

DEVELOPMENT OF A MOVABLE COLLIMATOR WITH LOW BEAM IMPEDANCE

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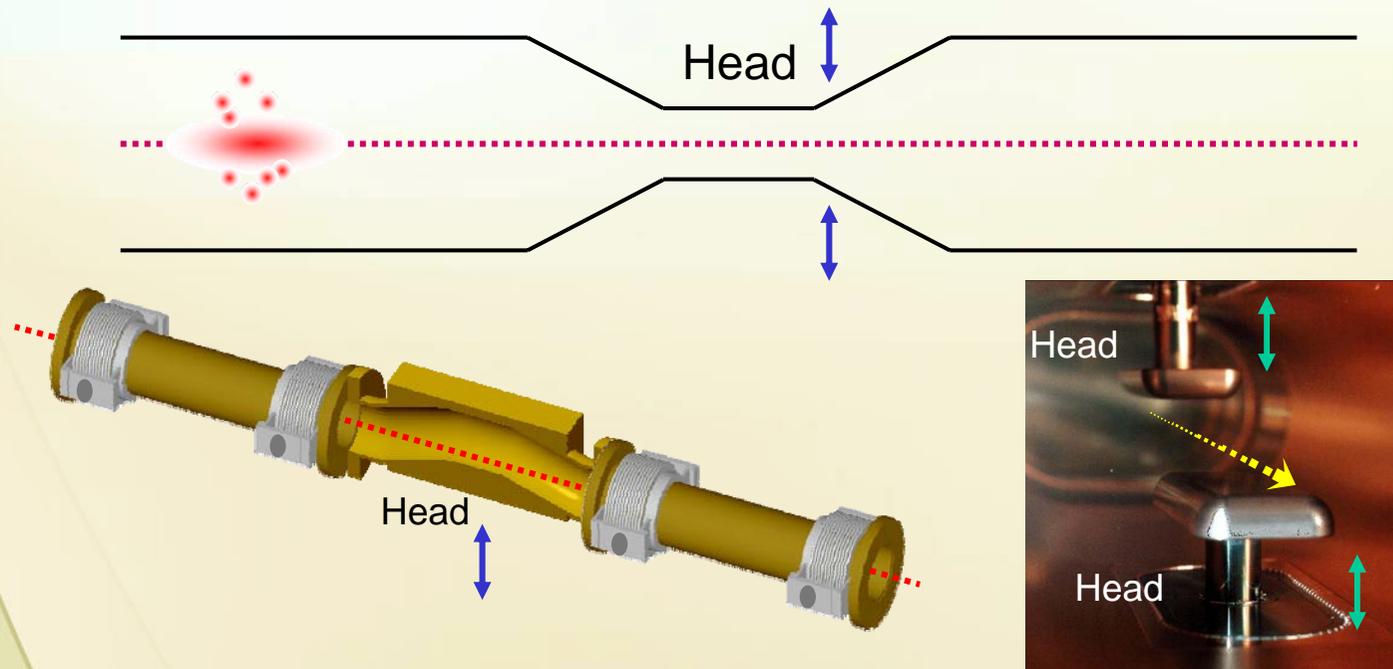
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1. Introduction

- Collimator

- Called as a mask or a scraper.
- A vacuum component equipped in colliders to cut off spent particles around a nominal beam orbit, and then to decrease the background of the detector.

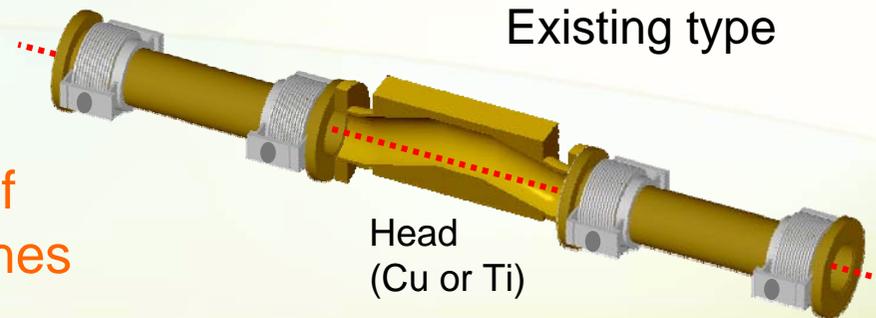
Collimators (Masks, Scrapers)



1. Introduction

- Problem in high-intensity colliders:
 - Structurally high beam impedance.

Loss Factor $\sim 1 \times 10^{12} \text{ V C}^{-1}$
(@ $\sigma_z = 3 \text{ mm}$)
200 kW for a beam current of
10A with 5000 bunches



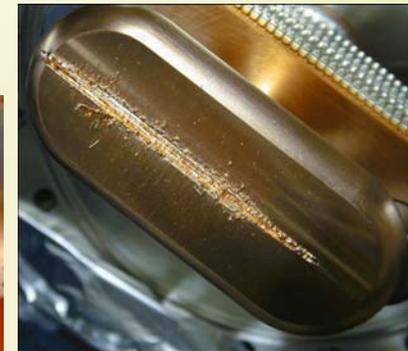
- Damage to the head due to direct striking of the intense beam.



New ideas?



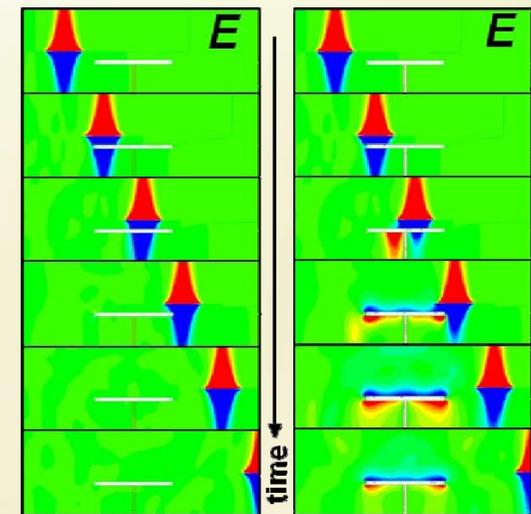
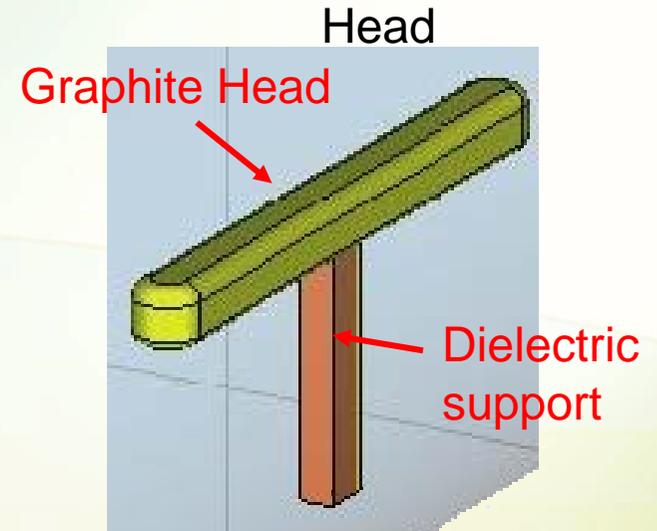
Cu (Observed even in Ti)



Cu

2. New Structure

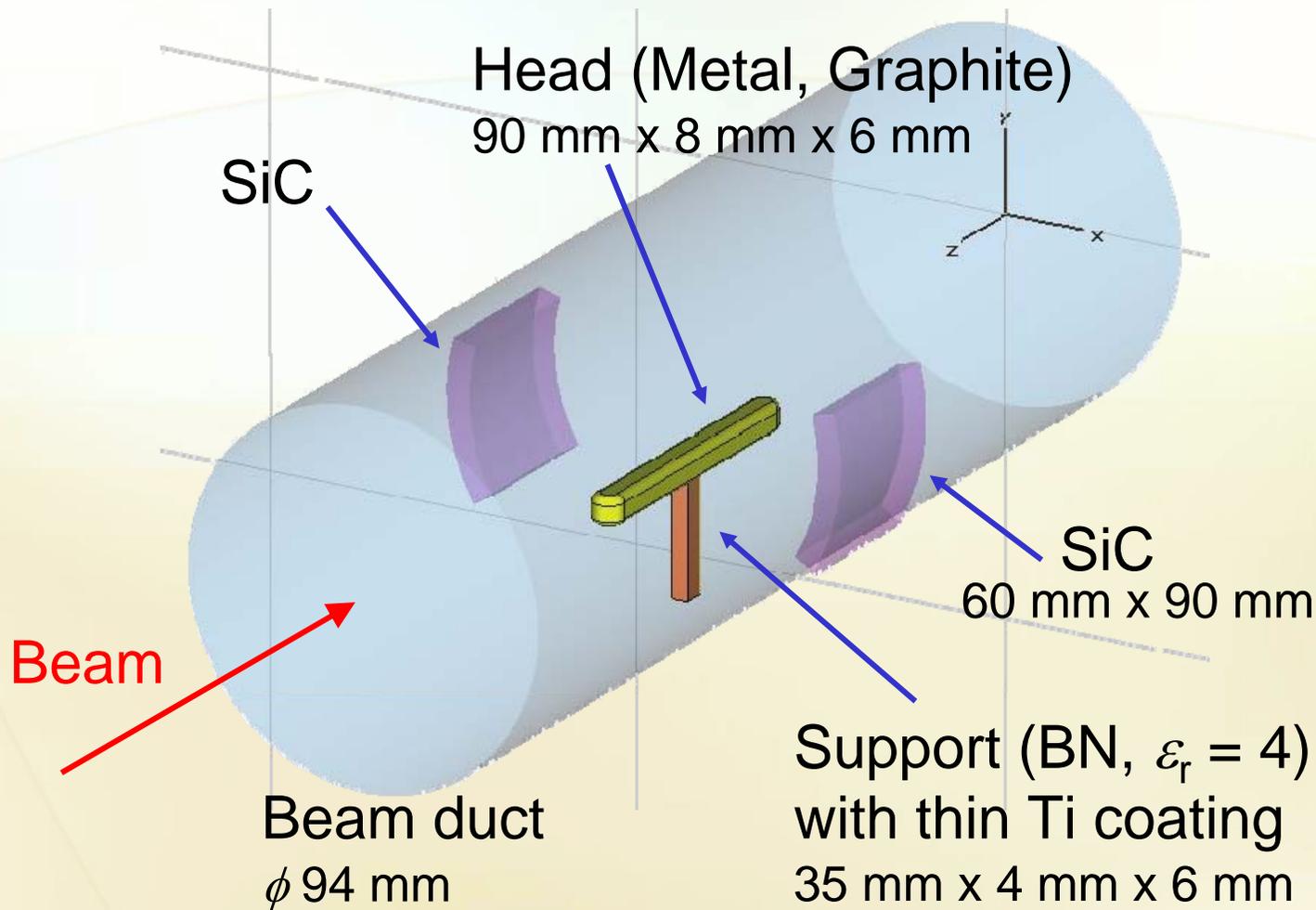
- Proposed here*
 - Dielectric (ceramics) support:
 - Reduce interference with beam
 - Similar idea to an “invisible electrode” by F. Caspers (1987)
 - Graphite head:
 - Higher thermal strength than other metals
 - Thin conductive layer on the support to avoid the unnecessary charge up of the head.
 - HOM (Higher Order Modes) absorber (SiC, for example) near to the head.



*Y. Suetsugu, K. Shibata, A. Morishige, Y. Suzuki and M. Tsuchiya, PRST-AB, 9 (2006) 103501.

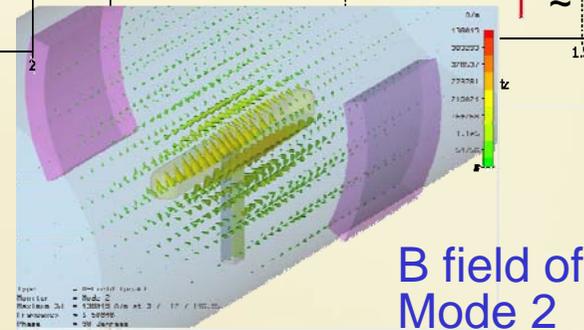
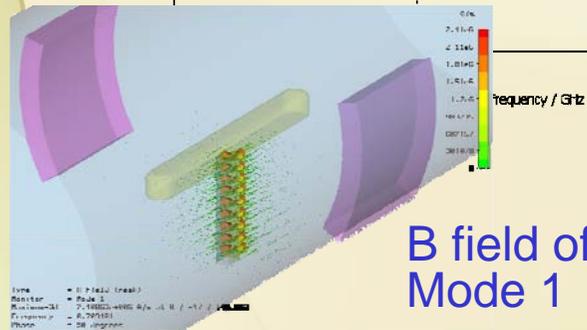
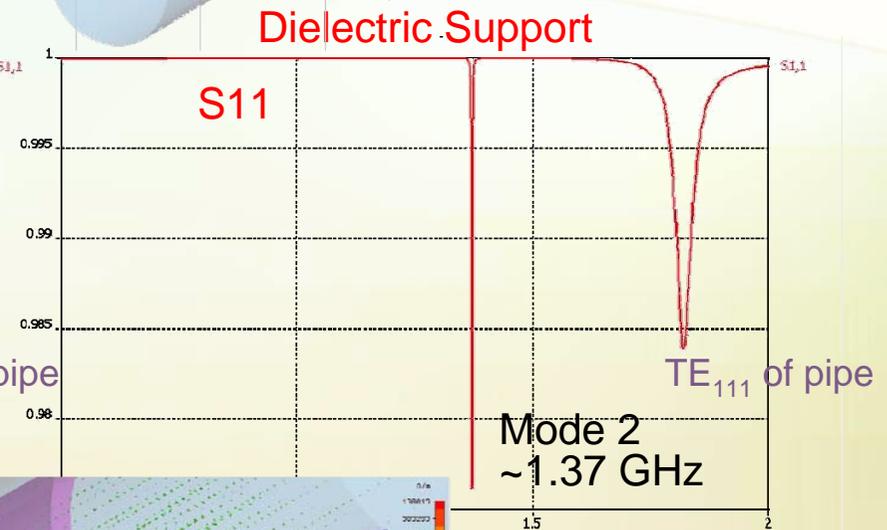
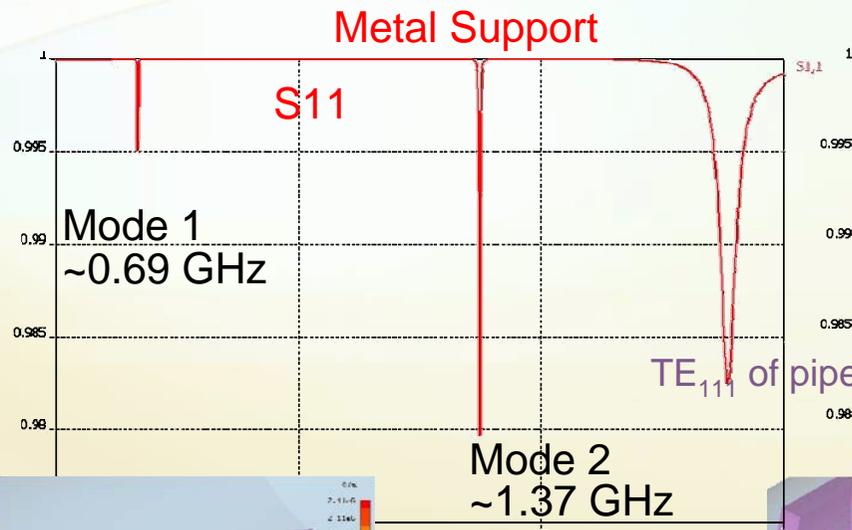
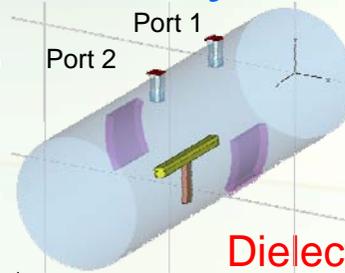
2. New Structure

- Design Model
 - Used for simulation



3. Properties

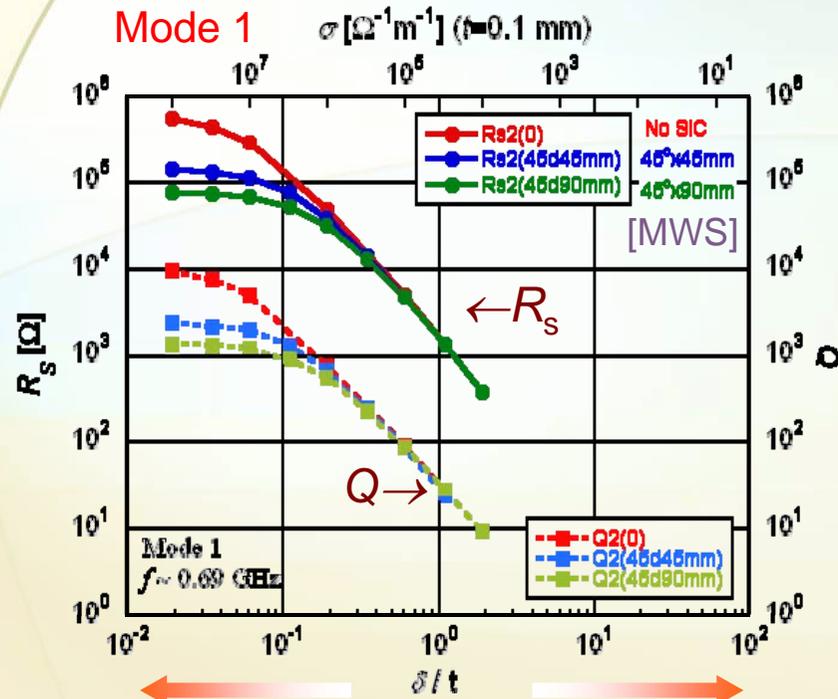
- RF properties were calculated by MAFIA and Microwave Studio [MWS].
- Trapped Modes



3. Properties

• Longitudinal Impedance of Trapped Modes

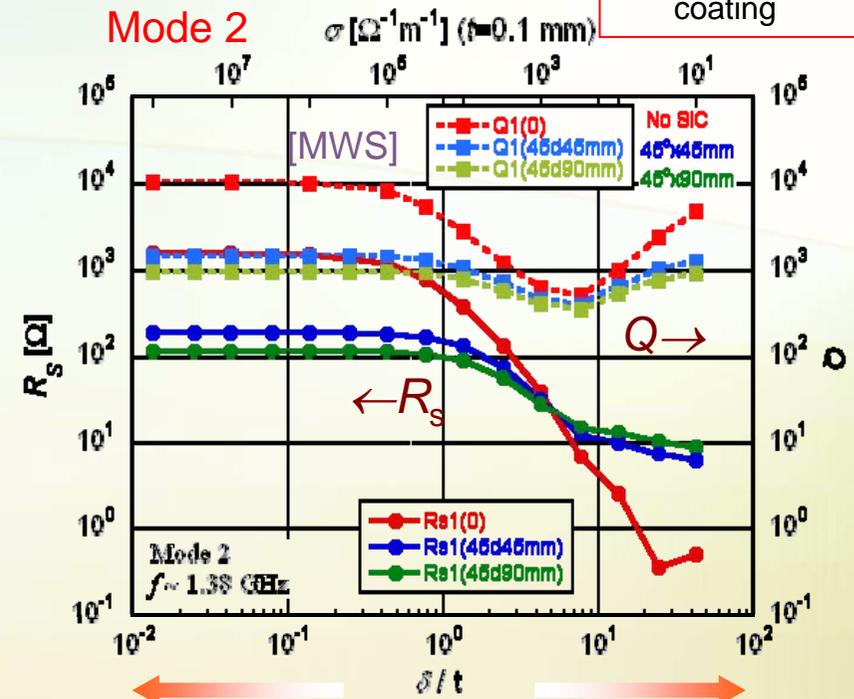
δ = skin depth
 t = thickness of coating



← Metal support Dielectric support →

At $\delta/t \sim 1$

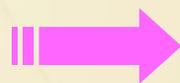
- $R_s \sim 1$ k Ω , $R_s/Q \sim 50$ [MWS]
- $R_s \sim 1$ k Ω , $R_s/Q \sim 200$ [MAFIA]



← Metal support Dielectric support →

At $\delta/t = 1 \sim 10$

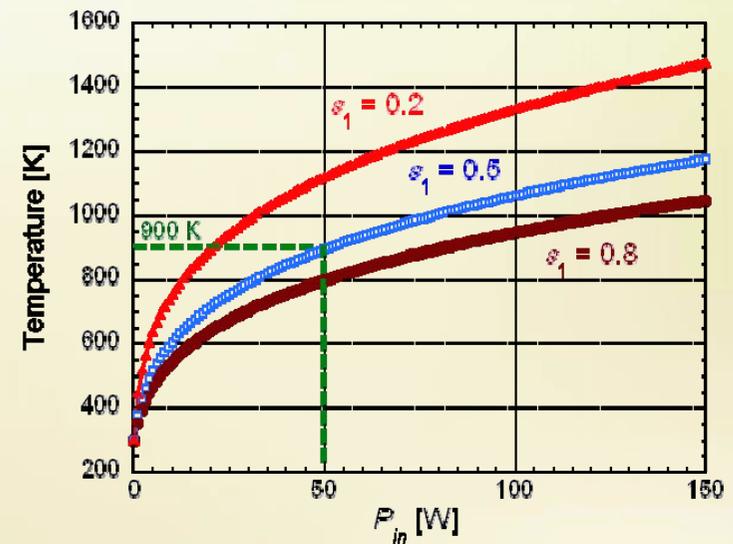
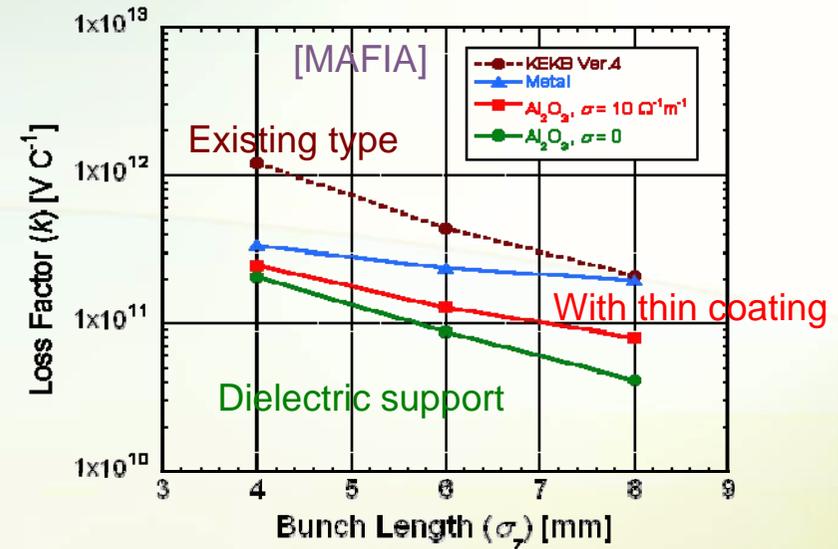
- $R_s = 100 \sim 10$ Ω , $R_s/Q = 0.1 \sim 0.02$ [MWS]
- $R_s = 100 \sim 10$ Ω , $R_s/Q = 0.5 \sim 0.05$ [MAFIA]



No longitudinal multi-bunch instability for $\delta/t > 3$
 Similar results for transverse instability

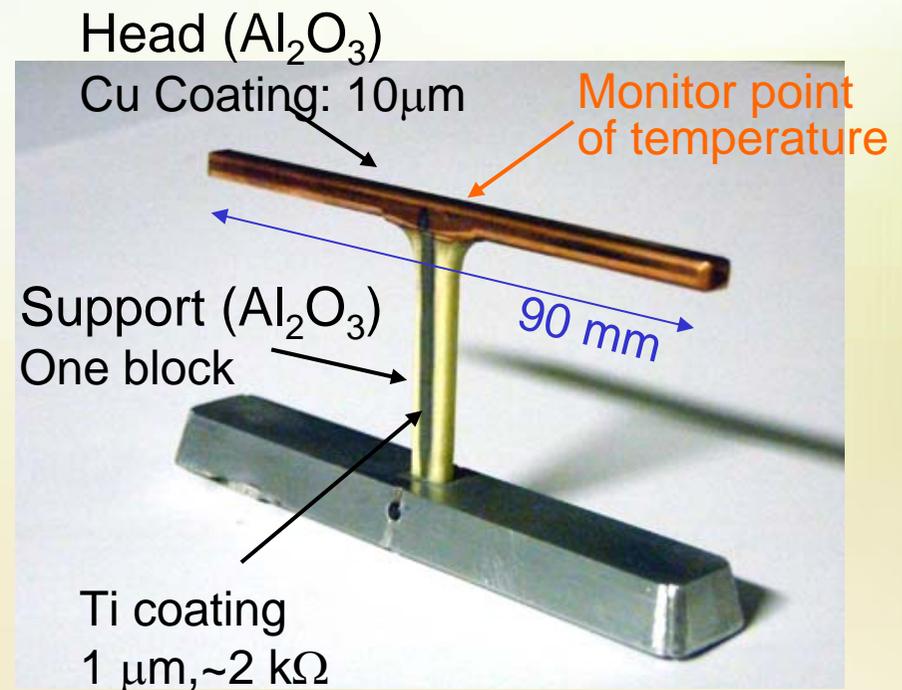
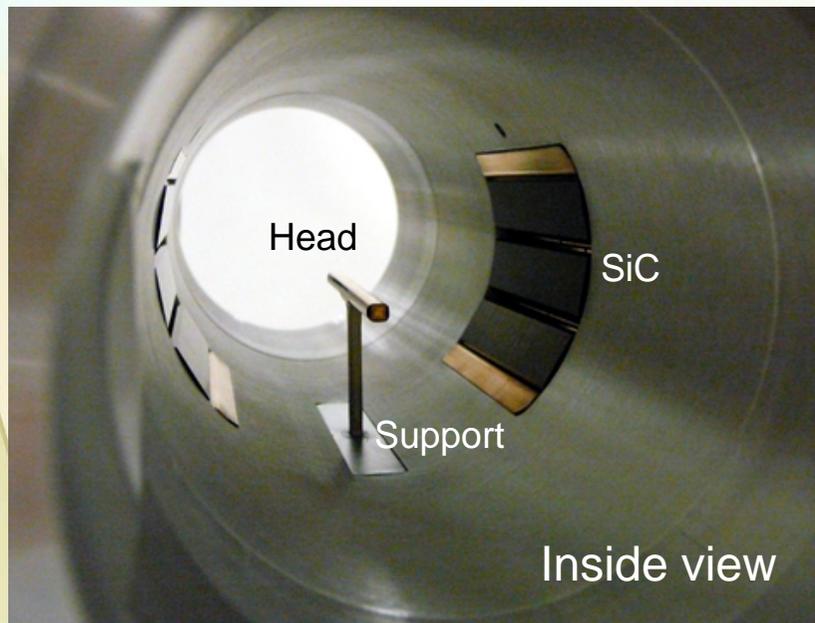
3. Properties

- Loss factors (without SiC)
 - Loss factor reduce to about 1/4 of conventional type.
- Heating
 - Heat transfer
 - Radiation
 - Considered input power
 - Trapped mode (Mode 2)
 - Joule loss
 - Negligible dielectric loss
 - Expected temperature
 - Input power ~ 50 W even at 10 A (5000 bunches)
 - ~1200 K, at most



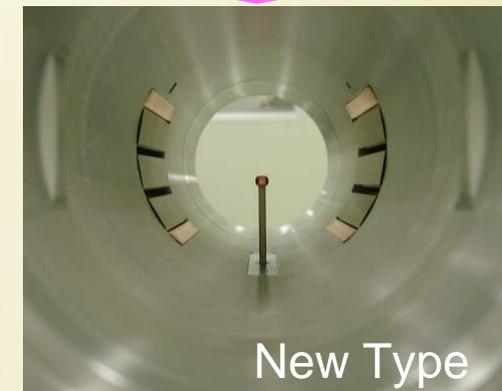
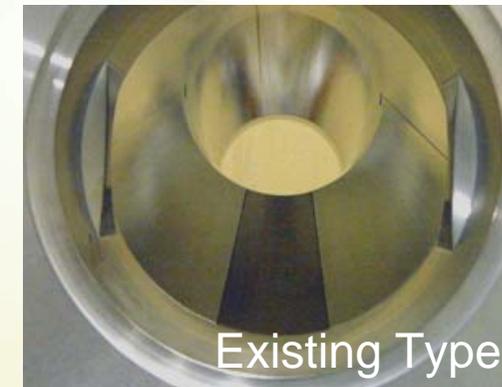
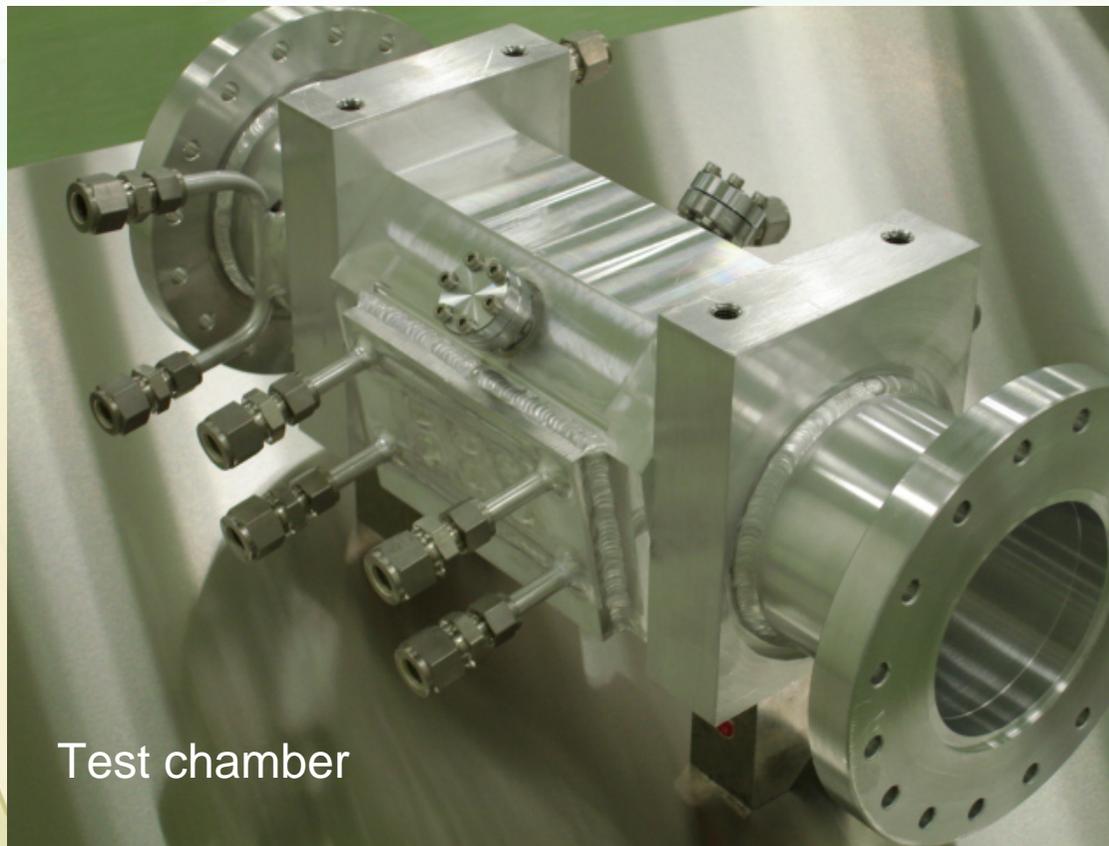
4. First Test Model

- Based on the simulation study, the first test model was manufactured.
- Simplified structure:
 - Aim proof of principle at low beam current
 - Make assembly easy



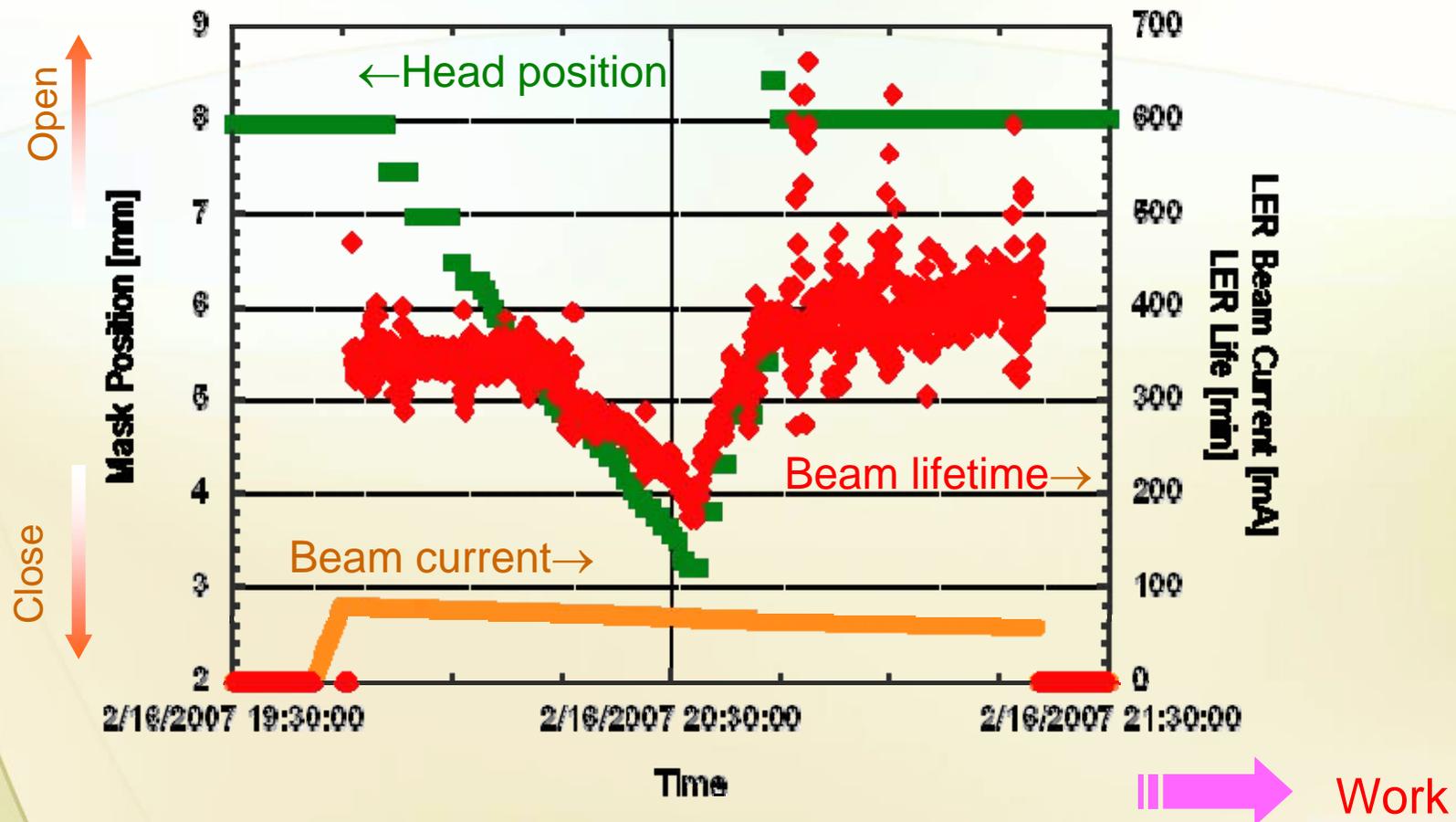
4. First Test Model

- Installed into the KEK B-factory ring
 - 3.5 GeV positron ring (LER)
 - Typically, $I = 1700$ mA, $N_b = 1389$ bunches, $\sigma_z = 6$ mm



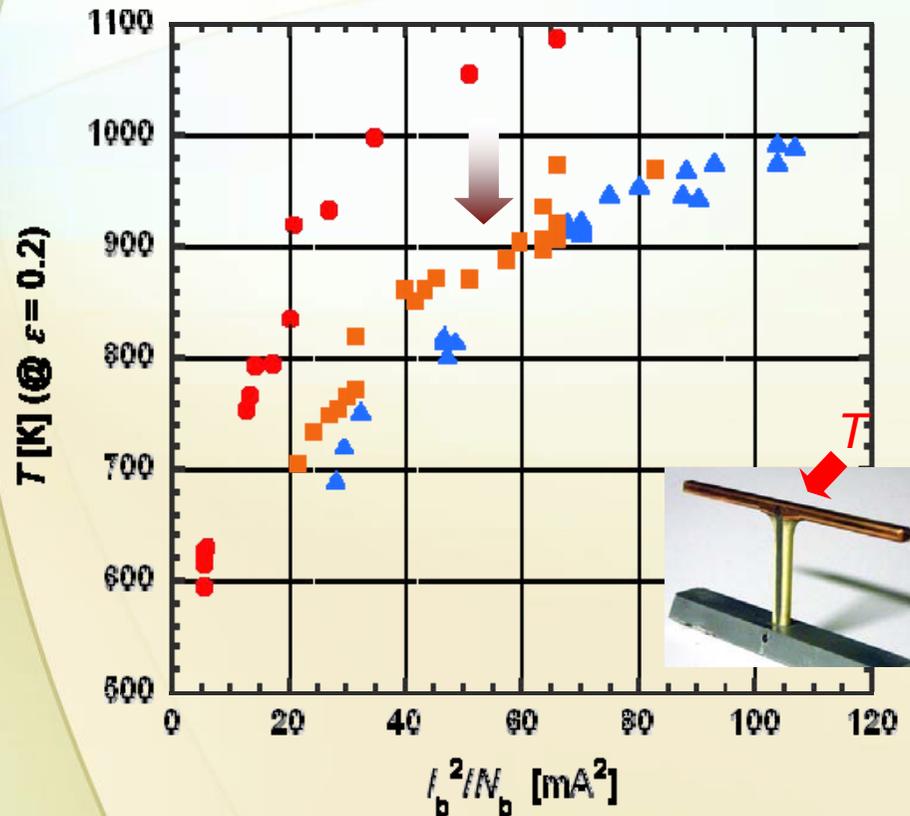
4. First Test Model

- Function as a collimator
 - Beam lifetime vs. head position



5. Problem

- Heating problem
 - Contrary to our expectation, extra heating was observed from the beginning of beam operation



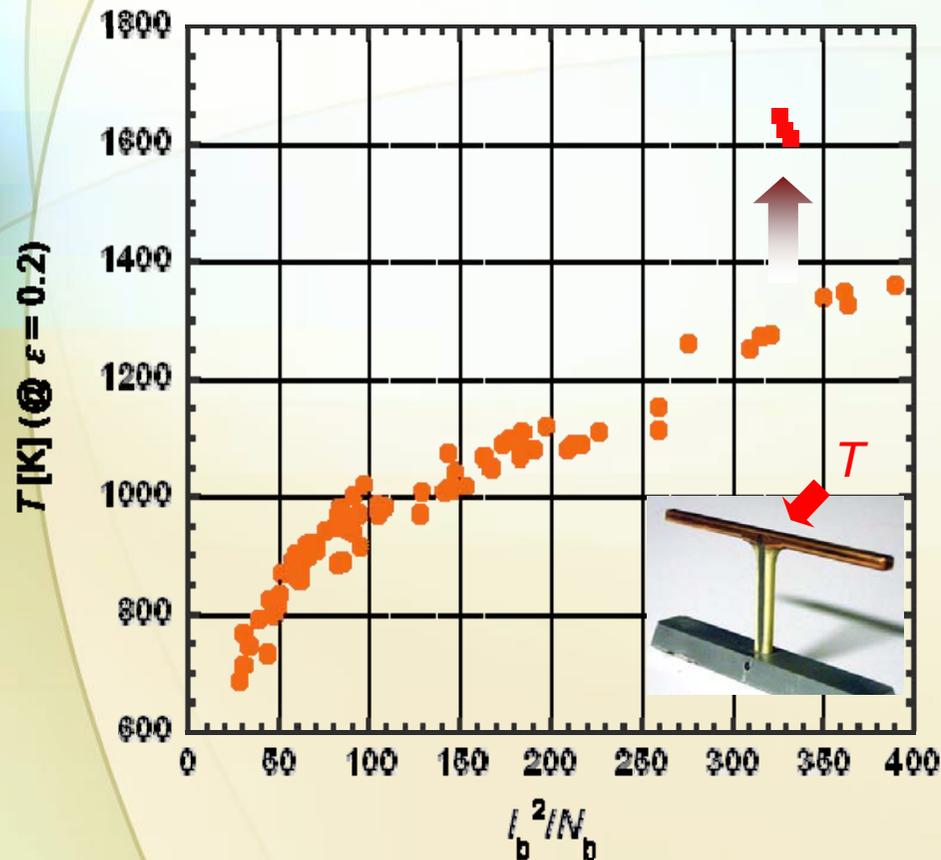
- At 42 mA (51 bunches) [$I_b^2/N_b = 35 \text{ mA}^2$], $T \sim 1000\text{K!}$ ($\epsilon = 0.2$ was set)
- After several days operation, the temperature decreased.



Change of surface condition or structure ?

5. Problem

- Heating problem



- Temperature was stable for a while.
- Temperature depends on I_b^2/N_b rather than I .

➡ Input power = HOM

- At 700 mA (1389 bunches) [$I_b^2/N_b = 353 \text{ mA}^2$], a pressure burst, and then extra heating was observed.

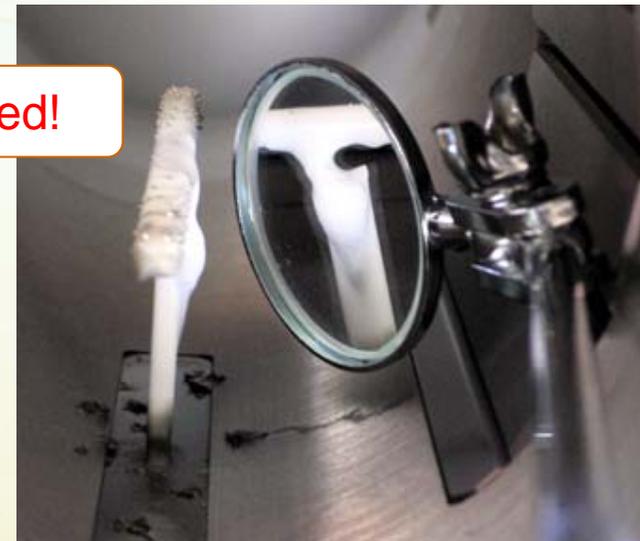
⬇ Inside Inspection by breaking vacuum

5. Problem

- Inside Inspection
 - Damage of head was found!



Side view

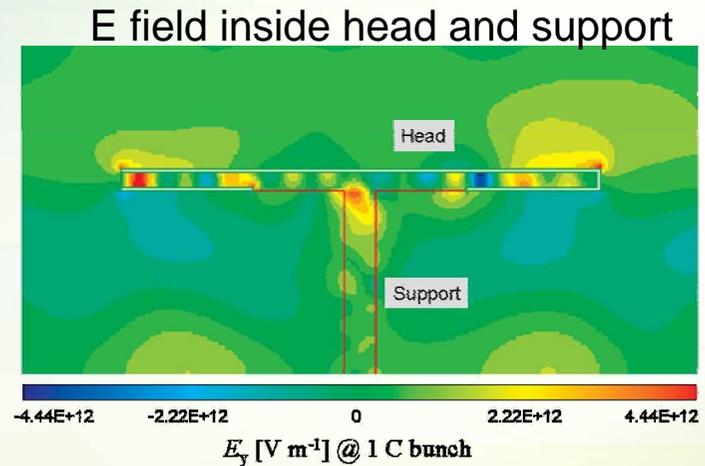


➡ Actually heated up!

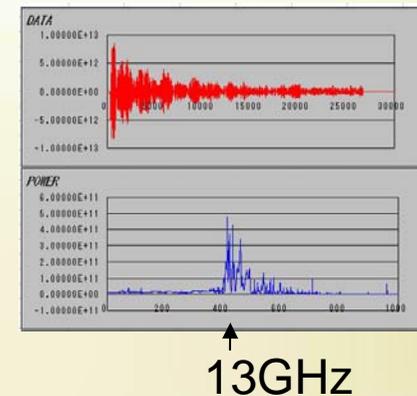
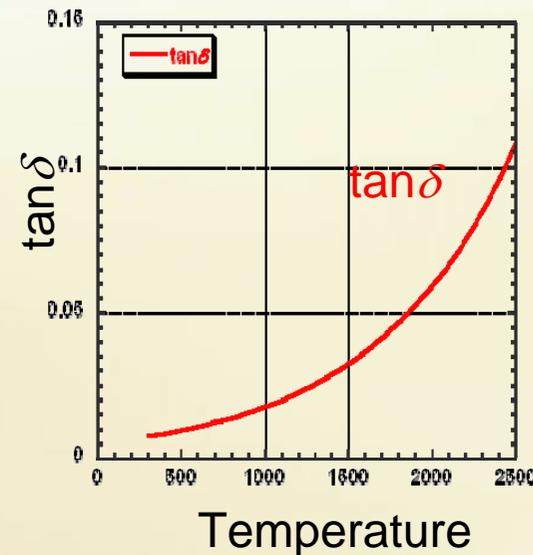
5. Problem

- What is the cause of failure?

- Structure of head; the Al_2O_3 head with Cu coating formed an rf cavity. The connection part of the support became a window of the cavity.



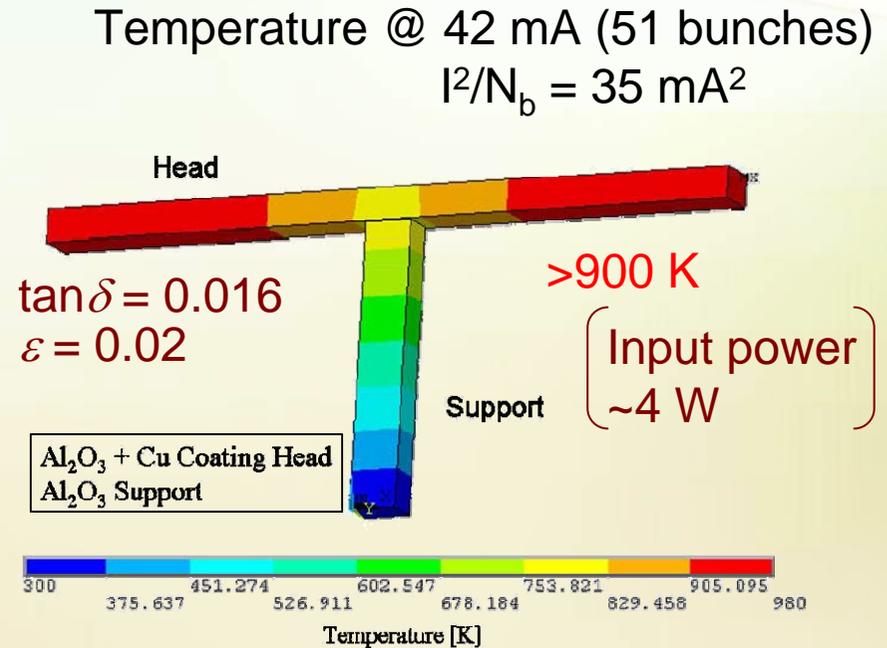
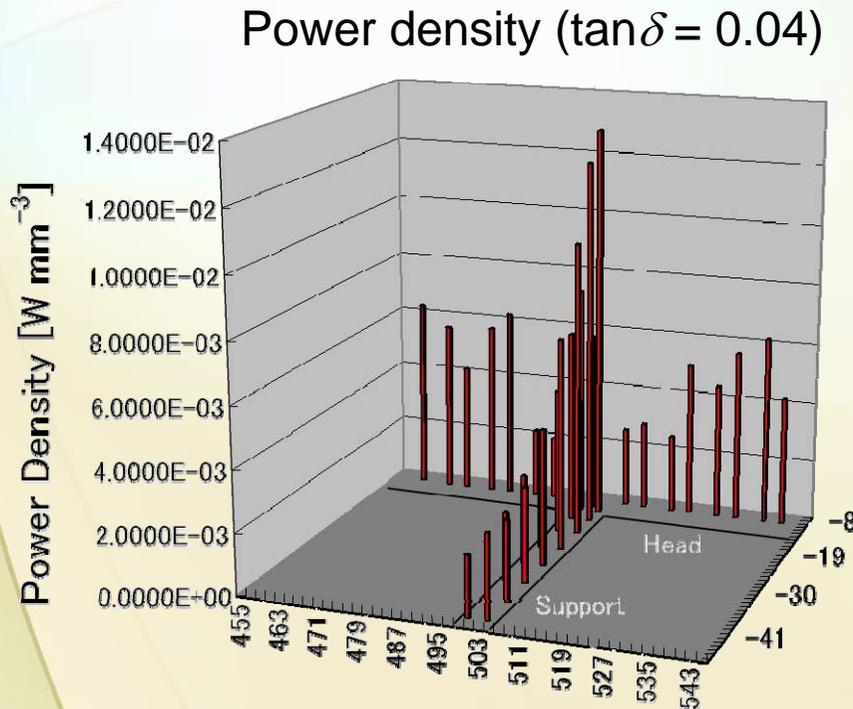
- Increase of $\tan \delta$ (loss tangent); the increase of $\tan \delta$ at high temperature and also high frequencies was under estimated.



5. Problem

- Thermal Analysis-1

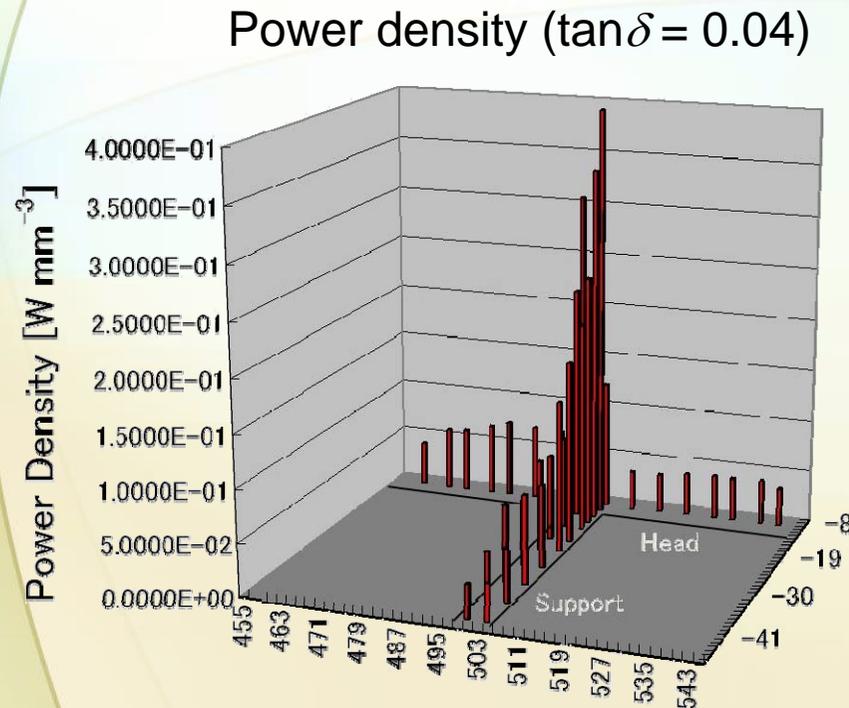
- Including dielectric loss considering the temperature dependence of $\tan \delta$
- For the original structure of the first test model



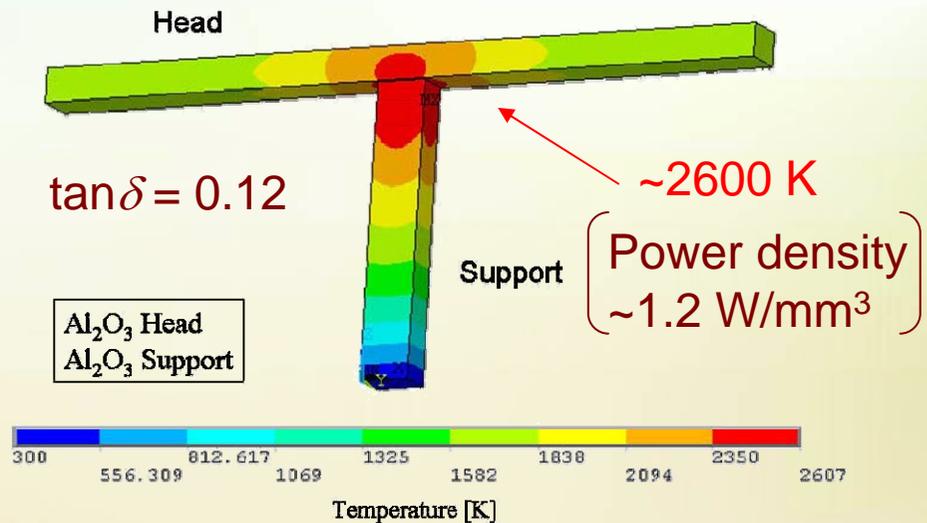
➡ Enough to evaporate Cu
(Vapor pressure $\sim 1 \times 10^{-6}$ Pa at 800 K)

5. Problem

- Thermal Analysis
 - After evaporation of copper coating



Temperature @ 700 mA (1389 bunches)
 $I^2/N_b = 353 \text{ mA}^2$



➡ Highest at connection
Enough to melt Al₂O₃

➡ Heating phenomena was well explained using reasonable parameters

6. Next Models

- Designed based on experiences in the first model
 - The same structure in principle, but appropriate choice of materials.
 - Temperatures for several promising materials were estimated similarly.

Promising materials

| | Materials | Electric Conductivity (1/Ωm) | Thermal Conductivity* (W/m/K) | Relative dielectric constant | Emissivity |
|---------|--------------------------------------|------------------------------|-------------------------------|------------------------------|------------|
| Head | Copper | 5.8x10 ⁷ | (400) | | 0.02 |
| | Graphite | 1x10 ⁵ | 50 | | 0.7 |
| Support | Al ₂ O ₃ (99%) | | 10 | 10 | 0.5 |
| | BN | | 20 | 4 | 0.5 |
| | Quartz (SiO ₂) | | 1.5 | 4 | 0.5 |
| | AlN | | 100 | 9 | 0.5 |
| | Diamond | | 500 | 6 | 0.4 |

* ~1/2 of the values at room temperature

6. Next Models

- Expected temperatures
 - Most promising combination is Graphite head and Diamond support.
 - Good thermal conductivity of diamond stabilizes the performance.

| Material of Head | Material of support | Max. T (K) (I ² /N=353) | Max. T(K) (I ² /N=2000) | Loss Factor (V/C) |
|--------------------------------|--------------------------------|---------------------------------------|---------------------------------------|----------------------|
| Cu (Coating) | Al ₂ O ₃ | (980 @42mA,#51) | Present KEKB | 1.4x10 ¹¹ |
| Al ₂ O ₃ | Al ₂ O ₃ | 2607 | | 3.7x10 ¹¹ |
| Graphite | Al ₂ O ₃ | 800 | | 7.9x10 ¹⁰ |
| Graphite | Quarts Glass | 706 | | 2.7x10 ¹⁰ |
| Graphite | AlN | ~480 | 1220 | 7.9x10 ¹⁰ |
| Graphite | BN | ~580 | 1078 | 2.7x10 ¹⁰ |
| Graphite | Diamond* | ~410 | ~730 | 2.1x10 ¹⁰ |

*1.2 mm x 5 mm x 35 mm



Second model is now under testing (Brazing of diamond etc.)

7. Conclusions

- New structure of movable collimator was proposed.
- First test model was designed and tested with beam at the KEKB positron ring.
 - Extra heating was observed at considerably lower beam current than expected.
 - Provided a valuable experience, and taught us a renewed recognition of the difficulty in dealing intense HOM.
- Next model was designed based on the experience.
 - The Most promising structure is graphite head supported by diamond.
 - The second model was under design.



- End

- Estimation of temperature taking into account the temperature dependence of $\tan \delta$

