  $\pi/2$  mode are good stability and small sensitivity to mechanical, temperature and assembly imperfections. The structure consists of a chain of accelerating and coupling cavities, the latter being much shorter than the accelerating ones, serve only for coupling and in the  $\pi/2$  mode are not excited to the first order. The dispersion curve given by the relation (1) of such structure consists of two branches which for the well tuned structure should coincide at the shift angle  $\varphi = \pi/2$

$$k_{ac}^2 \cos^2 \varphi = \left(1 - \frac{\omega_a^2}{\omega^2} + k_{aa} \cos 2\varphi\right) \left(1 - \frac{\omega_c^2}{\omega^2} + k_{cc} \cos 2\varphi\right) \quad (1)$$

Using this dispersion relation (1) we will solve the following problem: given five measured dispersion frequencies, find five parameters  $\omega_a$ ,  $\omega_c$ ,  $k_{ac}$ ,  $k_{aa}$  and  $k_{cc}$  defining the acceleration structure and realizing acceptable, sufficiently small, stop band  $SB = |f_a - f_c|$ .

## SYSTEM OF EQUATIONS FOR FIVE ELEMENTS METHOD OF TUNING BIPERIODIC ACCELERATING STRUCTURE

To formulate the equations for five elements method it will be useful to introduce some conventions and notations.

We will assume that for phases  $\varphi$  between 0,  $\pi$  the dispersion curve  $f(\varphi)$  is monotonically increasing, and has the shape presented in Fig. 1.

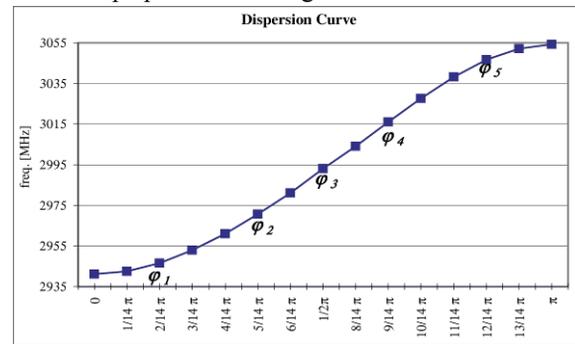


Figure 1: Arbitrary dispersion curve.

Each point  $P_i(\varphi_i, f_i)$  of the dispersion curve is defined by two parameters  $(\varphi_i, f_i)$ , with  $i = 1 \dots 5$ , which we assume to be given by measurements. Taking into account the symmetry of the dispersion curve in respect to central phase  $\varphi_3 = \pi/2$ , in each set of five points taken into consideration, except central phase  $\pi/2$ , following two pairs of correlated phases will be chosen:

$$(\varphi_1, \varphi_5), \text{ where } \varphi_5 = \pi - \varphi_1 \quad (2)$$

$$(\varphi_2, \varphi_4), \text{ where } \varphi_4 = \pi - \varphi_2 \quad (3)$$

According to this choice we will have

$$\cos \varphi_5 = -\cos \varphi_1, \cos^2 \varphi_5 = \cos^2 \varphi_1 = 1/c_1 \quad (4.1)$$

$$\cos \varphi_4 = -\cos \varphi_2, \cos^2 \varphi_4 = \cos^2 \varphi_2 = 1/c_2 \quad (4.2)$$

$$\cos 2\varphi_5 = \cos 2\varphi_1 = b_1 \quad (4.3)$$

$$\cos 2\varphi_4 = \cos 2\varphi_2 = b_2 \quad (4.4)$$

For any set of five points  $P_i$  lying on the dispersion curve chosen according to the above procedure using expressions (2) to (4.4), together with corresponding frequencies and dispersion relation (1), one obtains following set of five equations:

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$$k_{ac}^2 = c_2(1 - a_2 F_a^2 + b_2 k_{aa})(1 - a_2 F_c^2 + b_2 k_{cc}) \quad (5.1)$$

$$k_{ac}^2 = c_2(1 - a_2 F_a^2 + b_2 k_{aa})(1 - a_2 F_c^2 + b_2 k_{cc}) \quad (5.2)$$

$$0 = (1 - F_a^2 - k_{aa})(1 - F_c^2 - k_{cc}) \quad (5.3)$$

$$k_{ac}^2 = c_2(1 - a_4 F_a^2 + b_2 k_{aa})(1 - a_4 F_c^2 + b_2 k_{cc}) \quad (5.4)$$

$$k_{ac}^2 = c_1(1 - a_5 F_a^2 + b_1 k_{aa})(1 - a_5 F_c^2 + b_1 k_{cc}) \quad (5.5)$$

where:

$$F_a = \frac{f_a}{f_3}, F_c = \frac{f_c}{f_3}, a_i = F_i^{-2}, i = 1, 2, \dots, 5 \quad (6)$$

We will solve the system of equations (5.1) to (5.5) by successive elimination of unknowns by expressing them in terms of unknown  $F_a$ . As a result we obtain biquadratic equation (7) for  $F_a^2$ .

$$PF_a^4 - QF_a^4 + R = 0 \quad (7)$$

Where

$$P = c_1(a_1 + b_1)(a_5 + b_1) - c_2(a_2 + b_2)(a_4 + b_2) \quad (8)$$

$$Q = c_1(1 + b_1)(a_1 + a_5 + 2b_1) - c_2(1 + b_2)(a_2 + a_4 + 2b_2) \quad (9)$$

$$R = c_1(1 + b_1)^2 - c_2(1 + b_2)^2 \quad (10)$$

Using definitions of  $b_k$  and  $c_k$ , ( $k=1,2$ ), given by expressions (4.1) to (4.4) one finds

$$c_k(1 + b_k) = 2$$

$$c_1(1 + b_1)^2 - c_2(1 + b_2)^2 = 2(b_1 - b_2)$$

Taking above into account one obtains

$$R = 2(b_1 - b_2) \quad (11)$$

$$Q = 2[(a_1 + a_5) - (a_2 + a_4) + R] \quad (12)$$

Solution to the equation (7) is

$$F_{a_i}^2 = \frac{Q \pm \sqrt{\Delta}}{2P} \quad (13)$$

where the discriminant  $\Delta$  is equal to

$$\Delta = Q^2 - 4PR \quad (14)$$

Knowing  $F_a^2$  the remaining unknowns  $k_{aa}$ ,  $k_{cc}$ ,  $F_c^2$  and  $k_{ac}$  can be calculated). In this way all parameters defining

the dispersion relation of the  $\pi/2$  biperiodic accelerating structure and the stop band  $SB = f_a - f_c$  are found.

Usually calculated parameters can be different for different five element sets of dispersion frequencies, although, they should define the same structure. This effect is due to the errors in dispersion frequencies measurements and these errors influence also the calculated parameters of dispersion relation. Since results of measurements are random, one can assume, that errors distribution is normal and the most probable values of calculated parameters will be an arithmetic mean of all individual results. For structure composed of  $N$  ( $N$  is odd) cells, the number  $N_s$  of different combinations of sets composed of five cells, chosen according to the prescription given by equations (2) and (3) will be

$$N_s = (N-1)(N-3)/8$$

The knowledge of the calculated most probable values of the biperiodic accelerating structure parameters will be very useful in the process of tuning the structure.

## THE TUNING

Principally process of tuning in the five cells method is similar to that of three cells method. Tuning starts with 3 elements sets:  $\frac{1}{2}$  accelerating + coupling +  $\frac{1}{2}$  accelerating cavities. The aim of tuning is to obtain minimum field level in the coupling cavities. Joining successively the three elements pretuned sets one obtains sets composed of 5, 7...  $2N+1$  cavities. Beginning from the set of 5 cavities, according to the above described method, one can calculate, all five parameters defining the successively growing up accelerating structure. On each step of building up the structure different checks and corrections are available.

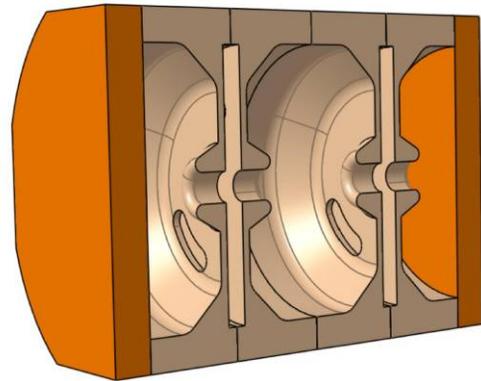


Figure 2: RF quintuplet.

The first check depends on the sign of the discriminant  $\Delta$  (14) of eq.(7). If  $\Delta < 0$ , then the frequencies  $f_a$ ,  $f_c$  and  $f_{\pi/2}$  are complex and there is attenuation in time of the electromagnetic wave propagating in the structure.

Analysing the dependence of the quantities  $P$ ,  $Q$ ,  $R$  and  $\Delta$  on the parameters  $a_k(f_k)$  one can find, which measured frequencies  $f_k$  of the dispersion curve belonging to the considered five elements set, should be changed. Similar situation can happen with the sign of the square of coupling coefficient  $k_{ac}$ . If  $k_{ac}^2 < 0$  for some set of frequencies  $f_k$ , then the analysis of the expressions for  $k_{ac}^2$  (eq. (5.1) or (5.2)) will give indications in which direction one should go with changes of  $f_k$  to obtain  $k_{ac}^2 > 0$ .

However, the most important corrections are possible due to the knowledge of average calculated values of dispersion curve parameters. Since these values are the most probable parameters defining dispersion relation of the measured structure, we can solve the following problem: given the parameters  $f_a$ ,  $f_c$ ,  $k_{ac}$ ,  $k_{aa}$ ,  $k_{cc}$  of the dispersion curve, find dispersion frequencies  $f_i(\varphi_i)$  of the structure.

A simple program TUNING was written to solve the equation (7). As the input data for the program only the measured dispersion curve of the tuned structure is needed.

Below an example of tuning of a short accelerating structure is given. The first dispersion curve presents measured data without corrections, and the second presents data after tuning.

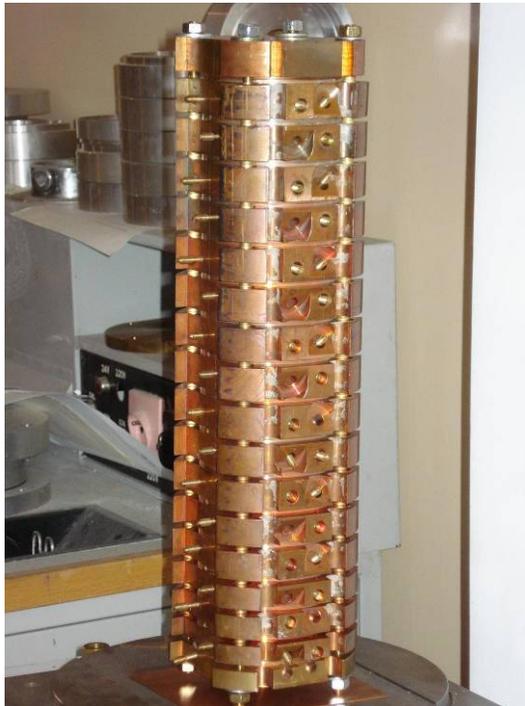


Figure 3: Biperiodic 3GHz accelerating stack.

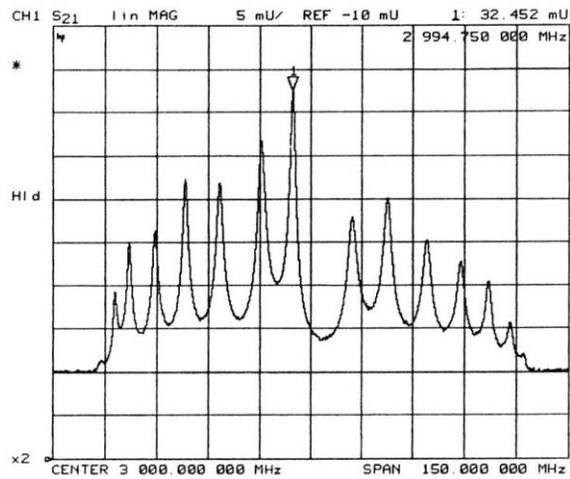


Figure 4: Frequency spectrum during tuning (8 cell stack).

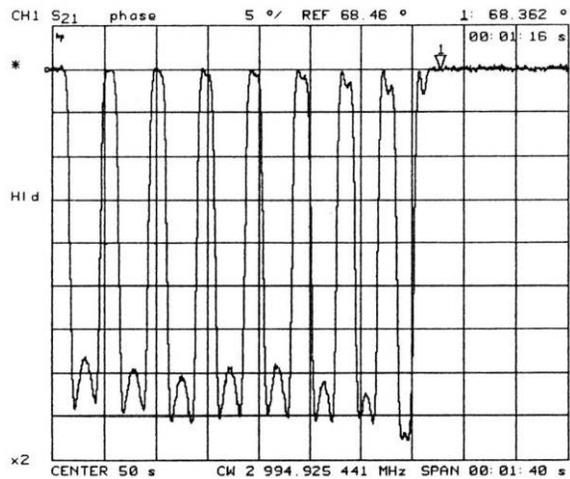


Figure 5: Accelerating field distribution in 8 cell stack.

**REFERENCES:**

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