

CRYOGENIC CONTROL

The cryogenics from a refrigeration and liquefaction plant are provided to the CTC, cryogenic heat-exchanger box (HEX CAN) and HTC via a cold Processing Area Valve Box (PAVB) designed for testing CESR RF cryomodules. The liquid nitrogen (LN2) valve body and stem were extended and seat plug changed to convert the valve from manual to proportional control. For the CTC, only LN2 is needed. The HEX CAN and HTC require both LN2 and liquid helium (LHe). The HEX CAN has LN2 and LHe reservoirs.

The LN2 level stick is a commercial capacitive type sensor while the LHe stick is a resistive device. Both use commercial controllers with 4-20mA output sent to the PLC. PID loops in the PLC provide PAVB valve control and thus liquid level regulation. Cold helium gas return is operated in an open loop configuration.

The HTC takes cryogen supply and return via the HEX CAN. The system has a pre-cool circuit for slow cooldown via a manual valve. When the pre-cool is finished, the system switches to the normal helium loop.

The HTC has four 2K LHe level sticks installed in the two-phase line; two of the four are spares. The 2K helium level controllers send process variable (PV) signals to the PLC. The PLC output module control variable (CV) regulates the HEX CAN Joule-Thompson (JT) valve that supplies helium liquid to the HTC.

The HTC LHe level sticks look at both ends of the 2K two-phase line. Helium level differences at the ends of this line may provide useful data for control optimization. A Helium cold Gas Return Pipe (HGRP) is part of the 2K vacuum pumping line. The 2K return gas passes through a counter-flow heat exchanger where it pre-cools the incoming 4K helium just upstream of the JT valve. A resistive heater then warms the return gas to room temperature for a pumping skid. The operating pressure is between 23 and 12 Torr. The 2K pressure control is independent of the PLC. This loop is regulated with a PID controller. The PV for this loop is a room temperature capacitive manometer, and the CV for the pumping skid is an AC motor speed control.

CRYOMODULE SENSORS & INSTRUMENTATION

Temperature Sensors

Several types of temperature sensors are employed in these cryostats (see Table 1 and Figure 2):

- CLTS (Cryogenic Linear Temperature Sensor)
- PT100, PRT (Platinum Resistance Thermometer)
- AB-RT (Allen Bradley 100 Ohm Carbon Resistor)
- TC (Thermocouple, T-type and K-type)
- IR Sensor (Infrared Sensor)

CLTS's are 4-wire temperature sensors with a near linear response from ~300K to 4K. CLTS response at 2K will be tested with the HTC.

Table 1: List of temperature sensors.

Sensor	Temperature Range	Where used
CLTS	2K to 300K	CTC, HTC
PT100	73K to 450K	HTC
AB-RT	1.5 K to 20K	HTC
TC	77K to 450K	CTC, HTC
IR Sensor	233K to 873K	CTC

PT100's are 4-wire temperature sensors that have a resistance of 100 Ohms at 0°C and 134 Ohms at 100°C. These sensors will be used in the HTC to monitor RF coupler surfaces expected to operate above LN2 temperature. They will also be used as a PV for an *in-situ* coupler bake.

AB-RT's are 4-wire carbon resistor thermometers. These sensors are mounted on the HTC HGRP and inside the 2K two-phase helium line.

Both CTC and HTC use T-type thermocouples on the RF input couplers. The HTC tuner motor windings have a K-type thermocouple.

The CTC uses IR sensors to monitor RF coupler center conductor temperature near the cold ceramic. The unit is mounted inside the insulation vacuum. The HTC is not equipped with IR sensors.

Sensors were both demountable and permanently mounted where practical for reuse on subsequent tests.

RF Cables

HTC cavity RF field probes, WPM (Wire Position Monitor), HOM field probes are ported out of the cryomodule via 0.86" diameter, stainless steel, semi-rigid coaxial cables with SMA connectors. Cable layout has carefully designed routes inside the 80K shield. Right angle bends, and bulkhead connectors at the 80K shield reduce connection count. Cable between 80K and 300K is 0.141" diameter semi-flexible RF coax. Due to low radiation levels for the HTC, all RF cables in the HTC have PTFE dielectric.

Cavity Tuner, Piezo and Motor

The HTC has four piezo tuner actuators, each with an integral force sensor. The tuner motor is specifically designed for cryogenic operation and is driven with a compatible linear stepper motor drive.

HTC Heaters

The HTC is equipped with several heaters. The 2K two-phase line has a 10 watt heater for calibration and load leveling. The HOM loads have 400 watt (80K loop) and 10 watt (5K loop) heaters for calibration.

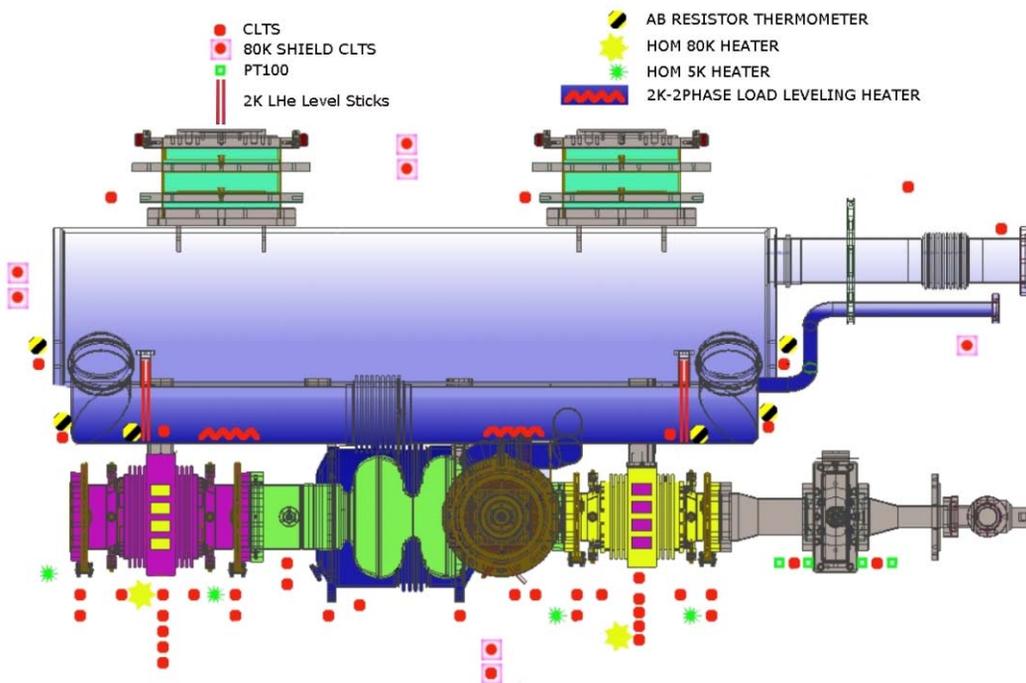


Figure 2: Temperature sensor map of HTC (input coupler sensors not shown).

IN-SITU INPUT COUPLER BAKE

For the HTC the plan is to bake the couplers *in-situ* with insulation vacuum established. Four Kapton™ film heaters will be mounted on each coupler, three inside the insulation vacuum space and one outside. Hot air will be blown into the coupler center conductor cooling port. As the cavity and tuner motor cannot get much hotter than 30°C, cool gas will be forced through the 5K circuit. The 2K circuit will be purged with nitrogen.

DATA ACQUISITION AND USER INTERFACE

CTC data acquisition was done by modifying the CESR Digital Cryogenic control system [4] installed for CESR cryomodule testing. A breakout box was designed and built to take advantage of the built in modularity of the digital control system. The interface between the breakout box and the PLC rack remained unchanged.

The HTC uses the same data acquisition equipment as the CTC with some additions and modifications. The Sensoray 2519DIN is a sixteen channel A/D converter with an imbedded Ethernet interface along with a combination of commercial and in-house built signal conditioners. The A/D converter takes 4-wire sensor inputs and ports conditioned signals directly to the lab subnet for viewing, in this case, with EPICS. To avoid potential network problems, all control loops are hardwired to the PLC.

CONCLUSIONS

The *in-situ* coupler bake, if successful, will reduce cryomodule assembly and conditioning lead time. The CTC and HTC provided a window into the challenges of getting a cryomodule instrumented from sensor to displaying of acquired data. This information will prove useful when designing the same system for the Cornell ERL Injector Cryomodule and beyond.

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