

Coherent Radiation Diagnostics for Short Bunches

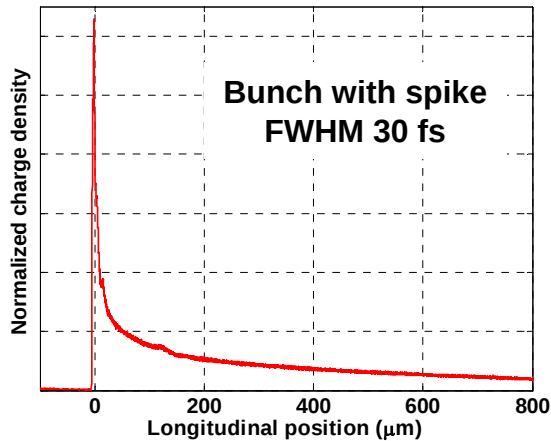
Bunch length measurement in the frequency domain

Oliver Grimm

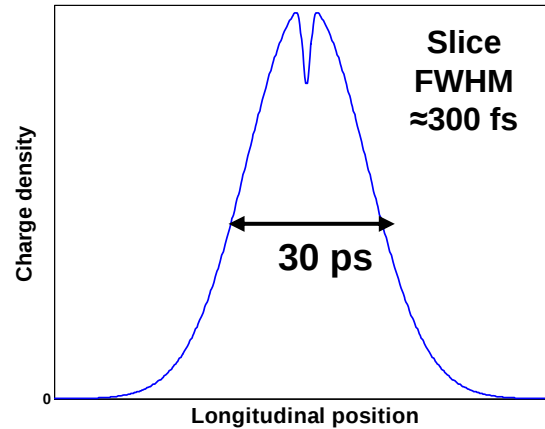
**PAC, Albuquerque
28 June 2007**

The **longitudinal charge distribution** is an important parameter for machine operation...

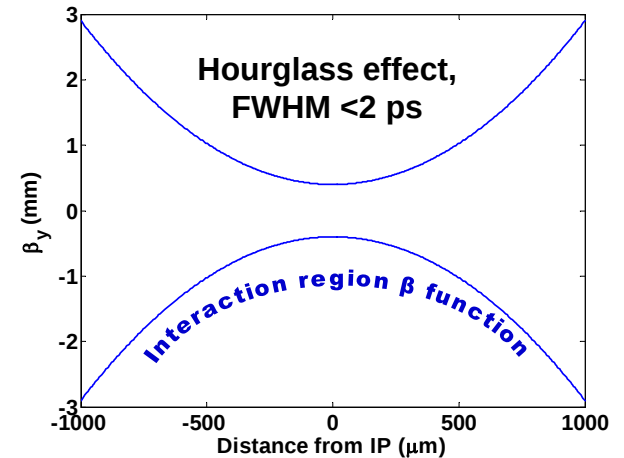
FEL



Bunch slicing

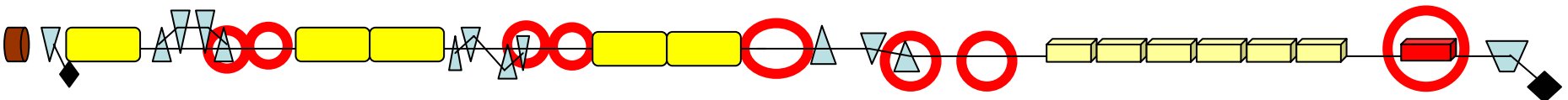


Linear collider



... and **difficult to measure** (non-destructively)
for short and/or complicated bunches.

Example for CRD at FLASH (FEL at DESY)

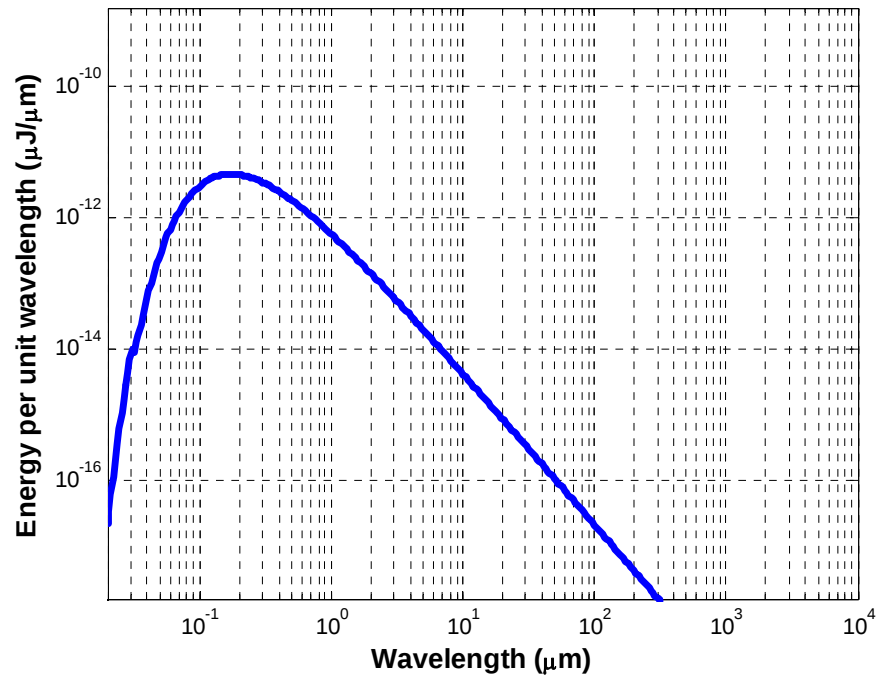


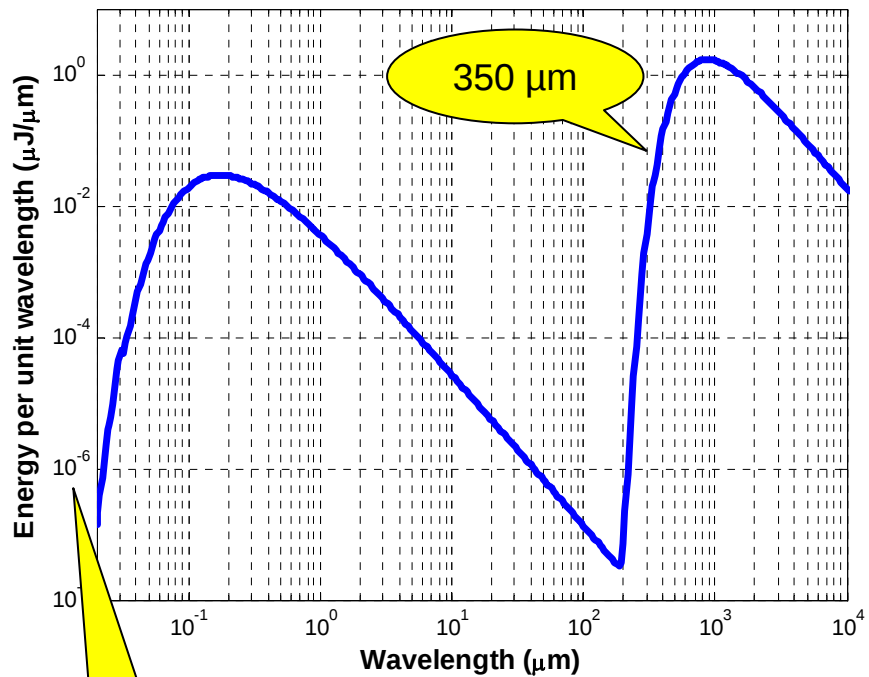
...also used at ALS, ANKA, BESSY, JAERI, NewSubaru, LCLS, SLS, UVSOR-II, ,...

Illustration of basic principle of CRD

Single electron synchrotron radiation spectrum

Circular motion, 130 MeV, $R=1.6$ m

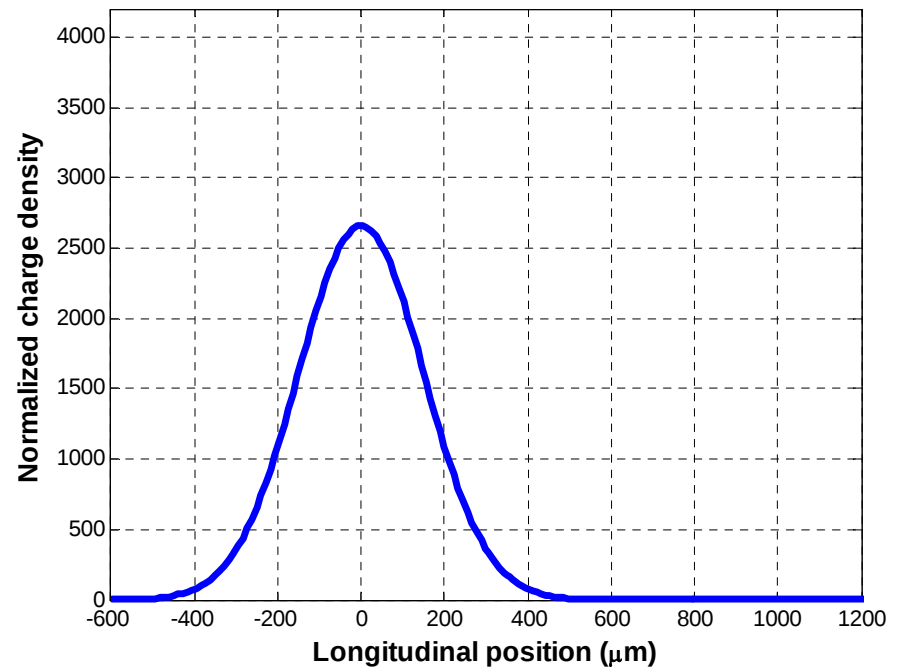


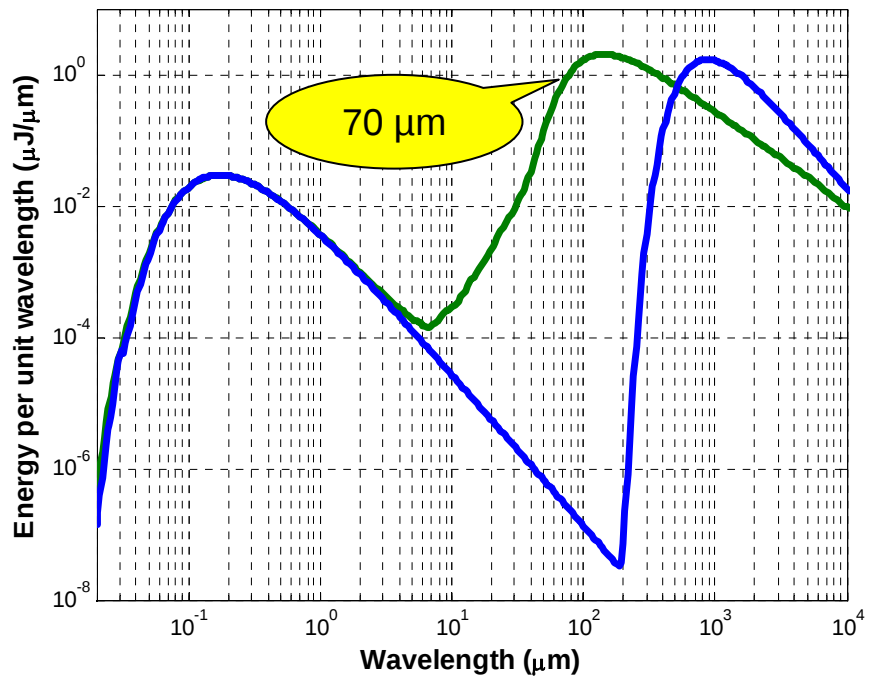


Charge 1 nC

Gaussian (line) bunch

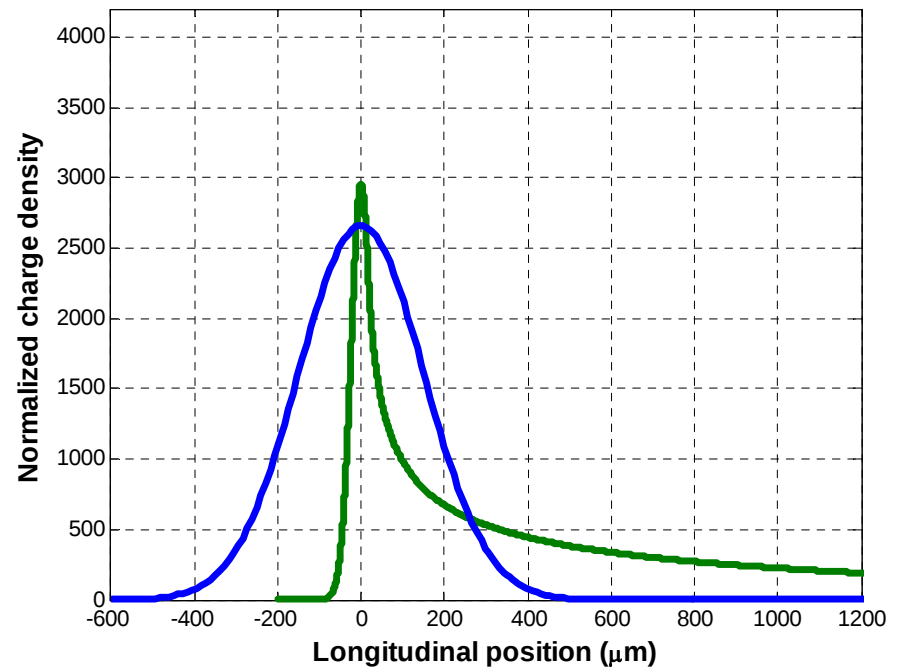
FWHM=350 μm

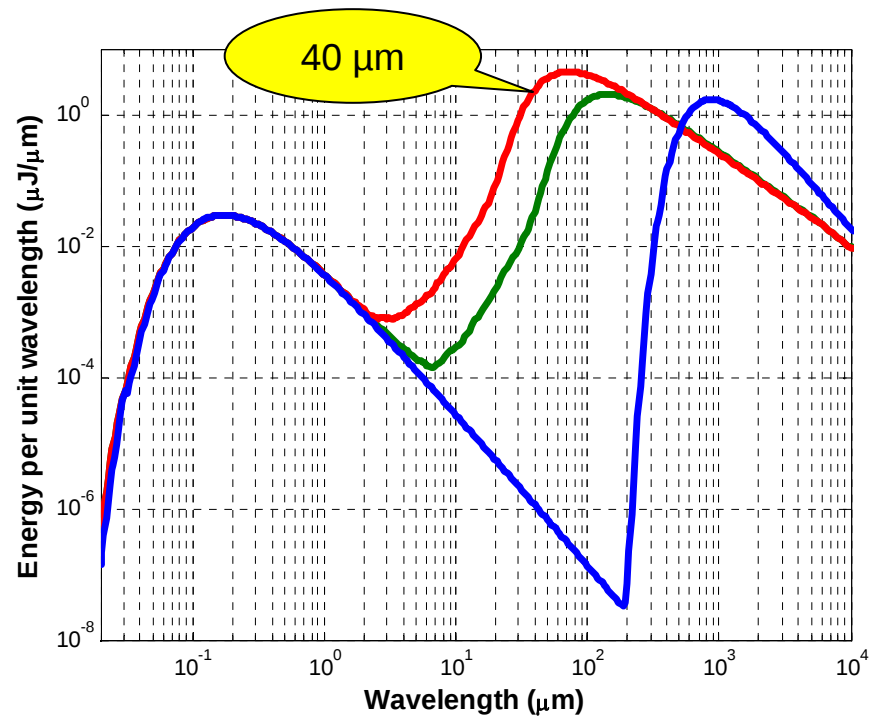




Spiked bunch

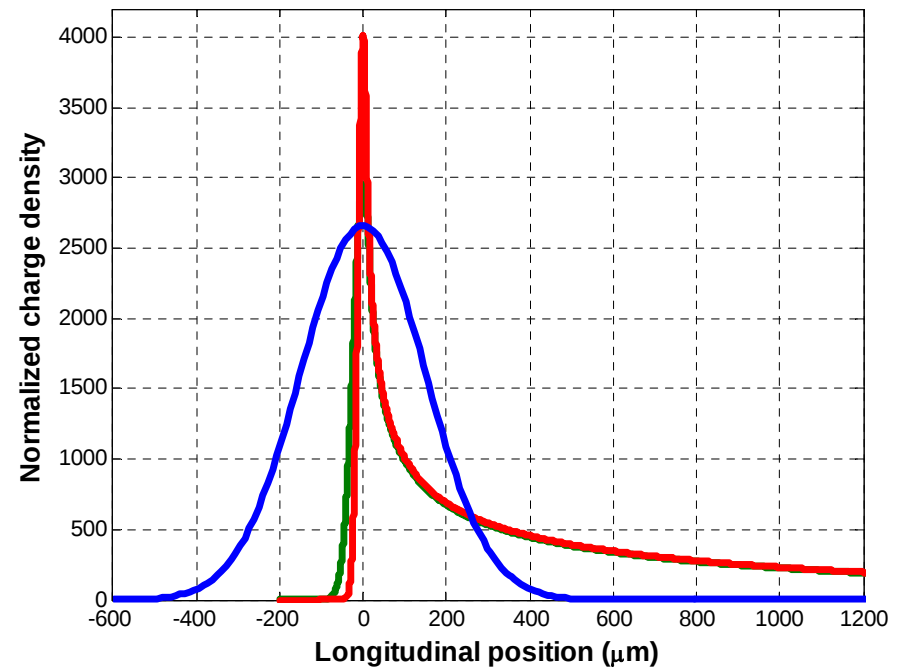
FWHM=70 μm





Spiked bunch

FWHM=40 μm



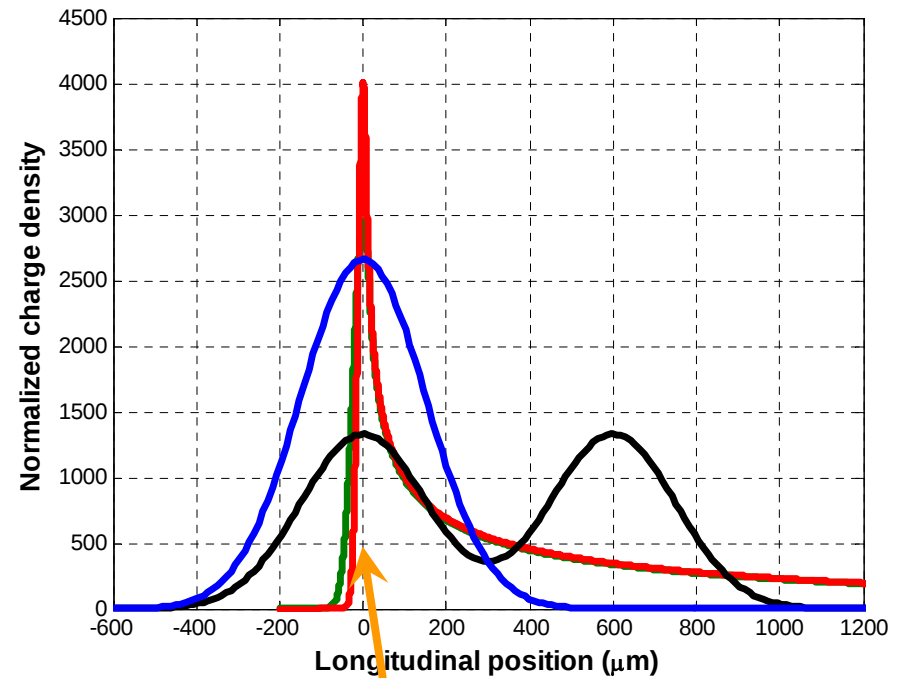
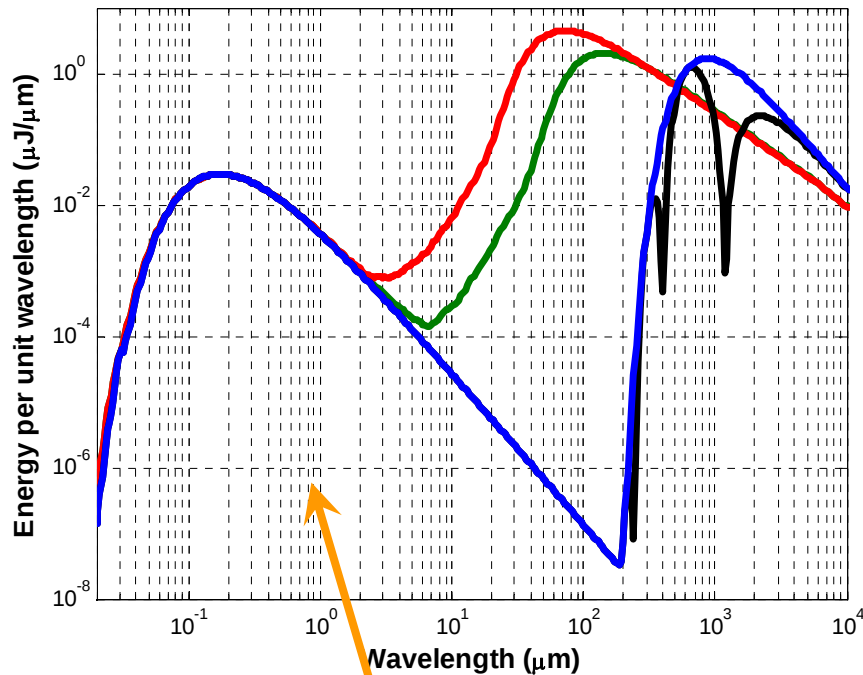
Basic relation of CRD

Emission spectrum depends on *longitudinal* charge distribution.

Transverse effects exist, not covered

Double Gaussian Bunch

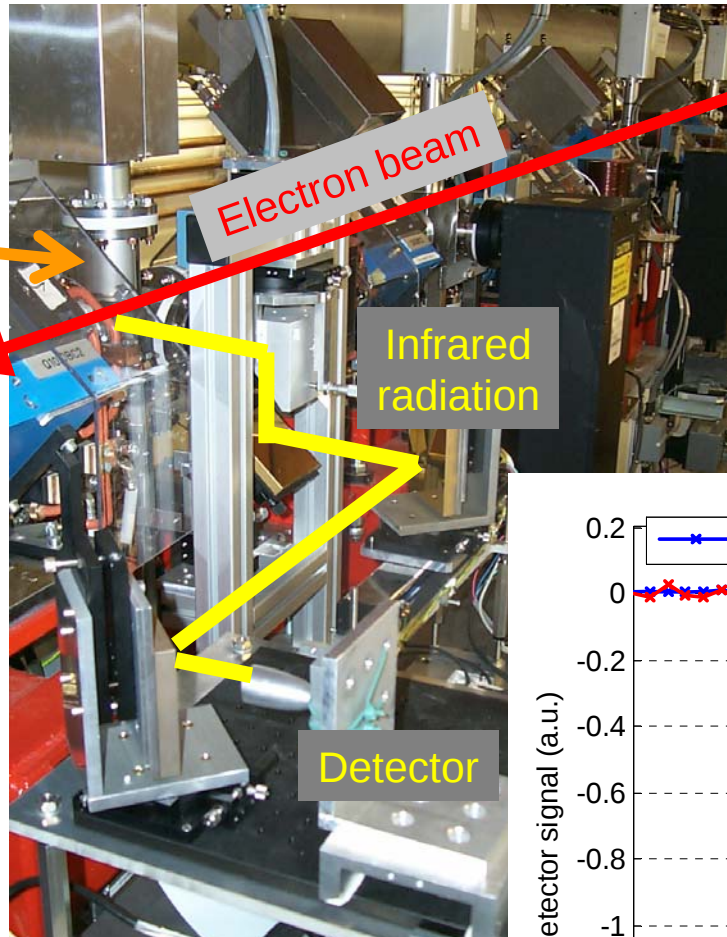
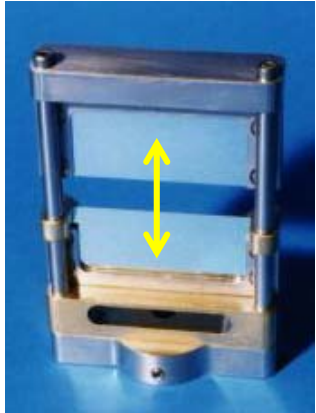
FWHM=350 μm , $\Delta=600$ μm



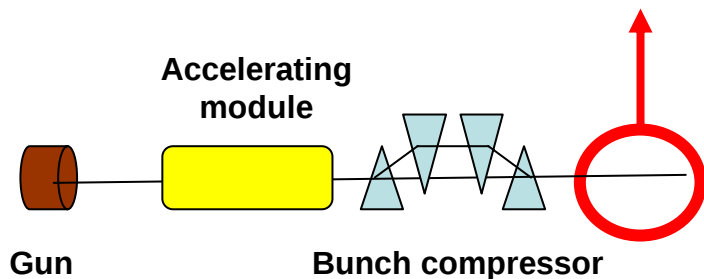
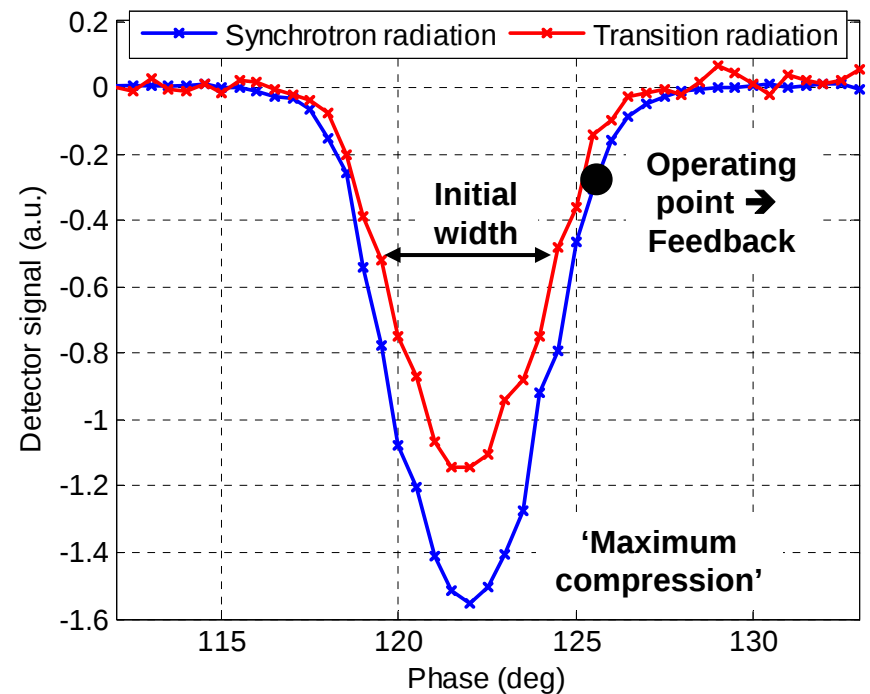
$$\frac{dU}{d\lambda} = \left(\frac{dU}{d\lambda} \right)_1 \left(N + N(N-1) |F(\lambda)|^2 \right) \quad F(\lambda) = \int S(z) e^{\frac{2\pi i z}{\lambda}} dz$$

Bunch compression monitor

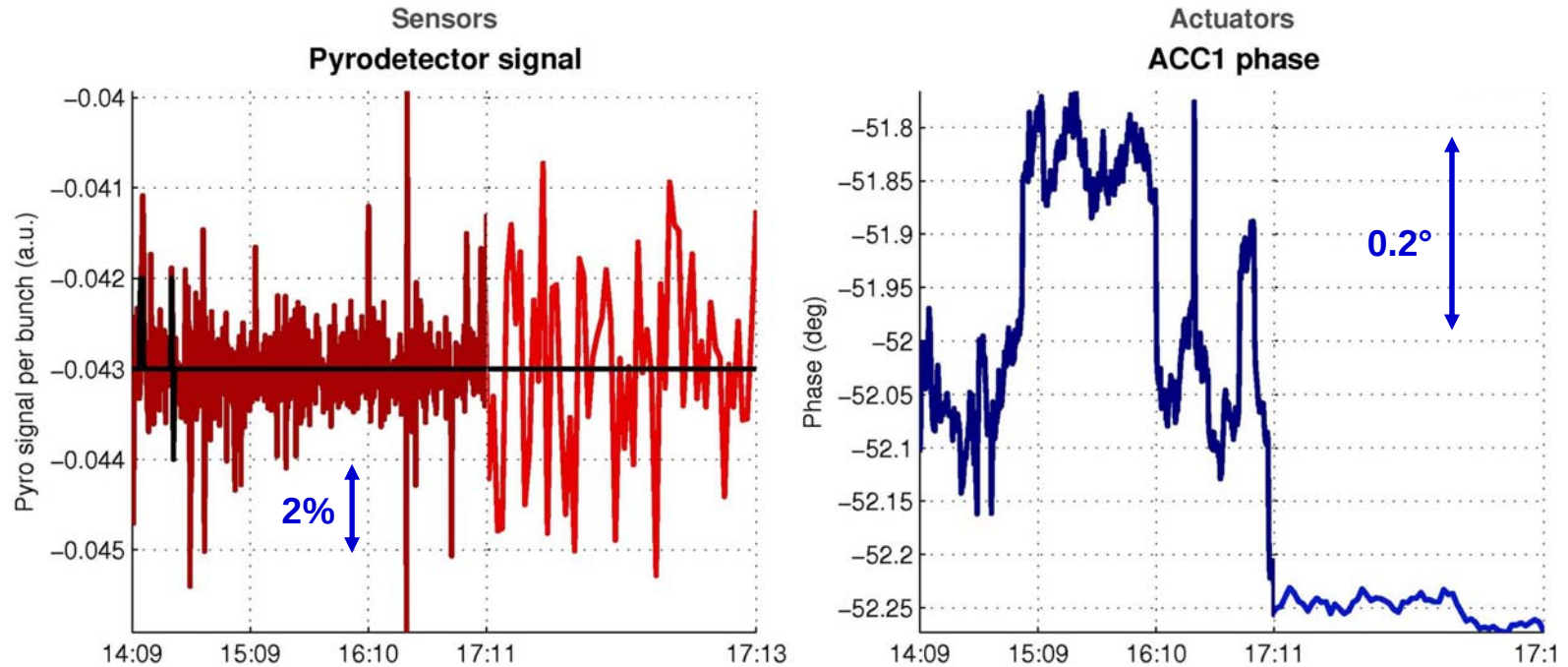
Transition/Diffraction Radiator



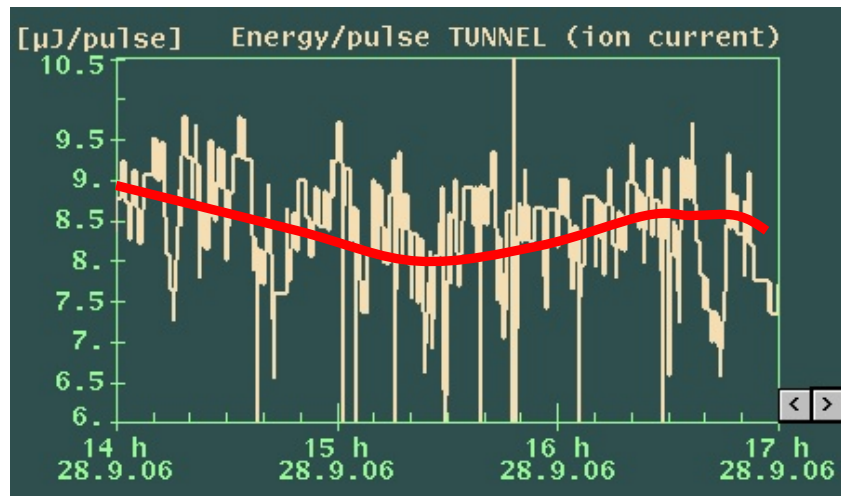
Phase/compression scan



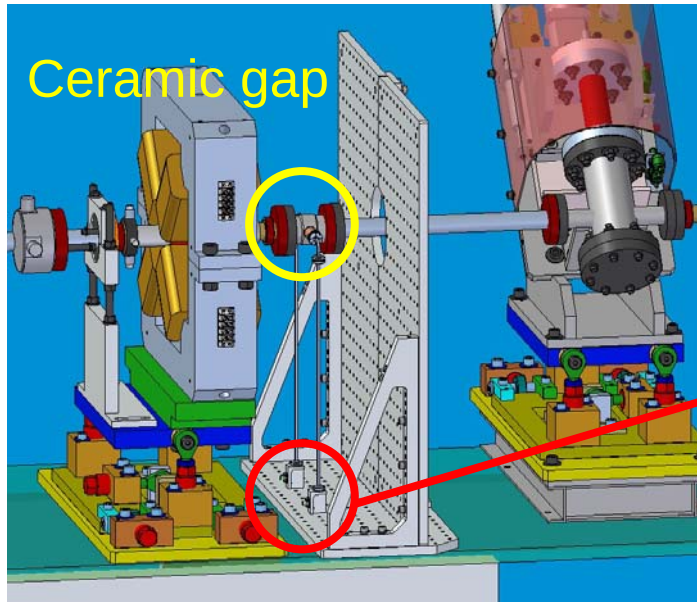
Compression monitor feedback on phase



SASE intensity

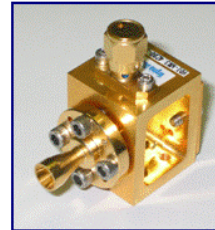


Diode detector as bunch compression monitor

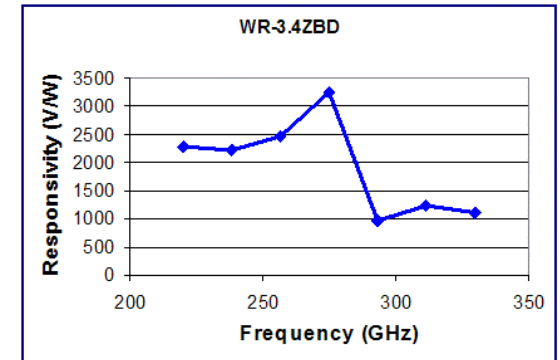


VDI Virginia Diodes, Inc.

- Tunerless Design
- No bias required
- NEP: $1\text{E-}10\text{ W/Hz}^{0.5}$ (typ.)
- TSS: -44 dBm (typ.)
TSS measured with 30 kHz video bandwidth



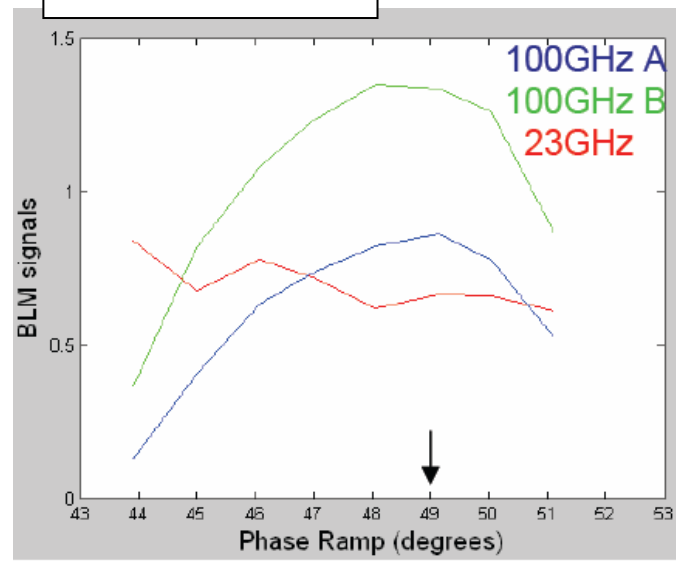
VDI Model: WR3.4ZBD
220-330 GHz Zero Bias Detector



Contact VDI today for specifications and quotation details.

Virginia Diodes, Inc., Ph:434.297.3257, FAX:434.297.3258, www.virginiadiodes.com, VDIRFQ@virginiadiodes.com

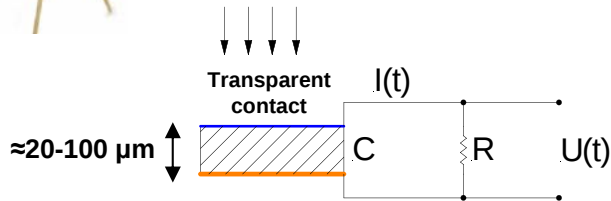
Phase scan



Courtesy J. Frisch, SLAC

Pyroelectric detector

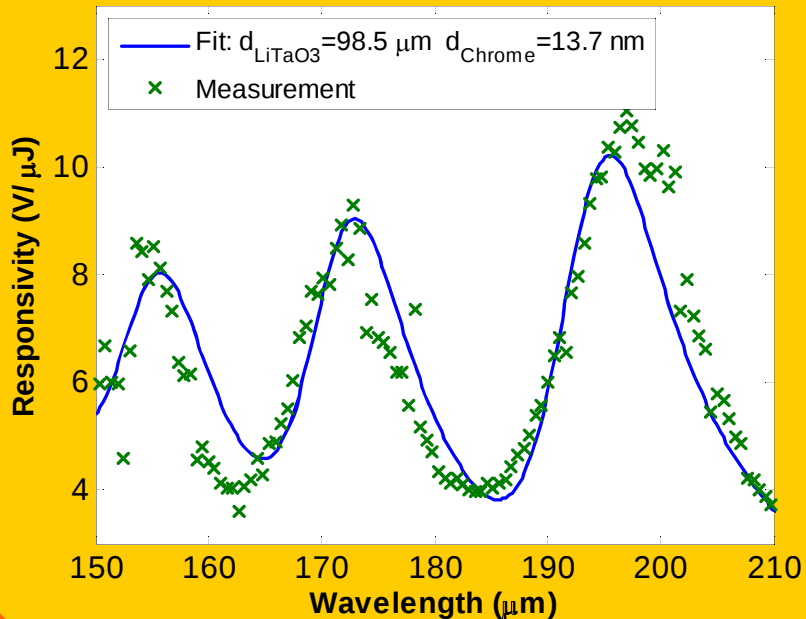
— room-temperature —



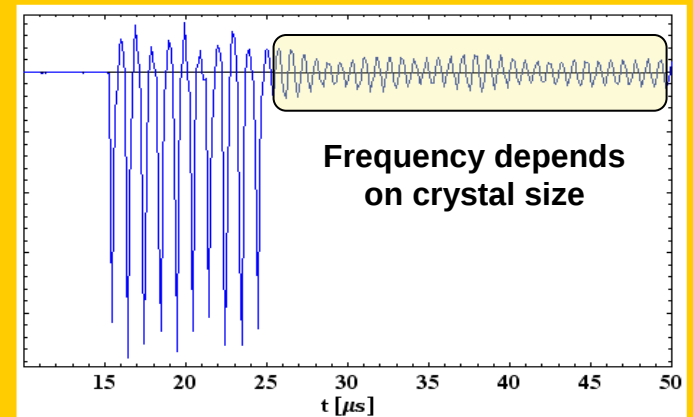
Absorption of radiation

- Conversion into temperature variation
- Conversion into polarization (pyroelectric effect)
- Detection of charge/current/voltage

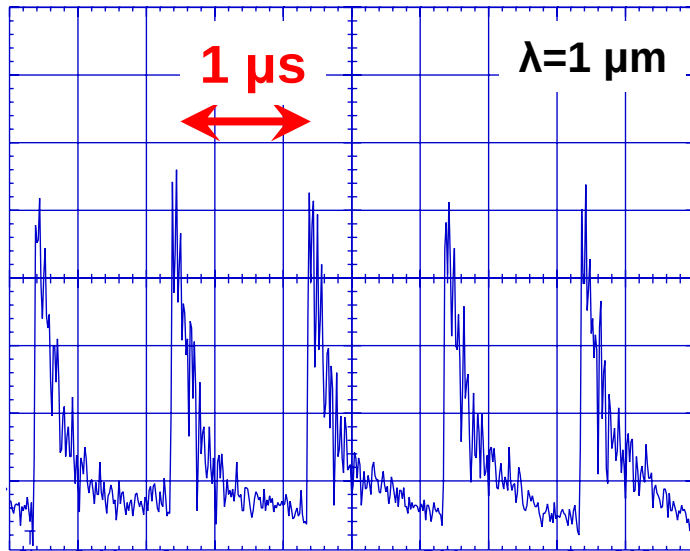
Etalon interferences



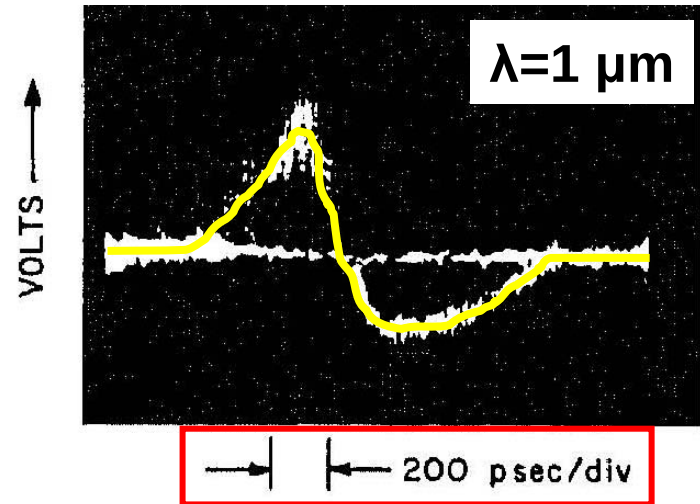
Piezoelectric vibrations



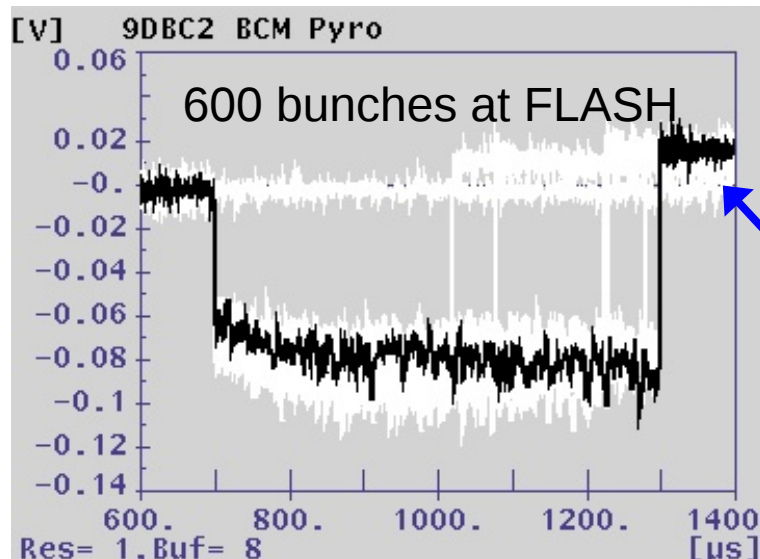
Pyros are intrinsically fast



...even very fast!



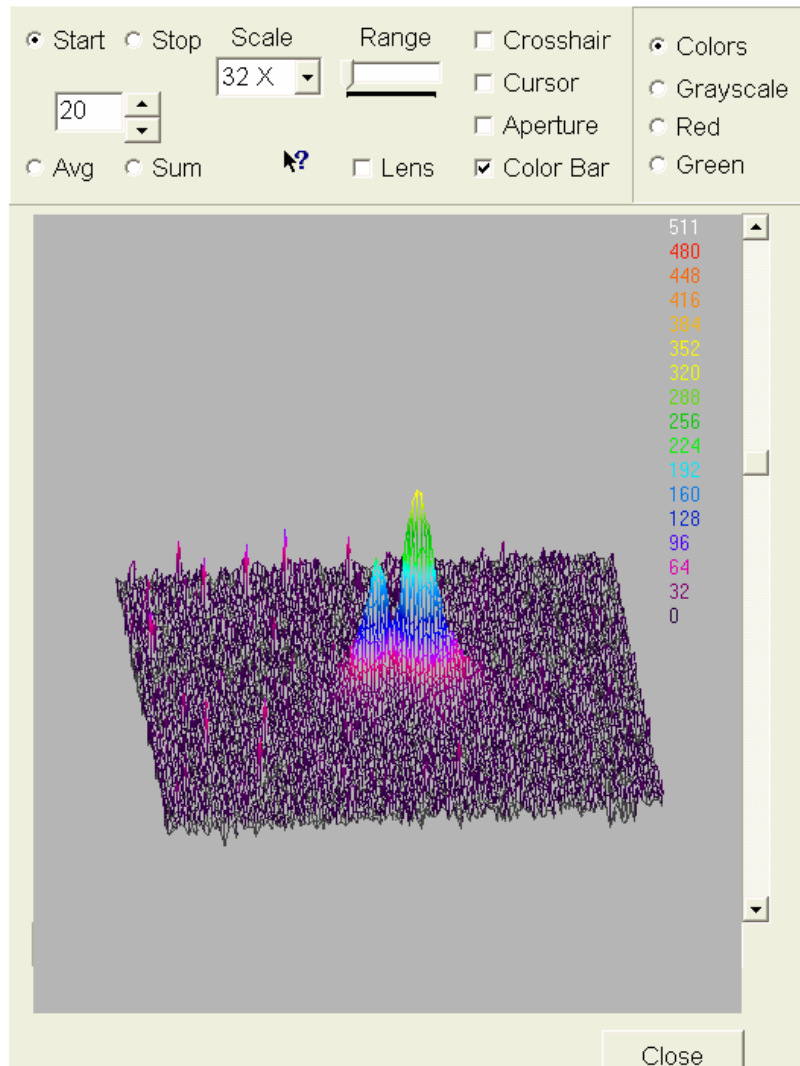
from: C.B. Roundy,
SPIE Vol. 62, 191 (1975) Infrared Technology



Heating of pyro
($\tau_{\text{thermal}} \approx 100 \text{ ms}$)

Pyrocam

Transition radiation at FLASH



Spiricon pyroelectric camera (LiTaO_3)

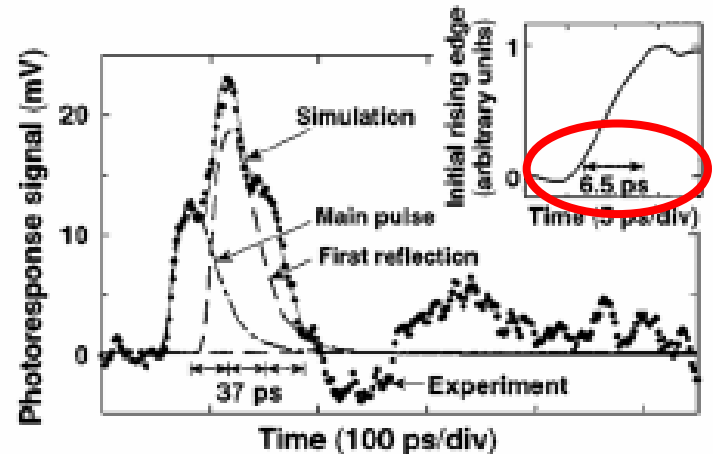
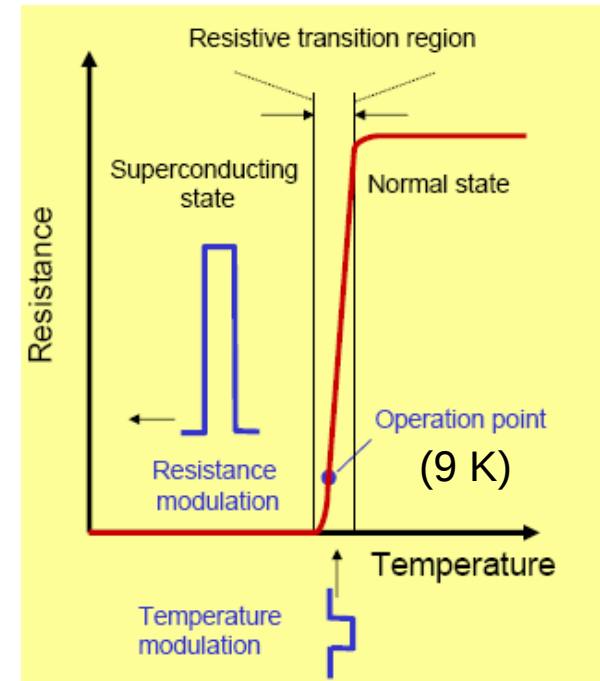
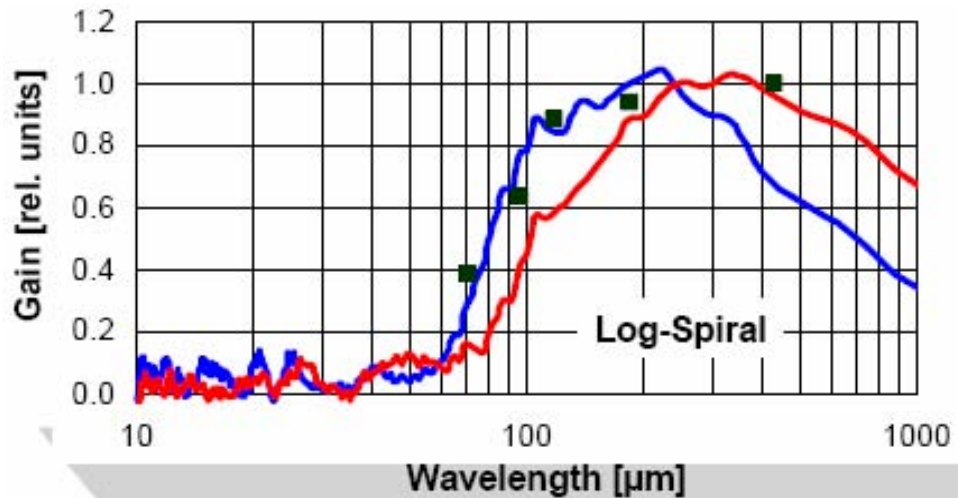
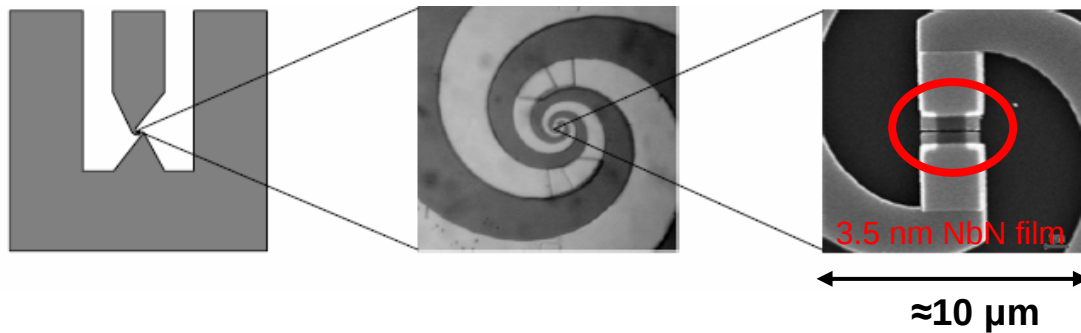
124x124 pixels, 100 μm pitch

7 nJ per pixel noise limit



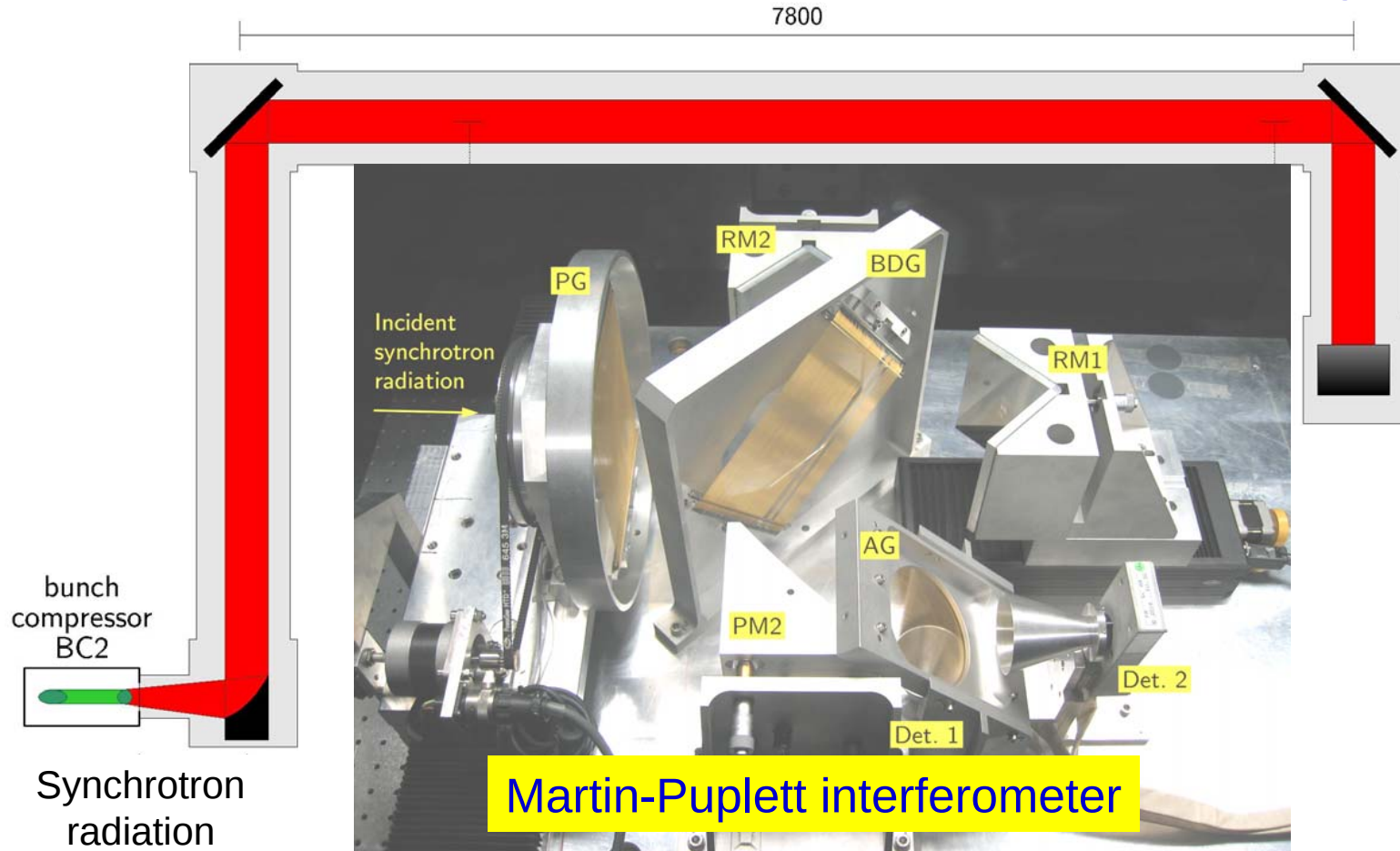
Fast superconducting hot-electron bolometer

Log-spiral antenna receiver

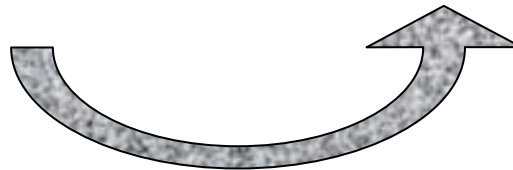
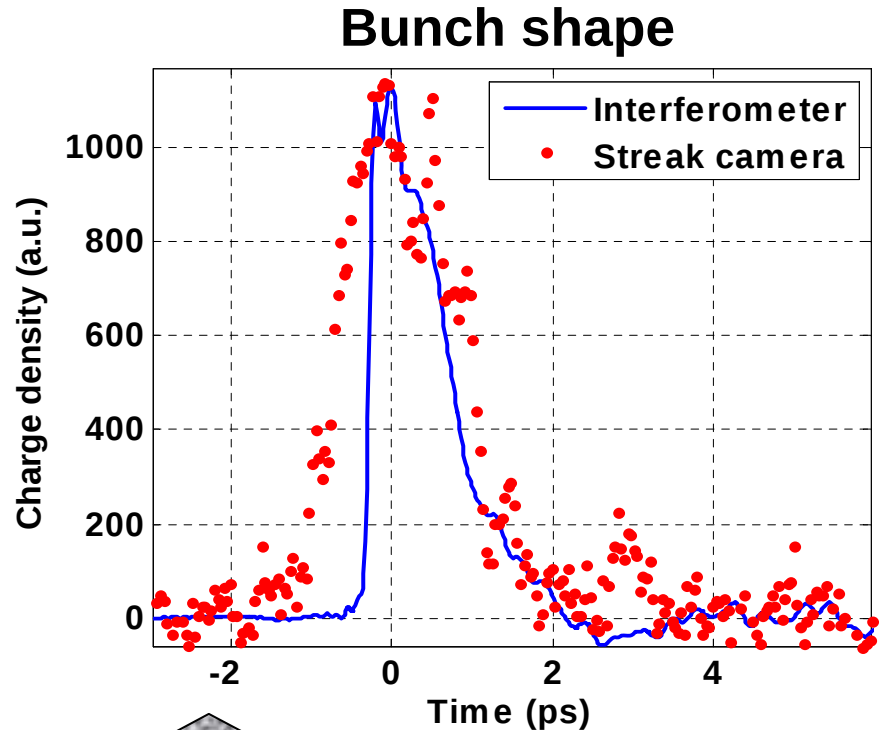
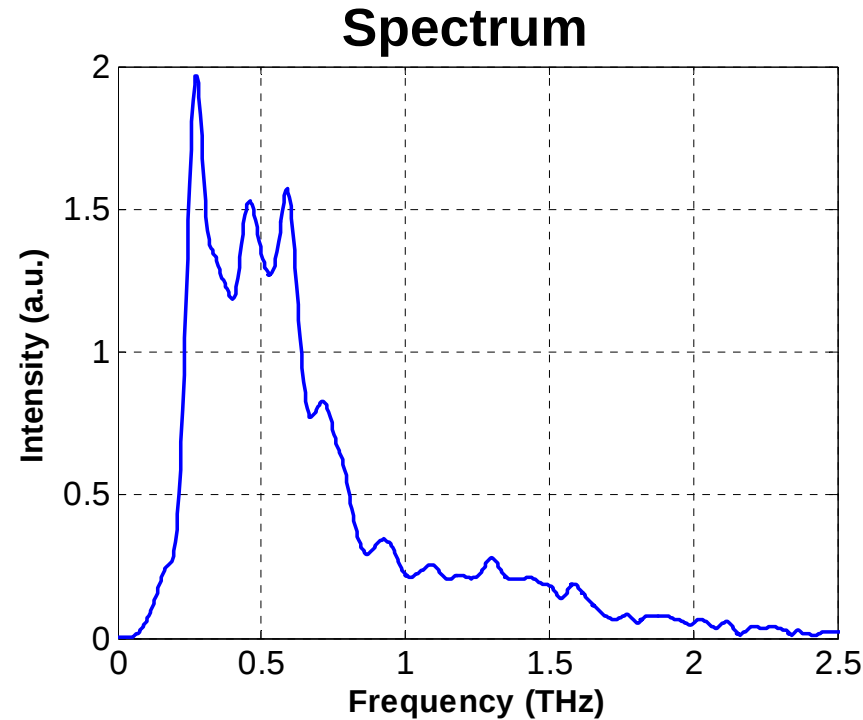


FLASH synchrotron radiation beamline

For **experimental studies**, an **accessible laboratory** outside of the accelerator confinement is **mandatory**.

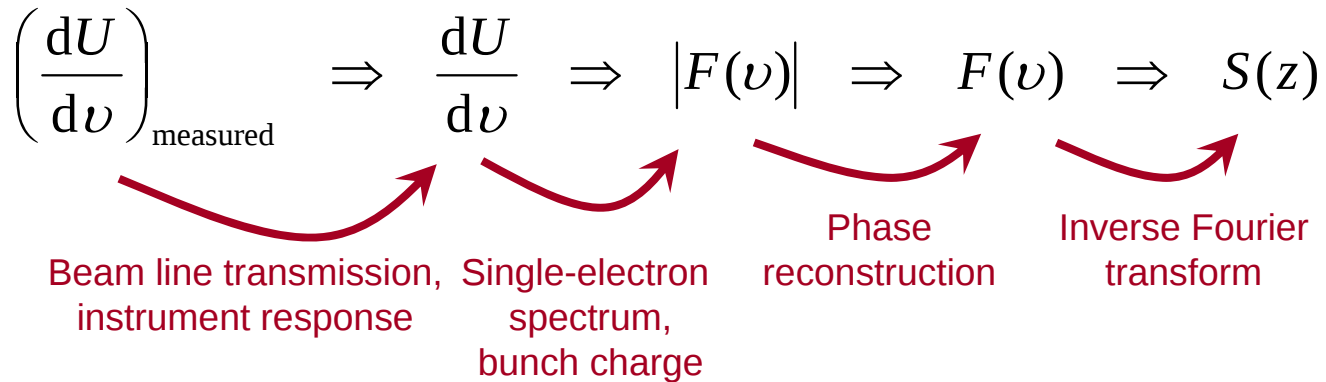


Bunch reconstruction



through inversion of
$$\frac{dU}{d\nu} = \left(\frac{dU}{d\nu} \right)_1 \left(N + N(N-1) |F(\nu)|^2 \right) \quad F(\nu) = \int S(t) e^{2\pi i \nu t} dt$$

The reconstruction procedure



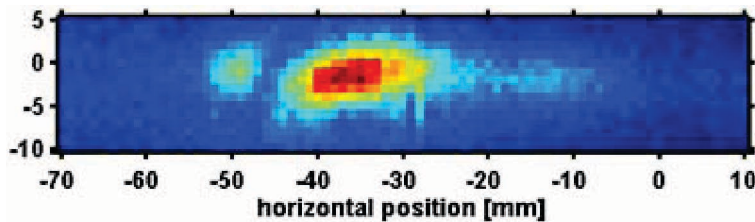
Complex form factor $F(\nu) = |F(\nu)|e^{i\Theta(\nu)}$

Kramers - Kronig relation (phase retrieval)

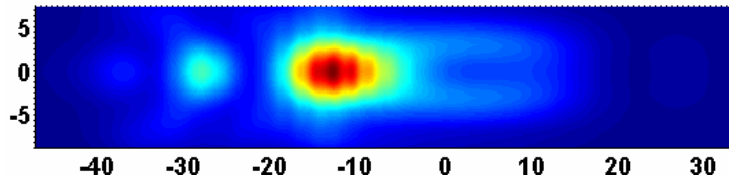
$$\Theta(\nu) \geq \frac{2\nu}{\pi} \int_0^{\infty} \frac{\ln \frac{|F(\nu')|}{|F(\nu)|}}{\nu^2 - \nu'^2} d\nu'$$

Synchrotron radiation is a complex source...

Measurement ($\lambda=155\text{ }\mu\text{m}$)

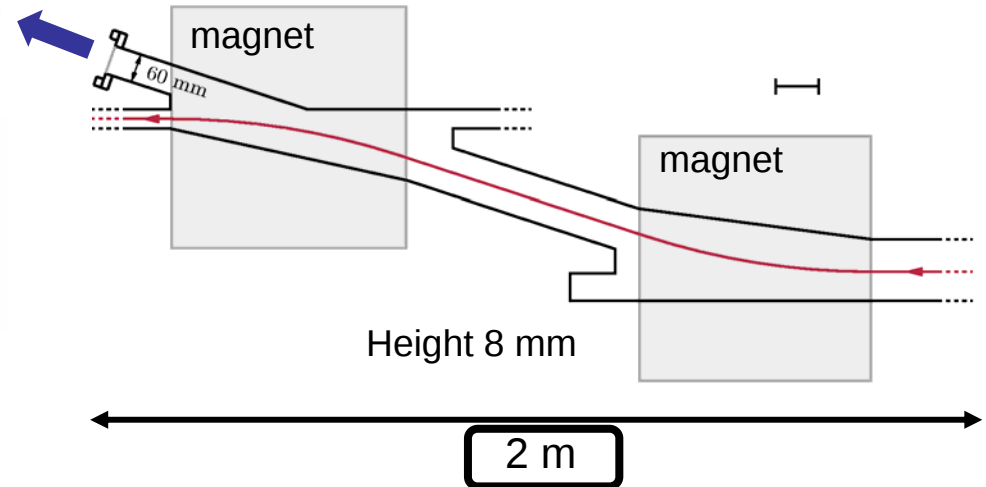


Simulation using UTD



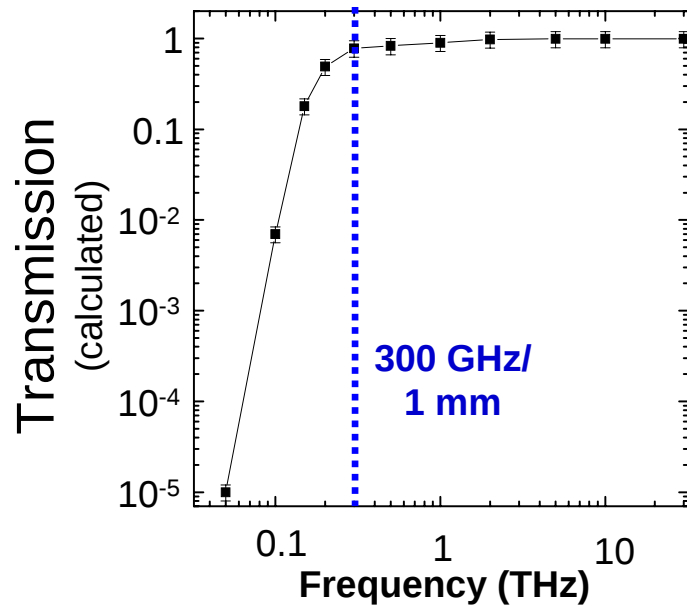
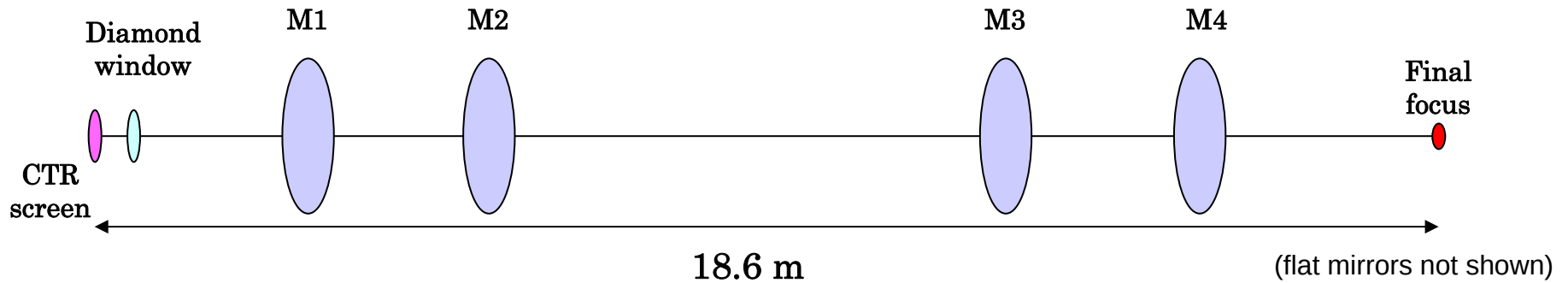
Uniform Theory of Diffraction =
geometrical optics + diffraction

- Edge effects
- Shielding

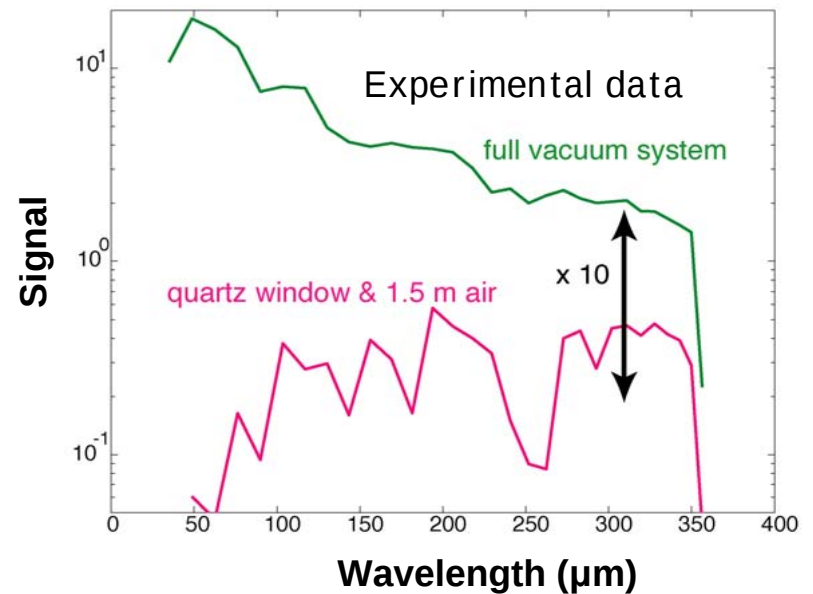


Poster Friday: FRPMN015

FLASH transition radiation beamline

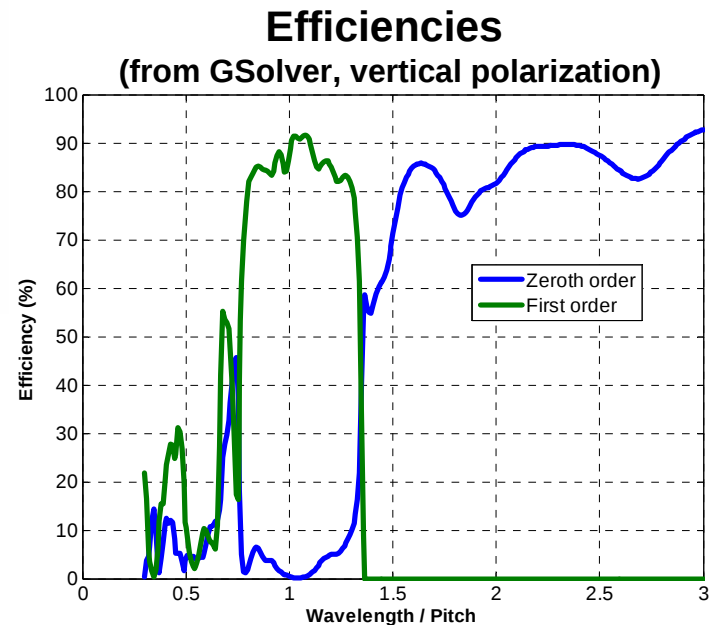
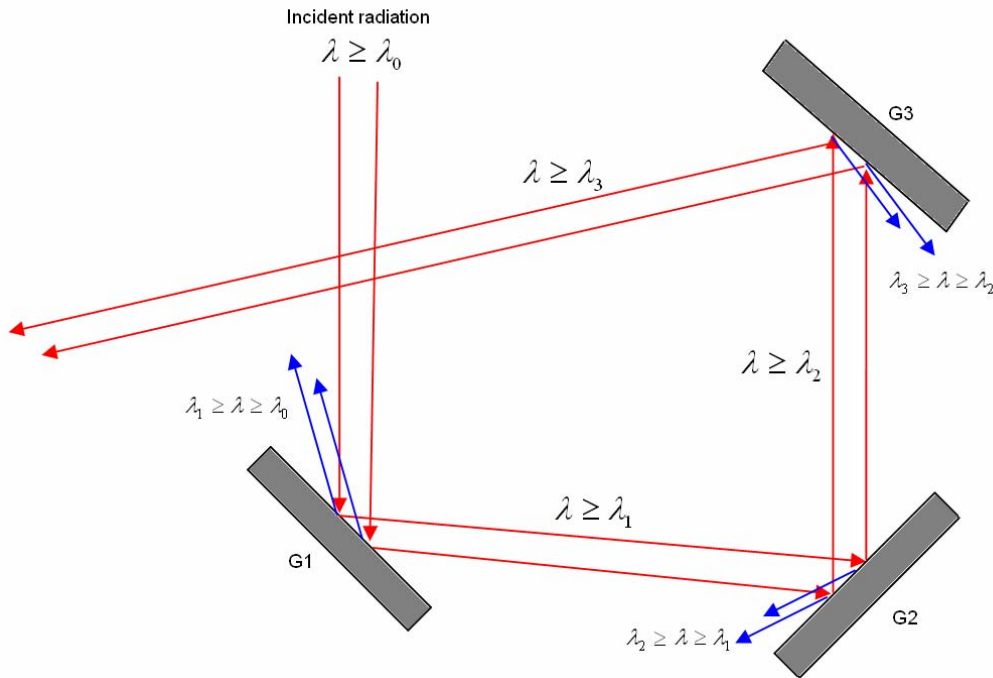


Advantage of vacuum+diamond

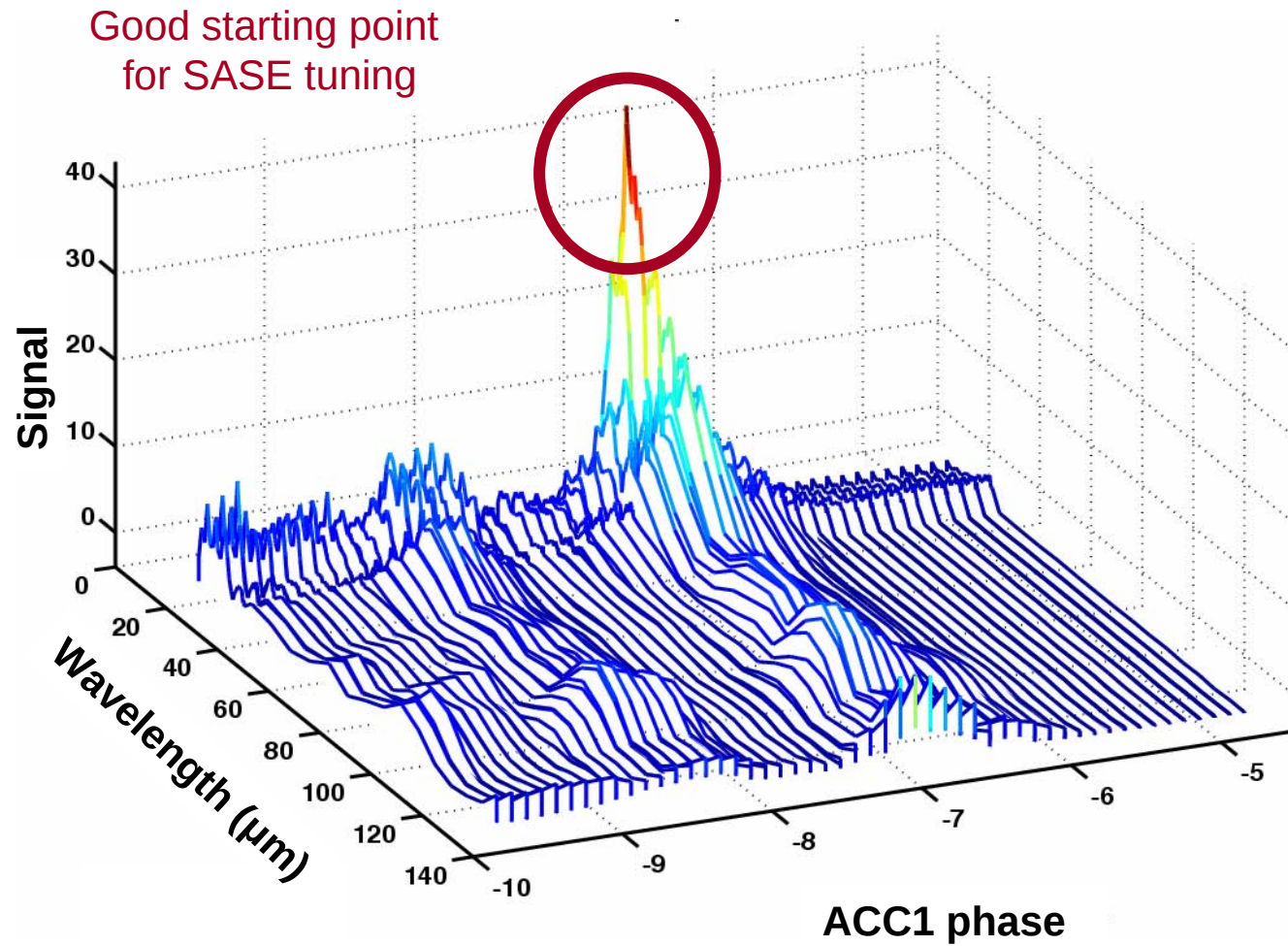


Single shot grating spectrometer

Based on staged blazed gratings

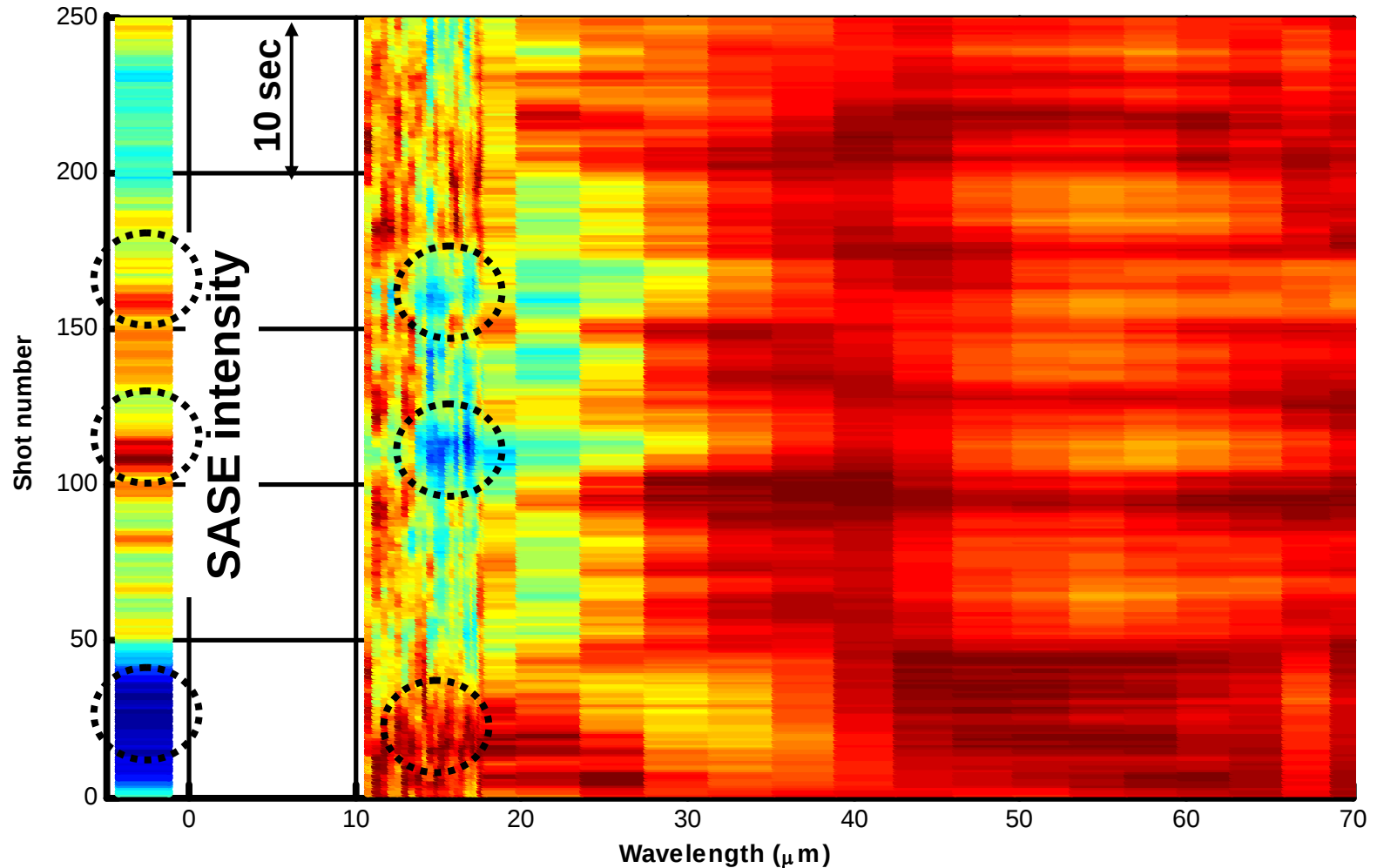


Phase scan



Correlations

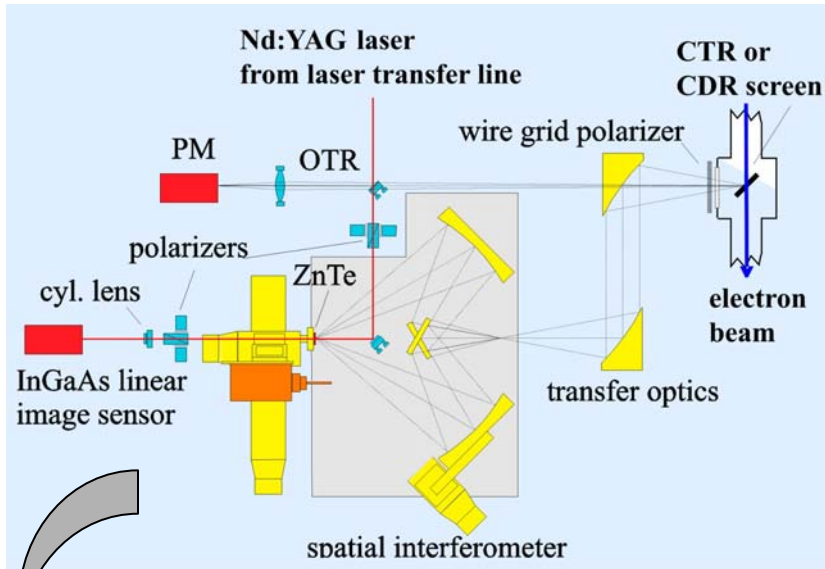
Fluctuations over 50 seconds of stable SASE run



Anti-correlation!

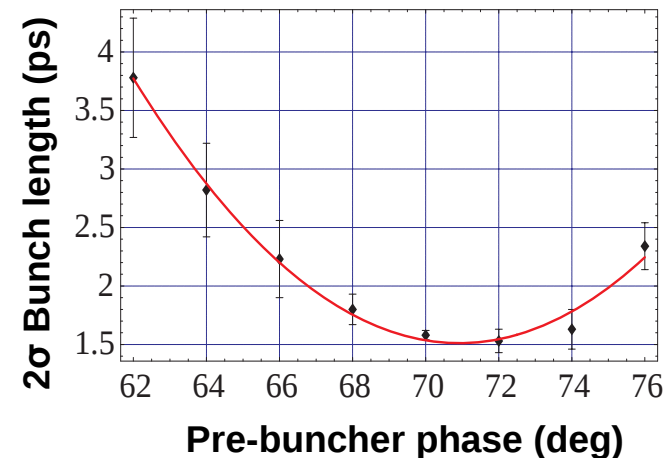
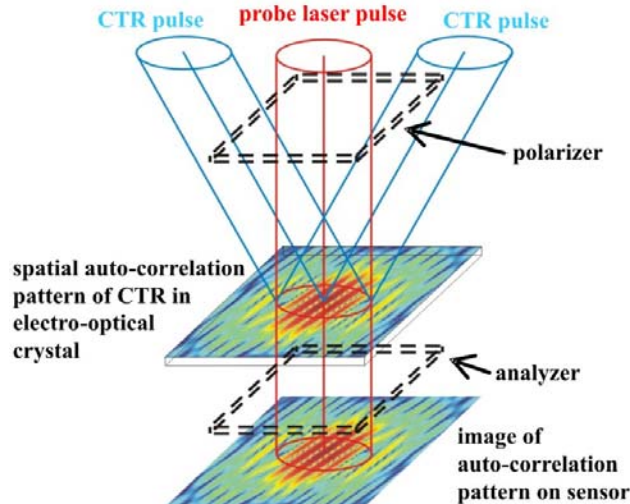
Courtesy H. Delsim-Hashemi, DESY

Spatial Electro-Optical Auto-Correlation Interferometer (PSI)



- Interferometer images coherent transition radiation onto electro-optic crystal
- Spatial auto-correlation pattern read out by Nd:YAG laser using cross polarizer scheme and linear image sensor
- Single shot bunch length monitor providing ~200 fs resolution

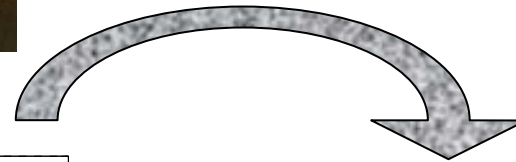
Measurement at SLS pre-injector LINAC



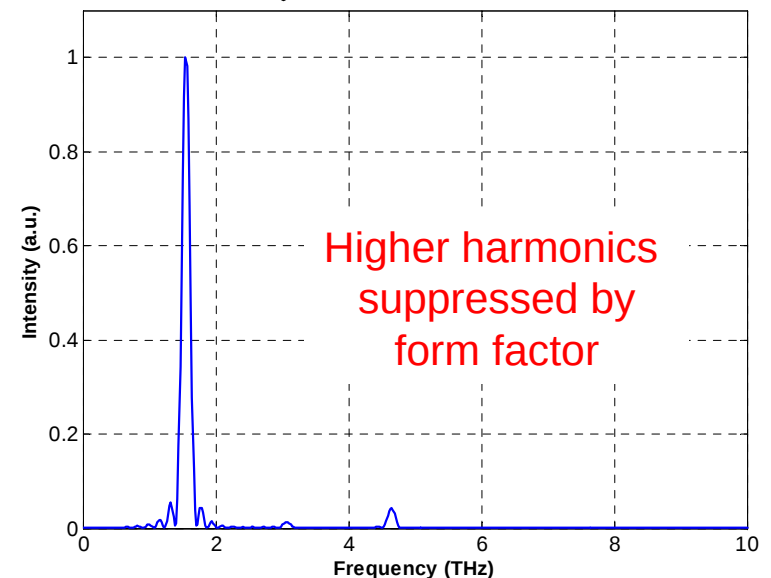
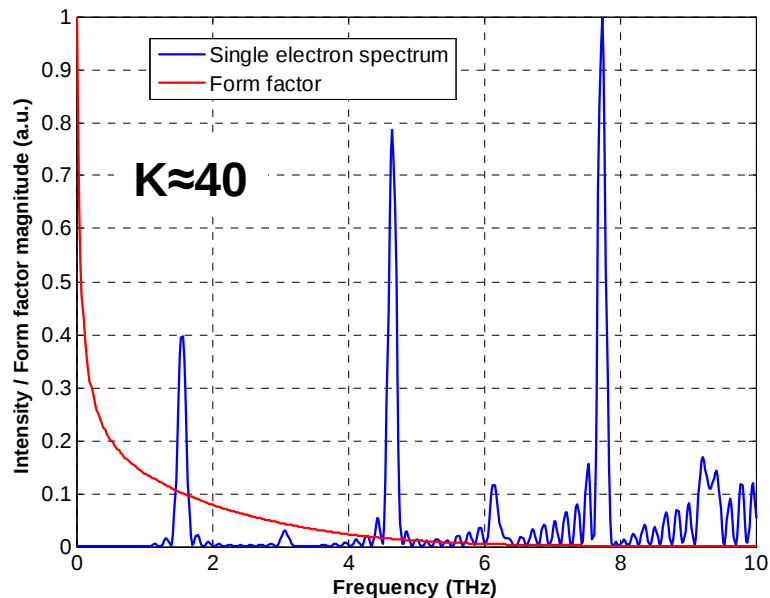
FLASH infrared undulator

Electromagnetic undulator, tuneable **1-200 μm** (at 500 MeV)

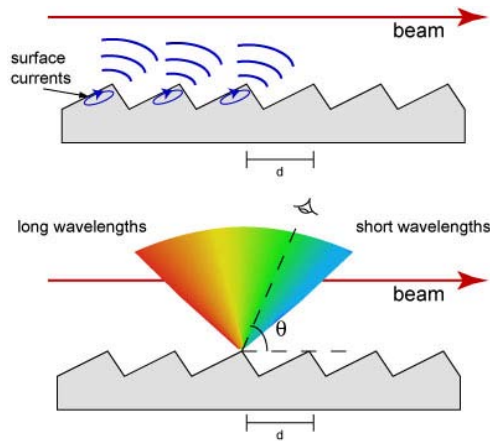
The same bunches generate SASE and infrared radiation (naturally synchronized)



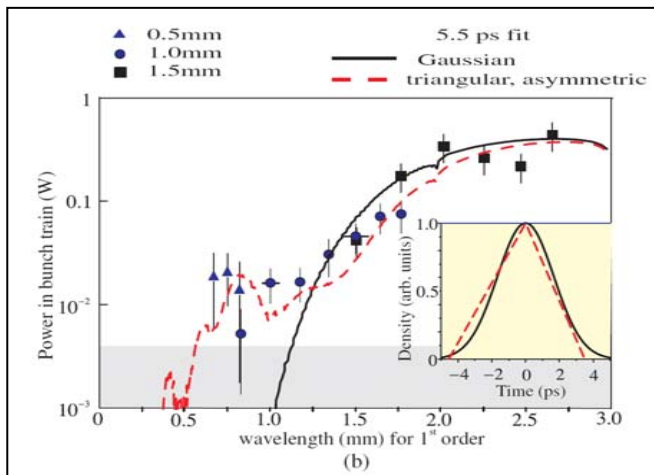
**Total emission
spectrum**



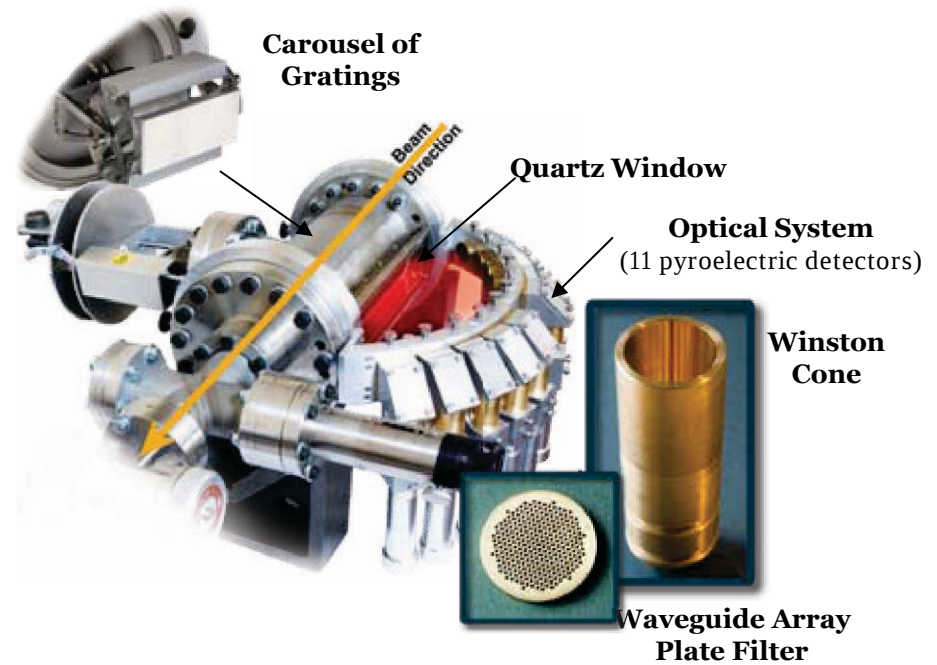
Smith-Purcell radiation measurements



Measurement at 45 MeV, FELIX



see PRST 9,092801 (2006)



Results of a run at 28.5 GeV from SLAC are currently being analyzed.

Courtesy G. Doucas, V. Blackmore, Oxford

Summary

- **Longitudinal bunch shape investigations** using coherent radiation are a **standard tool** for all machines operating with short bunches or bunch features (slicing).
- **Standard tools** employ **non-calibrated** devices.
- Full longitudinal charge profile reconstruction is a **specialist application** (thesis level...).
- Additional benefit from **wide wavelength coverage** in a **single-shot manner** — comes at the price of higher **hardware complexity** (vacuum, diamond window, optics)

***Thanks very much for the kind help of many colleagues
who provided material (of which I could not cover everything, sorry!)
or advise!***

Phase retrieval – Kramers-Kronig relations

Generally, **Kramers-Kronig relations** result from an expression

$$\text{Response} = \text{Stimulus} \times \text{Response function}$$

and connect the real and imaginary part of the response function.*

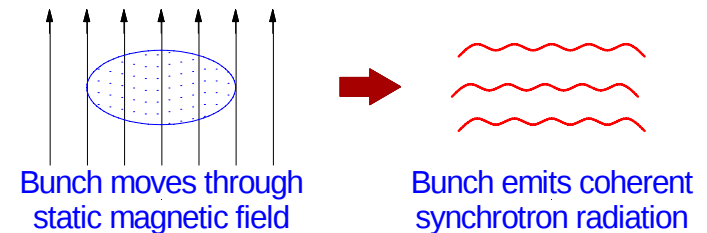
— Formal relation —

$$\begin{aligned} \underbrace{\langle E(\nu) \rangle}_{\text{Response}} &= E_1(\nu) \left\langle \sum e^{2\pi i \nu \Delta t} \right\rangle \\ &= E_1(\nu) \int NS(z) e^{\frac{2\pi i \nu z}{c}} dz \\ &= \underbrace{NF(\nu)}_{\text{Response function}} \underbrace{E_1(\nu)}_{\text{Stimulus}} \end{aligned}$$

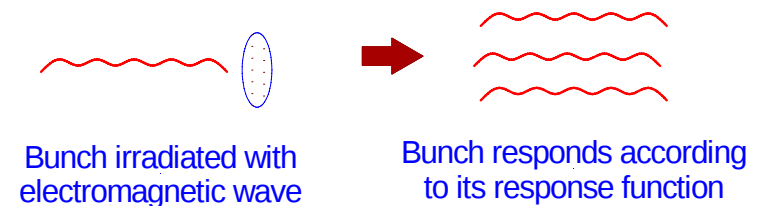
Check concept with Lorentz-Transformation of static field etc.

— Conceptual picture — (for synchrotron radiation)

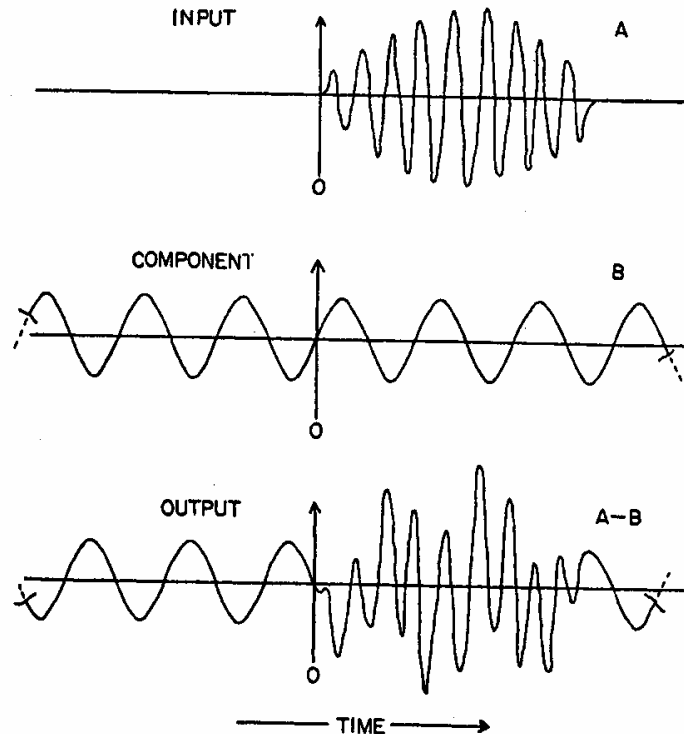
Laboratory system



Co-moving system



Where is the connection between phase and magnitude?



Original time dependent signal
(=0 for $t < 0$)

One Fourier component

Signal if this component is removed
($\neq 0$ for $t < 0$)

FIG. 1. This figure illustrates schematically the basic reason for the logical connection of causality and dispersion. An input A which is zero for times t less than zero is formed as a superposition of many Fourier components such as B , each of which extends from $t = -\infty$ to $t = \infty$. These components produce the zero-input signal by destructive interference for $t < 0$. It is impossible to design a system which absorbs just the component B without affecting other components, for in this case the output would contain the complement of B during times before the onset of the input wave, in contradiction with causality. Thus causality implies that absorption of one frequency must be accompanied by a compensating shift of phase of other frequencies; the required phase shifts are prescribed by the dispersion relation.

Conclusion: The **phases** must be automatically **adjusted** (e.g. by a filter) such that signal=0 for $t < 0$.

From: John S. Toll,
Phys. Rev. **104**, 1760(1956)