

# ANALYTICAL SOLUTIONS IN THE TWO-CAVITY COUPLING PROBLEM

M.I.Ayzatsky, National Science Center, Kharkov Institute of Physics&Technology(KIPT),

310108, Kharkov, Ukraine.

## 1 INTRODUCTION

In the papers [1-3], we derived precise equations, describing the rf-coupling of two cavities through a centerhole of arbitrary dimensions. On the base of these equations we numerically calculated the relationship of coupling coefficients versus different parameters (frequency, hole radius, etc.). This paper presents analytical solutions of these equations for various limited cases. In particular, it is explicitly shown that in the case of small holes  $a \rightarrow 0$  the formulated equations agree with those derived in the papers [4-6] on the base of quasi-static approach. Besides, expressions are derived for coupling coefficients which are valid up to the second order in the relation of the hole dimension ( $a$ ) with the free-space wavelength ( $\lambda$ ). For derivation of these expressions we have used the method of solving of an infinite set of linear algebraic equations, based on its transformation into dual integral equations.

## 2 PROBLEM DEFINITION. ORIGINAL EQUATIONS

Let us consider the coupling of two cavities through a circular hole with the radius  $a$  in a separating wall that has the thickness  $t$ . For simplicity's sake, we will consider the case of two identical cavities, with  $b$  -being the cavity radii and  $d$  - their length. In the papers [1-3] it was demonstrated that if the field is expanded with the short-circuit resonant cavity modes and  $E_{010}$ -modes are selected as fundamental, the precise set of equations will consist of two equations for the amplitudes of  $E_{010}$  - modes, where coupling coefficients are defined by the way of solution of an infinite set of linear algebraic equations. Let us generalize the case considered in [1-3], choosing as fundamental  $E_{0pq}$ -modes of closed cavities ( $q$  is the number of field variations across the radius,  $p$  is the number of field variations along the longitudinal coordinates). Using the method, similar to the one in [1-3], one can show that the set of equations, describing the system under consideration, has the form:

$$\begin{aligned} \varepsilon_p Z_{q,p} a_{q,p}^{(1)} = \\ = -\omega_{q,0}^2 \frac{4}{3\pi J_1^2(\lambda_q)} \frac{a^3}{b^2 d} \left[ a_{q,p}^{(1)} \Lambda_1 - (-1)^p a_{q,p}^{(2)} \Lambda_2 \right] \end{aligned} \quad (1)$$

where

$$Z_{q,p} = \omega_{q,p}^2 - \omega^2, \quad \omega_{q,p}^2 = c^2 \left[ \lambda_q^2 / b^2 + (p\pi / d)^2 \right],$$

$$\varepsilon_p = \begin{cases} 2, & p = 0 \\ 1, & p \neq 0, \end{cases} \quad p = 0, 1, \dots, \infty, \quad J_0(\lambda_s) = 0, \quad s = 1, 2, \dots, \infty,$$

$a_{q,p}^{(i)}$  is the amplitude of  $E_{0qp}$ -mode in the  $i$ -th cavity ( $i=1,2$ ). The normalized coupling coefficients  $\Lambda_i$  are determined by the expression:

$$\Lambda_i = \Lambda_i(\omega) = J_0^2(\theta_q) \sum_{s=1}^{\infty} w_s^{(i)} / (\lambda_s^2 - \theta_q^2), \quad (2)$$

where  $w_s^{(i)}$  are the solution of the following set of linear equations:

$$\begin{aligned} w_m^{(2)} + \sum_s G_{m,s} \left( w_s^{(2)} f_m^{(1)} + w_s^{(1)} f_m^{(2)} \right) = \\ = 3\pi f_m^{(1)} / (\lambda_m^2 - \Omega_*^2) \end{aligned} \quad (3)$$

$$f_m^{(j)} = \frac{\mu_m}{\sinh(\mu_m)} \begin{cases} \cosh(q_m) - \cosh(q_m t / l), & j = 1 \\ \cosh(2q_m t / l), & j = 2, \end{cases}$$

$$q_m = \mu_m l / a, \quad l = 2d + t, \quad \mu_m = \sqrt{\lambda_m^2 - \Omega^2}, \quad \Omega = \omega a / c,$$

$$\Omega_*^2 = \Omega^2 - (\pi a p / d)^2,$$

$$\begin{aligned} G_{m,s} = B_{m,s} - \frac{1}{2\mu_m} \delta_{m,s} \coth\left(\frac{d}{a} \mu_m\right) + \\ + \frac{2\pi a^2 \theta_q^3 J_0^2(\theta_q)}{d b \varepsilon_p \chi_q (\lambda_m^2 - \theta_q^2) (\lambda_s^2 - \theta_q^2) \left\{ \mu_m^2 + (\pi a p / d)^2 \right\}}, \end{aligned}$$

$$B_{m,s} = \pi \frac{a}{b} \sum_{l=1}^{\infty} \frac{\theta_l^2 J_0^2(\theta_l) R_l}{\chi_l (\lambda_m^2 - \theta_l^2) (\lambda_s^2 - \theta_l^2)},$$

$$\theta_l = \lambda_l a / b, \quad \chi_l = \pi \lambda_l J_1^2(\lambda_l) / 2, \quad \nu_l = \sqrt{\theta_l^2 - \Omega^2},$$

$$R_l = \begin{cases} \theta_q \coth(\nu_q d / a) / \nu_q - \\ - 2a \theta_q / \left\{ \varepsilon_p d \left( \nu_q^2 + (\pi a p / d)^2 \right) \right\}, & l = q, \\ \theta_l \coth(\nu_l d / a) / \nu_l, & l \neq q. \end{cases}$$

The coefficients  $w_s^{(i)}$  have a simple physical sense. Really, it is easy to show that the tangential electric field component in the left cross-section of the coupling hole  $E_r^{(-)}(r)$  has the form:

$$E_r^{(-)}(r) = E_{\text{ind}}^{(1)} - E_{\text{ind}}^{(2)} = \tilde{E}_{0,q,p}^{(1)} Q^{(1)}(r) - \tilde{E}_{0,q,p}^{(2)} Q^{(2)}(r), \quad (4)$$

where  $Q^{(i)}(r) = \frac{1}{3\pi_s} \sum_s \frac{J_1(\lambda_s r / a)}{J_1(\lambda_s)} w_s^{(i)}$ ,  $\tilde{E}_{0,q,p}^{(i)}$  is the value

of the longitudinal (perpendicular to the hole) electric

field of  $(0, q, p)$ -mode in the first cavity on the left coupling hole cross-section at  $r = a$ , while  $\tilde{E}_{0,q,p}^{(2)}$  is the same value for the right-hand cavity on the right coupling hole cross-section at the same radius. From the expression (4) it follows that the tangential electric field component on the left coupling hole cross-section<sup>1</sup> is equal to the difference of two induced fields, each of which is proportional to the perpendicular electric field components of  $E_{0,q,p}$ -modes, taken to be fundamental.

There, the coefficients  $w_s^{(i)}$  are the ones of expansion of the appropriate functions with the complete set of functions  $\{J_1(\lambda_s r/a)\}$ . Thus, the two-cavity coupling problem, rigorously formulated on the base of the electric field expansion with the short-circuit resonant cavity mode, is reduced to the induced field definition on the right and left cylindrical hole cross-section..

### 3 INFINITELY THIN WALL CASE

An important role in the problem of cavity coupling plays the case of infinitely thin wall, dividing the cavities ( $t = 0$ ). In this case, from Eqs.(3) it follows that  $w_m^{(1)} = w_m^{(2)} = w_m$ . In this case the set of equations for  $w_m$  will take on the form<sup>2</sup>:

$$\sum_{s=1}^{\infty} w_s B_{m,s} = 3\pi / \left\{ 2(\lambda_m^2 - \Omega_s^2) \right\}. \quad (5)$$

For the case  $t = 0$   $\Lambda_1 = \Lambda_1 = \Lambda$ , where

$$\Lambda = J_0^2(\theta_q) \sum_s w_s / (\lambda_s^2 - \theta_q^2). \quad (6)$$

#### 3.1 Small coupling hole case ( $a \rightarrow 0$ )

If in Eqs.(5,6) the hole radius tends to zero<sup>3</sup>, then Eq.(5) will become:

$$\sum_{s=1}^{\infty} w_s \int_0^{\infty} d\theta \frac{\theta^2 J_0^2(\theta)}{(\lambda_s^2 - \theta^2)(\lambda_m^2 - \theta^2)} = \frac{3\pi}{2\lambda_m^2}. \quad (7)$$

In order to get the solution for Eq.(7) we will introduce an integer odd function  $f_1(z)$  the values of which in the points  $z = \lambda_s$  are equal  $f_1(\lambda_s) = w_s J_1(\lambda_s)$ . Let us assume that at  $|z| \rightarrow \infty$   $f_1(z)$  grows not faster than  $\exp(z)$ , then, in accordance with Cauchy theorem, the function  $(f(z)/J_0(z))$  can be expanded into the series over mere fractions

$$f_1(z)/J_0(z) = 2z \sum_{n=1}^{\infty} w_n / (\lambda_n^2 - z^2). \quad (8)$$

Using (8), and, also, multiplying Eq.(7) by  $J_1(\lambda_m x)/J_1(\lambda_m)$ , where  $0 < x < 1$ , and doing summation over sub-index  $m$ , we will get

$$\int_0^{\infty} f_1(z) J_1(xz) dz = 3\pi x / 2, \quad 0 < x < 1. \quad (9)$$

By multiplying (8) by  $z J_1(xz)$  and integrating over  $z$  from 0 to  $\infty$ , we will obtain at  $x > 1$ :

$$\int_0^{\infty} z f_1(z) J_1(xz) dz = 0, \quad x > 1. \quad (10)$$

In this way, the set of linear algebraic equations (7) with a complicated coefficients matrix that cannot be expressed via elementary functions and can be calculated only numerically, has been reduced to two integral equations (9,10). Having determined the kind of function  $f_1(z)$ , there is no need in calculating the sum (6), since

$$\Lambda = \sum_s w_s / \lambda_s^2 = \lim_{z \rightarrow 0} \left[ f_1(z) / \left\{ 2z J_0(z) \right\} \right]. \quad (11)$$

The method of solving the dual integral equations of the type (9,10) on the base of the Mellin transformation, as well as the property of Cauchy-type integrals, can be found in [7]. The brief summery of their solutions is given in [8]. We shall dwell briefly on a simpler method of resolving this system.

Since  $f_1(z)$  is the odd function it can be represented in the form  $f_1(z) = \int_0^{\infty} \sin(zt) \eta(t) dt$ . Substituting this expression in Eq.(10) we obtain such integral equation for  $\eta(t)$ :  $\int_x^{\infty} dt \eta(t) / \sqrt{t^2 - x^2} = 0$ ,  $x > 1$ . The solution of this equation is  $\eta(t) = 0$  for  $t > 1$ . Consequently, any function of the type

$$f_1(z) = \int_0^1 \sin(zt) \eta(t) dt \quad (12)$$

satisfies Eq.(10). Substituting (12) into (9), we obtain the first kind Volterra equation Abelian type

$$\int_0^x dt t \eta(t) / \sqrt{x^2 - t^2} = 3\pi x^2 / 2, \quad 0 < x < 1, \quad (13)$$

the solution for which can be found in the analytical form. Omitting the intermediate formulae, we shall give the final expression for the function  $f_1(z)$ :  $f_1(z) = 6 j_1(z)$ , where  $j_n(z)$  is the spherical Bessel function of order  $n$ .

The normalized coupling coefficients, as follows from (11), is equal to  $\Lambda = 1$ . Since  $w_s = f_1(\lambda_s) / J_1(\lambda_s)$ , then, from (4), we will obtain

$$E_r^{(-)}(r) = \frac{E_{0,q,p}^{(1)}(r=0) - E_{0,q,p}^{(2)}(r=0)}{\pi} \frac{r}{\sqrt{a^2 - r^2}}. \quad (13)$$

Thus, on the base of a rigorous electrodynamic description of the two cavity coupling system we are the first to prove, by the way of the limit transition  $a \rightarrow 0$ , the correctness of the equations formulated in the papers [4-6] on the basis of the quasi-static approximation, and

<sup>1</sup> The same is true for the right cross section

<sup>2</sup> We have neglected terms of order  $a^5$  in the expression for  $G_{m,s}$

<sup>3</sup> In this case, as follows from Eqs.(1), the coupling coefficients will be proportional to  $a^3$

to obtain the expression for the tangential electric field on the hole.

### 3.2 The case of small, though finite, values of coupling hole radius

The above method presents the opportunity to obtain analytical expressions for the normalized coupling coefficients with an accuracy on the order of  $(a/\lambda)^2$ . If  $a/\lambda$  is small, though finite, then, the coefficients  $w_s$  in (5) will be dependent on the hole radius value  $a$ :  $w_s = w_s(a)$ . Let's introduce the function of two variables:  $\psi(a, z) = 2z J_0(z) \sum_{n=1}^{\infty} w_n(a) / (\lambda_n^2 - z^2)$ . We

will assume that relative to the variable  $z$  the function  $\psi(a, z)$  will obey the conditions formulated in Subsec.3.1. Using the technique, similar to that described in Subsec.3.1, the set (5) can be reduced to:

$$\sum_{l=1}^{\infty} \theta_l J_1(x \theta_l) \psi(a, \theta_l) / \chi_l = 0, \quad 1 < x < b/a, \quad (14)$$

$$\pi \frac{a}{b} \sum_{l=1}^{\infty} \frac{J_1(x \theta_l) \psi(a, \theta_l) R_l}{\chi_l} = \frac{3\pi J_1(x \Omega_*)}{\Omega_* J_0(\Omega_*)}, \quad 0 < x < 1. \quad (15)$$

Letting  $a \rightarrow 0$  in Eqs.(14,15), we derive a set of equations (9,10), and, consequently,  $\psi(0, z) = f_1(z)$ .

Let's represent  $\psi(a, z)$  in the form  $\psi(a, z) = \psi(0, z) + a^2 \varphi(a, z)$ . From (14,15) it follows that  $\varphi(0, z)$  satisfies the following equations:

$$\int_0^{\infty} \theta J_1(x \theta) \varphi(0, \theta) d\theta = 0, \quad x > 1, \quad (16)$$

$$\int_0^{\infty} J_1(x \theta) \varphi(0, \theta) d\theta = F(x), \quad 0 < x < 1, \quad (17)$$

$$\text{where } F(x) = \frac{3\pi x}{8a^2} \left[ \Omega_*^2 - \Omega^2 - \frac{x^2}{4} (2\Omega_*^2 - \Omega^2) \right].$$

The solution of Eqs.(16,17) has the form

$$\varphi(0, z) = \frac{\Omega_*^2 - \Omega^2}{4a^2} f_1(z) - \frac{2\Omega_*^2 - \Omega^2}{2a^2} f_2(z), \quad (18)$$

where  $f_2(z) = j_3(z)/2 - 3j_1(z)/(2z^2)$ .

The normalized coupling coefficients  $\Lambda$ , accurate to the order  $(a/\lambda)^2$ , is determined by the relationship:

$$\Lambda \approx 1 - \frac{1}{5} \left( \frac{a \lambda_q}{b} \right)^2 - \frac{3}{20} \left( \frac{a \omega_{q,p}}{c} \right)^2 - \frac{1}{20} \left( \frac{a \omega}{c} \right)^2. \quad (19)$$

For the case  $\omega \approx \omega_{q,p}$  the expression (19) agrees with that for the generalized polarizability, obtained in [9] at  $b \rightarrow \infty$  via the variation technique. Note that the expression (19) is true for the frequency  $\omega$  that is not close to the resonant frequencies of the non-fundamental modes of closed cavities:  $\omega \neq \omega_{n,m}$  if  $(m, n) \neq (q, p)$ .

Knowing  $\psi(a, z)$ , and, consequently,  $w_s(a)$ , the form of

the tangential electric field around the hole can be reconstructed:

$$E_r^{(-)} = \frac{E_{0,q,p}^{(1)}(r=0) - E_{0,q,p}^{(2)}(r=0)}{\pi} \times \left\{ \left[ 1 - \frac{1}{4} \left( \frac{a}{b} \lambda_q \right)^2 + \frac{\Omega_*^2 - 2\Omega^2}{12} \right] \frac{r}{\sqrt{a^2 - r^2}} + \frac{2\Omega_*^2 - \Omega^2}{6} \frac{r}{a} \sqrt{1 - \left( \frac{r}{a} \right)^2} \right\}. \quad (20)$$

## 4 CONCLUSION

On the base of our method of reduction of the infinite linear algebraic equation set to dual integral equations, we obtained, in different limited cases, the rigorous analytical solutions regarding the two-cavity coupling problem. Alongside with general theory significance, the obtained solutions are of applied interest, since they can be used for a better convergence of the original equation solution (3), which are true for arbitrary dimensions of the coupling hole.

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## 5 REFERENCES

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